

July 1968

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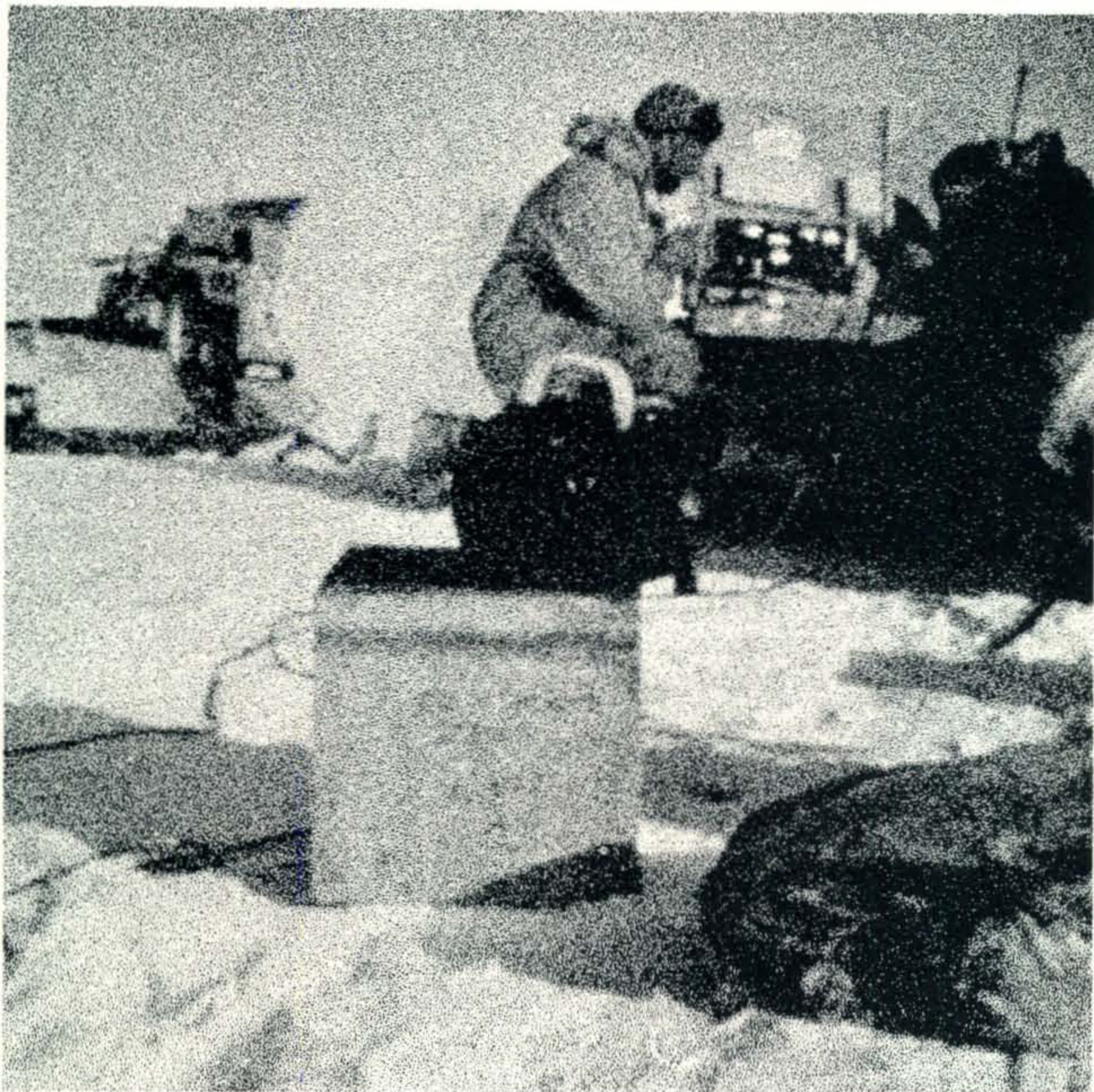
*newsletter*  
**CQ**  
ICD

**CQ W.W.  
C.W. DX**

**Contest Results: Page 34**



**The Radio Amateur's Journal**



# Barefoot to Ninety North

Four hundred seventy-five air miles—825 actual land miles—over the Arctic pack ice. Forty-four days on a frozen sea with temperatures down to 63° below. Finally: the Pole. Collins' KWM-2 furnished reliable communications every rugged mile of the Plaisted Polar Expedition. Just an example of the KWM-2's reserve performance and rugged dependability.



# NEW FROM INTERNATIONAL



## FM-2400 FREQUENCY METER

- For Mobile Or Base Station Use
- Tests Predetermined Frequencies 25 - 470 MHz
- Portable . . . Use It Anywhere

The FM-2400 is designed for testing and adjustment of mobile and base station transmitters and receivers at predetermined frequencies between 25 and 470 MHz. The FM-2400 provides an accurate standard frequency signal to which the transmitter can be compared. This same signal is applied to the associated receiver(s), thereby assuring an accurate frequency adjustment on all parts of the communications system.

Up to 24 crystals may be inserted into the meter for the selection of the frequencies required for testing of the system transmitters and receivers. The frequencies can be those of the radio frequency channels of

operation, and/or of the intermediate frequencies of the receiver between 100 KHz and 100 MHz. Self contained unit. Battery operated.

FM-2400 (meter only).....	\$395.00
RF Crystals with temperature run.....	\$23.50 ea.
IF Crystals	
200 - 2,000 KHz .....	See Catalog*
2,001 - 13,000 KHz.....	See Catalog*

\*WRITE FOR FREE CATALOG



CRYSTAL MFG. CO., INC.  
10 NO. LEE • OKLA. CITY, OKLA. 73102

# 10 reasons to buy Hallicrafters' new SR-400 Cyclone

FEATURE	Hallicrafters SR-400	Collins* KWM-2	Drake* TR-4
Power Input	SSB=400 watts CW=360 watts	SSB=175 watts CW=160 watts	SSB=300 watts CW=260 watts
Accessory "dual receive" VFO available	Yes	No	No
Noise Blanker	Yes	\$135.00 Accessory	No
Receiver Incremental Tuning	Yes	No	No
Built-in notch Filter	Yes	No	No
Sharp CW Filter	Yes 200 cycles	No	No
Sensitivity	.3 uv for 10 db S/N	.5 uv for 10 db S/N	.5 uv for 10 db S/N
1 kHz dial readout	Yes	Yes	No
Carrier Suppression	60 db	50 db	50 db
Unit Price	\$799.95	\$1,150.00	\$599.95

\*Data from published specifications.

## Now: can you think of one reason why you shouldn't?

Superb sensitivity, 400 watts RF, 200 cycle CW selectivity, receiver incremental tuning, 1 kHz readout, amplified automatic level control, exclusive notch filter! There's even the HA-20 dual receive VFO for sensational, award winning DX operation. No matter what specifications or features you choose as a standard of comparison, the exciting new SR-400 fixed/mobile transceiver is unsurpassed. Unsurpassed feature for feature. Unsurpassed for rugged dependable performance in all environments. Unsurpassed in value and versatility. Prove it to yourself. Write for complete specifications in a four page brochure. See your Hallicrafters' distributor today.



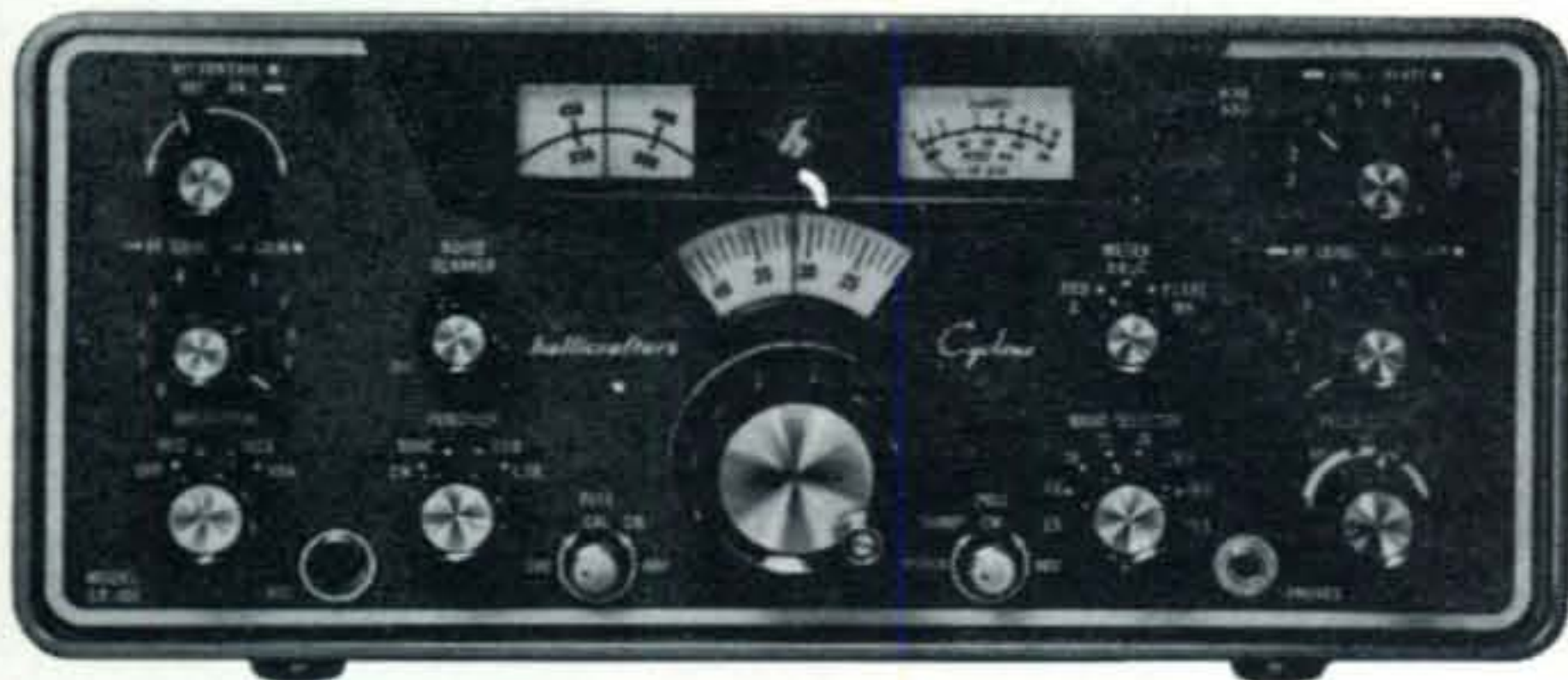
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600 Hick Rd., Rolling Meadows, Ill. 60008

A Subsidiary of Northrop Corporation

SR-400 Cyclone Transceiver

HA-20 VFO



Export: International Dept. Canada: Gould Sales Co.



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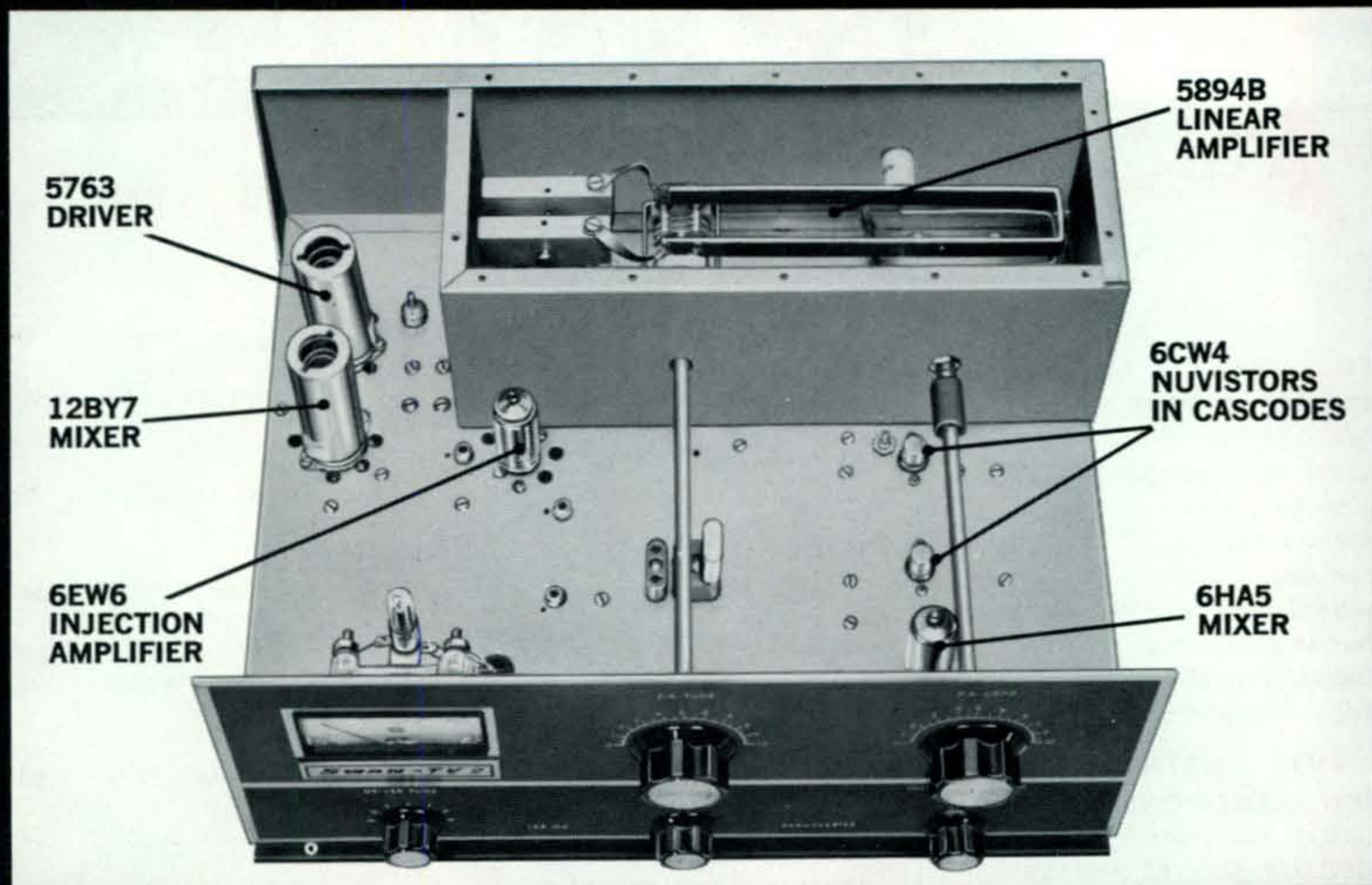
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# 2 METER SINGLE SIDEBAND

144-148 mc 240 WATTS P.E.P. INPUT



## THE NEW SWAN TV-2 TRANSVERTER

A receiving and transmitting converter for the 2 meter band, designed to operate with Swan Transceivers, models 250, 350, 350-C, 400, 500, and 500C.

### SPECIFICATIONS:

14 mc intermediate frequency is standard. Thus, when operating the Transceiver from 14 to 14.5 mc, the Transverter functions from 144 to 144.5 mc. Additional crystals may be purchased and switched in for other portions of the 2 meter band, such as 144.5-145, and 145 to 145.5 mc. Three crystal positions are available.

Alternately, the TV-2 Transverter may be ordered for an I.F. in the 21, 28 or 50 mc bands, if desired. Of course, for use with a Swan 250 six meter transceiver, the Transverter must be ordered for 50 mc. Otherwise, the standard 14 mc I.F. is recommended since bandsread and frequency read-out will then be optimum. The Transverter can easily be adjusted in the field for a different I.F. range, if required.

A 5894 B Power Amplifier provides a PEP input rating of 240 watts with voice modulation. CW input rating is 180 watts, and AM input is 75 watts.

Receiver noise figure is better than 3 db, provided by a pair of 6CW4 nuvistors in cascode.

Only a Swan Transceiver and Swan AC power supply, Model 117-XC, are required. The power supply plugs into the Transverter, and the Transverter in turn plugs into the Transceiver. Internal connections automatically reduce the power input to the Transceiver to the required level.

Tube complement: 5894B Pwr. Amp., 5763 Driver, 12BY7 Transmit Mixer, 2N706 crystal osc., 6EW6 Injection Amp., 6CW4 1st rec. amp., 6CW4 2nd rec. amp. in cascode, 6HA5 rec. mixer.

The Swan TV-2 may also be operated with other transceivers when proper interconnections and voltages are provided. A separate Swan 117-XC power supply will most likely be required.

Dimensions: 13 in. wide, 5½ in. high, by 11 in. deep.  
Weight: 13 lbs.

**\$265**



MODEL 250 ..... \$325  
MODEL 350C ..... 420  
MODEL 500C ..... 520

MODEL 117-XC  
AC POWER SUPPLY .. \$105

MODEL TV-2  
144 mc TRANSVERTER

  
**SWAN**  
ELECTRONICS  
Oceanside, California  
A SUBSIDIARY OF CUBIC CORP.



## ZERO BIAS

It's interesting how we amateurs seem to live by a distorted and often hypocritical set of standards. I'm not about to get up on my soap box and preach; I'm too confused about what ails us to do that, but rather I'd like to share a few thoughts.

For over four years we've been surrounded by controversy stemming from the word "incentive." Someone dared to suggest that American amateurs were not as adept and knowledgeable about their medium—radio—as they might be, and that someone—ARRL—proceeded to move to rectify the situation. Four years of squabbling and disention ensued, with opinion often appearing to be evenly divided between "Yes, let's improve ourselves" and "I'm ok the way I am." Finally, last Autumn, the decision was made by FCC to adopt an incentive program of amateur licensing which would attempt to upgrade the technical status of American amateurs. The squabbles surged forward one last time and then subsided, seemingly for good.

Two months ago, a new cry was heard, this time from the new amateur radio section of EIA. The latest contention is that amateur standards in the U.S. are too high for the newcomer, and must be reduced or we will risk the demise of our hobby. Funny, isn't it, how the pendulum swings? And funny, too, how the reaction of the individual amateur has swung in the opposite direction. Only a year ago so many readers argued against the upgrading of amateur license exams, with many voicing fears that the too-high standards would stifle the hobby. What we hear now is just the opposite. The proposal now is for reduced standards, but the public reaction is much the same. Our letters-to-the-Editor column this month gives only the scantest suggestion of the volume of similar mail we've received in the past few weeks. The average reader just won't hear of lowering the standards. Now suddenly, the code becomes important to these amateurs, and the technical examination becomes a needed weeding out device.

As I said at the start, I'm not criticizing or taking a stand. The whole thing has me a bit baffled right now, but I thought you might like to wonder along with me.

### More Reading In Store

A year ago, *CQ* did a little much-needed facelifting, bringing new life to an otherwise good magazine. The addition of four-color covers, higher quality paper, and color throughout the magazine seemed to alter the attitudes of readers and authors alike, with a more aware and up-to-date feeling permeating the pages month after month.

Also at that time we hinted of better things to come, so beginning next month and continuing at least through the November issue, *CQ* will expand at the rate of eight pages a month with the goal 152 pages for November. Further growth depends on several factors: reader support, advertising support, rate of supply of articles, and most important, the number of *new* subscribers we can add to the *CQ* subscription rolls as a result of publishing the most exciting magazine in amateur radio.

The advertising boys and circulation department are carrying the ball in their own areas, but the quality and quantity of editorial material in *CQ* is largely dependent upon the every day ordinary *CQ* reader who is responsible for fully *two-thirds* of the non-column text we print each month. Check a few issues. You'll notice that the great majority of authors are *not* the professional or semi-pro writers who eke out a living behind a typewriter. Most articles are written by John Q. Amateur who will probably publish a single article in his literary "career".

What we're leading up to is that in the months to come, *CQ* will be printing a great many more articles than it has before, and *they will be the best*. High editorial standards cost money. We're willing to pay, at the highest rates in the field, and if you've got something we really want, no magazine in amateur radio is going to out-bid us! That's a promise. A lot of good reading matter is going to go unpublished in *CQ* simply because good isn't going to be enough. The Best is what *CQ* represents from here on in.

73, Dick, K2MGA

# EIMAC

## 3-500Z's used in Drake's linear amplifier for 2 kW PEP at 3.5-30 MHz

The R. L. Drake L-4B linear amplifier shown here uses two of EIMAC's new 3-500Z zero-bias triodes in grounded grid circuitry to achieve 2-kW PEP SSB input and 1-kW dc input on CW, AM, and RTTY. Drive power is 100 watts PEP and 75 watts CW, AM, and RTTY.

Drake chose EIMAC 3-500Z's because these rugged, compact, high-mu power triodes are ideal for grounded grid operation. They can provide up to 20 times power gain in a cathode driven circuit. And the two tubes have a total plate dissipation rating of 1000 watts.

For more information on EIMAC's line of power tubes for advanced transmitters, write Amateur Services Department, or contact your nearest EIMAC distributor.

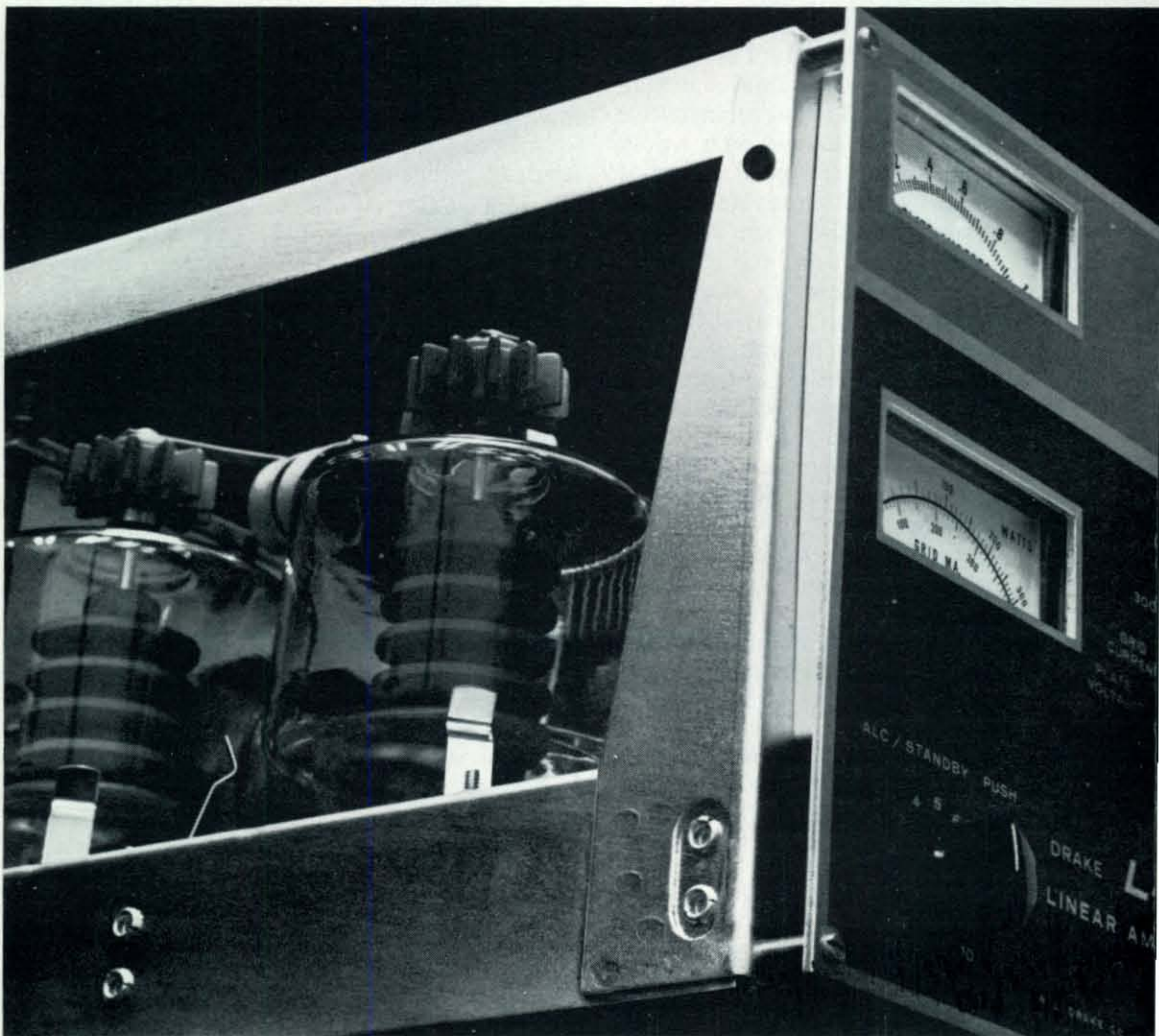
### 3-500Z TYPICAL OPERATION\*

DC Plate Voltage .....	2500 V
Zero-Sig DC Plate Current** .....	130 mA
Single-Tone DC Plate Current .....	400 mA
Single-Tone DC Grid Current .....	120 mA
Two-Tone DC Plate Current .....	280 mA
Two-Tone DC Grid Current .....	70 mA
Peak Envelope Useful Output Power .....	500 W
Resonant Load Impedance .....	3450 ohms
Intermodulation Distortion Products .....	-33 dB

\*Measured data from a single tube

\*\*Approximate

**EIMAC**  
Division of Varian  
San Carlos, California 94070





# LARGE ANTENNA LOAD



## BUILT FOR WIND

### THE TRI-EX FREESTANDING

# LM 470

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This advanced state of the art tower is aerodynamically designed to reduce tower wind drag. This means you can carry more antenna than ever before. Tri-Ex engineers have made this possible by using high-strength, solid-steel rod bracing. Only at Tri-Ex do you get "W" type continuous truss bracing. Developer of the freestanding, crank-up tower, Tri-Ex prides itself on the quality of its products. More Tri-Ex crank-up towers are in use today than all other crank-up towers combined. Find out why the LM 470 tower is such an outstanding success. Write today for free literature.

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# OUR READERS SAY

## EIA Proposal

Editor, *CQ*:

Now that the EIA has proposed a "code free" license, I expect eventually to read that someone has proposed that literacy be eliminated as a requirement for a license, as this may be preventing many prospective hams from getting on the air. Amateur radio does not need anyone who is too lazy (or too stupid) to meet a ridiculously low code requirement of five words per minute.

I hope that the EIA will have something constructive to offer to amateur radio, but in the meantime, I must view their motives with a great deal of suspicion. Their ultimate purpose is, obviously, to make money. Now I am all in favor of this, but at the same time, I sincerely believe that amateur radio would be a lot healthier if it were less commercialized.

I would like to offer my own "radical proposal". Only homebrew equipment should be allowed on the amateur bands!

Robert V. McGraw, W2LYH  
Riverhead, New York

## Assistance, Please

Dear Dick:

I have been a ham radio operator for eight years, holding a General license, and a U.S. Navy Radioman for the last five and a half years. Most of the last five years have been spent in the Far East, with very little time to devote to amateur radio.

Now I am stationed at Naval Communications Station, Japan on shore duty for three years, and I would like to, once again, become active in amateur radio.

There are several military clubs in the area, but my recent experience with the club on Yokosuka Naval Base has been anything but satisfactory.

I would sincerely appreciate any information you or your readers could give me on obtaining a license from the Japanese Government and/or information concerning Japanese Radio Clubs where I could meet some of the Japanese Amateurs in my local area.

My local address is: David E. Schmaus, 1-24 Mabori-Cho, Yokosuka, Kanagaw-Ken, Japan. My Military address is: Box 67, FPO San Francisco 96662.

Any help you could give me would be sincerely appreciated.

David E. Schmaus, K9ZXI/JA  
Yokosuka, Japan

With all those JA readers on the *CQ* subscription rolls, Dave should have little trouble meeting the locals.—*Ed.*

## \$30 Mobile Power

Editor, *CQ*:

A recent article in the February 1968 *CQ* entitled "A Mobile Power Supply for \$30" tells how a 175

watt Heath MP-10 Marine Power Converter can be used in adapting a.c. transceivers for mobile use. Basically the article itself is quite good, but I must disagree with a casual comment made at the bottom of page 65, "By the way, if you need more power, two or more converters may be hooked in parallel".

It is next to impossible without the use of highly sophisticated external circuitry to keep these two converters properly synchronized. If they are not, there will be huge quantities of circulating current flowing between the converters resulting in burning out either one or both of the converters if they are not properly protected. If they are, the protection circuitry will trip immediately, preventing any output power.

Because of this I would highly advise your readers against such a procedure.

Lou Schornack, KØQAZ  
Los Angeles, California

## Lazier—Yet Mobile Protection

Editor, *CQ*:

I have just read with interest the article "The Lazy Man's Mobile Protector", by David J. Goodman in May *CQ*.

Other readers may be interested in knowing that anti-theft door lock knobs are on the commercial market for those not having the time or inclination to make their own.

One such source is the Warshawsky Co., 1900-24 South State Street, Chicago, Illinois 60616. Their catalog No. 313 lists these devices on pages 3 and 46.

M. A. Ellis, K1ORV  
Sudbury, Mass.

Man, that's laziness!—*Ed.*

## Navy MARS

Editor, *CQ*:

Navy MARS, for the information of possible applicants, has more member stations in this area than can be used, except for two meter stations. I think it would be advisable for any amateur who wishes to get into traffic handling to investigate all MARS branches first. Otherwise, he may find he has nothing to do.

I have been a member of Navy MARS since February, 1967 and have never been assigned to a net or even used my call sign. I joined only because I had late model equipment, full legal power and thought there was a need for stations to move what must be a great deal of traffic. After repeated requests to be assigned to a net, I was informed that Navy MARS had all the stations they could use except for two meter stations. The amateurs who are in the nets are evidently doing a very efficient and commendable job, and deserve a rousing vote of thanks. I hope the other branches of MARS are doing as well, and I am sure they are.

C. R. Ferguson, WB6DUC  
Half Moon Bay, Calif.

# Some comments from warranty cards by owners of

## DRAKE TR-4 SIDEBAND TRANSCEIVERS



"The TR-4 is the best rig I have ever known to be made. Glad to own one."

Dan Tangorra, WA7FWH  
Tacoma, Wash.

"Finally got what I wanted!"

Ronald E. Lyons, WB2BQX  
Oakhurst, N. J.

"A superb piece of equipment, no comments necessary."

C. G. Noakes, G3UHR/V02  
Labrador City, Newfoundland

"Great rig—First contact was an ON5 in Belgium."

Bill Busse, WA9TUM  
Mt. Prospect, Ill.

"Best gear I have had the pleasure of working with. Receiver is exceptionally sharp and stable."

Albert V. Mitchell, WA9BUP  
Jeffersonville, Ind.

"Nothing to comment, except that my TR-4 is a real jewel, and I am very satisfied with it. I would like to receive the catalogue of your products."

Joe Braz Ribeiro, PY4UK  
Monte Carmelo (MG) Brazil

"A very F.B. piece of equipment. Audio very nice, especially on SSB, which is rare."

Thomas F. Totten, Jr. WB2GZR  
Saratoga Springs, N. Y.



"Running it with a Mosley "Classic" beam and proves a most fine and nice transceiver. Really proud of it."

Orlando Escudero O., CE-3-OE  
Santiago, Chile

"Looks good—sounds good—very well pleased with performance."

Wayne M. Sorenson, WA0ETL  
St. Paul, Minn.

"Have had Drake 2-B for three years. Knew that TR-4 was same Good Stuff."

Charles E. Bishop, WA8FTT  
Columbus, Ohio

"Just what I always wanted."

Daniel N. Hamilton, WA4WXQ  
Ashland, Va.

"Why not build a good 6 Meter SSB & AM Transceiver . . . hurry up, I'm waiting."

Harold A. Zick, WA9IPZ  
Creve Coeur, Ill.

"Excellent equipment."

W. T. Newell, WB6UZU  
Palm Springs, Calif.

"O.K. 100 x 100. RV-4: O.K./W-4: O.K./L-4: O.K. Very Good!"

Francisco Fau Campmany, TI-2-FAU  
San Jose de Costa Rica

"A beautiful piece of equipment. My second piece of Drake. The first was a 2-B and this sold one friend an R-4 receiver and another a TR-4. We are Drake-minded here in town. Many thanks."

Charles E. Boschen Jr., WA4WXR  
Ashland, Va.

"I'm sure this, like the other Drake equipment I have, is the finest money can buy. YOU MAY QUOTE ME ON THAT."

C. E. (Ed) Duncan, WA4BRU  
Greenville, S. C.

"I'm a real happy man with it. Does a real good job of getting thru."

Jerome D. Lasher, W2RHL  
Hamburg, N. Y.

"Replaces my TR-3."

D. G. Reekie, VE 6 AFS  
Calgary Alberta Canada

"Finest performing gear I have ever had the pleasure of operating."

Milton C. Carter, W2TRF  
Lakewood, N. J.

"PS Several months have passed . . . I now employ TR-4 as mobile unit and base station. I have logged more than 1000 contacts, many being rare DX. I am looking forward to owning a second unit to be used strictly for mobile. To date TR-4 has been trouble-free."

Milton C. Carter, W2TRF  
Lakewood, N. J.

"Well pleased."

Rev. James Mohn, W3CKD  
Lititz, Pa.

"I am delighted with Drake gear. This is the second of your transceivers for me. I have used a TR-3 in my car for about 2½ years—only trouble: replacing a fuse!"

Guy N. Woods, WA4KCN  
Memphis, Tenn.

**"Ask the ham who owns a Drake TR-4"**

... or write for details ...

Dept. 258 **R. L. DRAKE COMPANY** 540 Richard St., Miamisburg, Ohio 45342

See page 118 for New Reader Service

July, 1968 • CQ • 9

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# Announcements

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## London, England

An unusual feature of the 1968 City of London Festival, July 8th-20th, will be the amateur radio station installed and operated by the Radio Society of Great Britain. The G.P.O. has granted the use of the callsign, GB2LO. Equipment will be loaned by K. W. Electronics and will be operated by volunteers on the 10, 15, 20, 40 and 80 meter bands. Operation will be on single sideband only.

## Conconully, Wisconsin

The Okanogan Valley International Hamfest will be held on July 27 and 28 at the Conconully State Park, Conconully, Wisc. Registration for hams is \$1.50 and a piece of junk; XYL's \$1.00. For further information contact Harlan R. Tverber, WA7DFP, P.O. Box 1420, Omak, Wash. 98841.

## Evansville, Indiana

The Tri-State Amateur Radio Society's Twenty-first Annual Hamfest will be held July 21, 1968, at the 4-H Center on North 41 Highway. Advance registration \$1.50 and \$2.00 at the door. For details contact Jack Young, K9LAU, P.O. Box 492, Evansville, Indiana.

## Chatham, Illinois

The Quad-Co. Amateur Radio Club will sponsor the 11th Annual Hamfest of the Breakfast Club on July 20 and 21 at Terry Park. All other groups are invited, giving prior notice to the hamfest committee. Mobile talk-in on 3873 kc from noon Saturday until 11:00 A.M. Sunday.

Pre-registration until July 7th is \$1.00; \$1.50 at the gate. Write "Hamfest" c/o Quad-Co. ARC, Inc., Box 323, Chatham, Illinois 62629.

## Oak Ridge, Tennessee

The Oak Ridge Radio Operator's Club will sponsor the 18th Annual Crossville Picnic at Cumberland Mountain State Park July 20 and 21. For information, write The Oak Ridge Radio Operator's Club, Inc., P.O. Box 291, Oak Ridge, Tennessee 37830.

## Terre Haute, Indiana

The Wabash Valley ARA will hold its 20th Annual VHF Picnic on Sunday, July 28, 1968, at Turkey Run State Park. One dollar registration charge at the gate only. Mobile check-in on 52.525 mc.

## Navajo Celebration

To help the Navajo Indian people of Arizona and New Mexico celebrate the centennial of the signing of the treaty with the United States government and their consequent long walk back to their homeland from Ft. Sumner, K7NCR will be on the air from the site of several of the centennial celebrations. From July 4 to July 6 and again from August 30 to September 2. K7NCR will be located at Window Rock, Arizona, the capital of Navajoland. A special QSL card printed by the Navajo Tribal Printing Department will be sent to all stations contacted.

## New Orleans, Louisiana

In commemoration of the celebration of the 250th anniversary of the founding of the City of New Orleans in 1718 by Jean Baptiste Le Moyne, Sieur de Bienville, the Greater New Orleans Amateur Radio Club is offering a Commemorative Certificate to any amateur who submits a log extract indicating two-way communication on any bands, in any mode, with three Metropolitan New Orleans Area amateurs during 1968. With the log, send a s.a.s.e. to the Greater New Orleans ARC, 2935 International Trade Mart Tower, 2 Canal Street, New Orleans, La. 70130.

## West Paterson, N.J.

The Knight Raiders VHF Club will hold its Second Annual Hamfest on Saturday, July 20, 1968 at Weasel Drift Picnic Grove, West Paterson, N.J. from 10 A.M. until dark. Picnic tables and barbecue pits are available. No tickets, no fee. Refreshments available. Talk in station K2DEL/2 will operate on 50.4 mc and 146.898 mc. Special certificate for contacting the talk in station available. Many door prizes.

## Henderson, Kentucky

The annual Hamfest of the Henderson Amateur Radio Club will be held on Sunday, July 28, 1968, rain or shine, at the Audubon Raceway. For more information, contact WA4WTE, Box 83, Henderson, Kentucky 42420.

## Phoenix, Arizona

The Amateur Radio Council of Arizona will sponsor a Hamfest in Flagstaff, Arizona on July 26, 27, and 28. The Hamfest will be held at Fort Tuthill in Coconino County Fairgrounds. There will be talk in stations for mobiles on 3878 kc and 50.34 mc. For further information write to the Amateur Radio Council of Arizona, P.O. Box 6602, Phoenix, Arizona 85005.

## Paducah, Kentucky

The Paducah ARC will hold their Annual Ham Picnic at the Noble Park Community Center, Paducah, Kentucky, on July 14th. Lunch will be served. Bring along your swap material and equipment. For further information contact Don Fuller, WA4LME, 247 Seminole Drive, Paducah, Ky. 42001.

## Fond Du Lac, Wisconsin

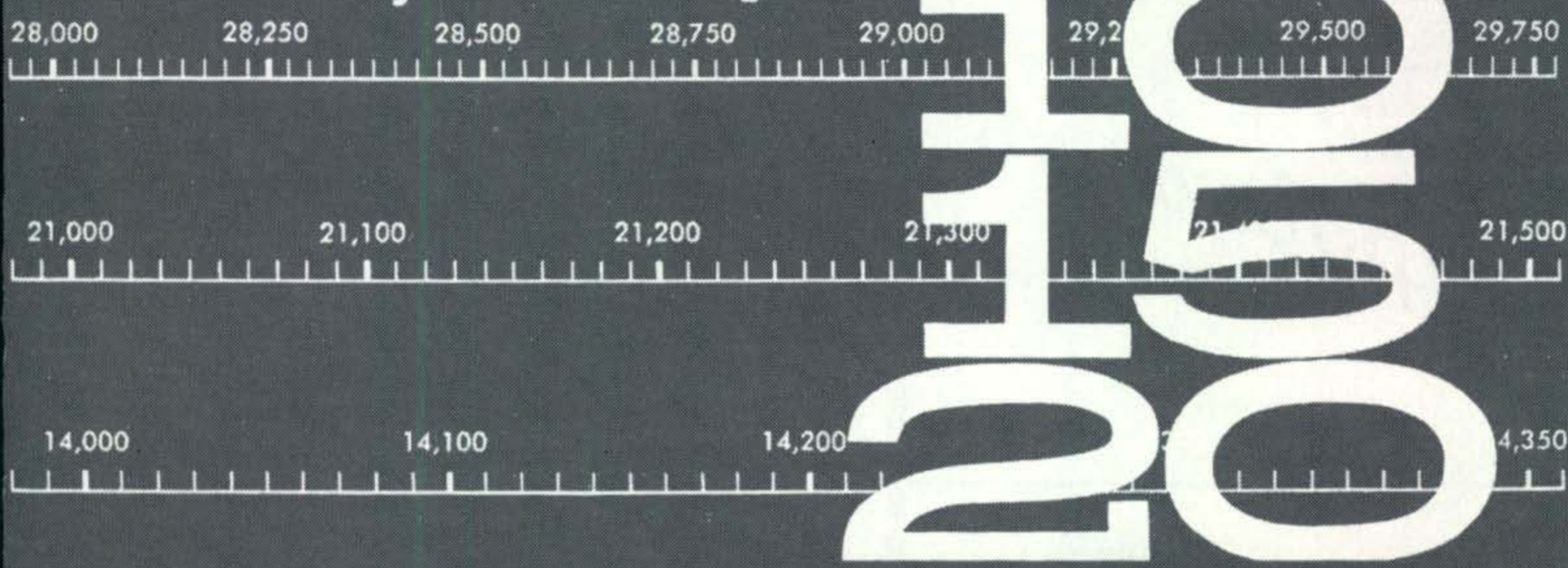
The 1968 Wisconsin Nets Association Picnic will be held July 14 at Fond Du Lac, Wisconsin in Lakeside Park. For further information contact K9GSC, Kenneth A. Ebner, 822 Wauona Trail, Portage, Wisconsin 53901, or ask on any of the Wisconsin nets.

## Greenville, Pennsylvania

A Novice Worked All States Net is being formed. The net will meet on 7.170 mc with an auxiliary frequency of 7.179 mc. Registration forms and more information can be obtained from either WN2EKW, 260 Ellen Drive, Buffalo, New York or WA3JDT, 4 Homer Street, Greenville, Pennsylvania.

# NEW | Cubical Quads

by *Mosley*



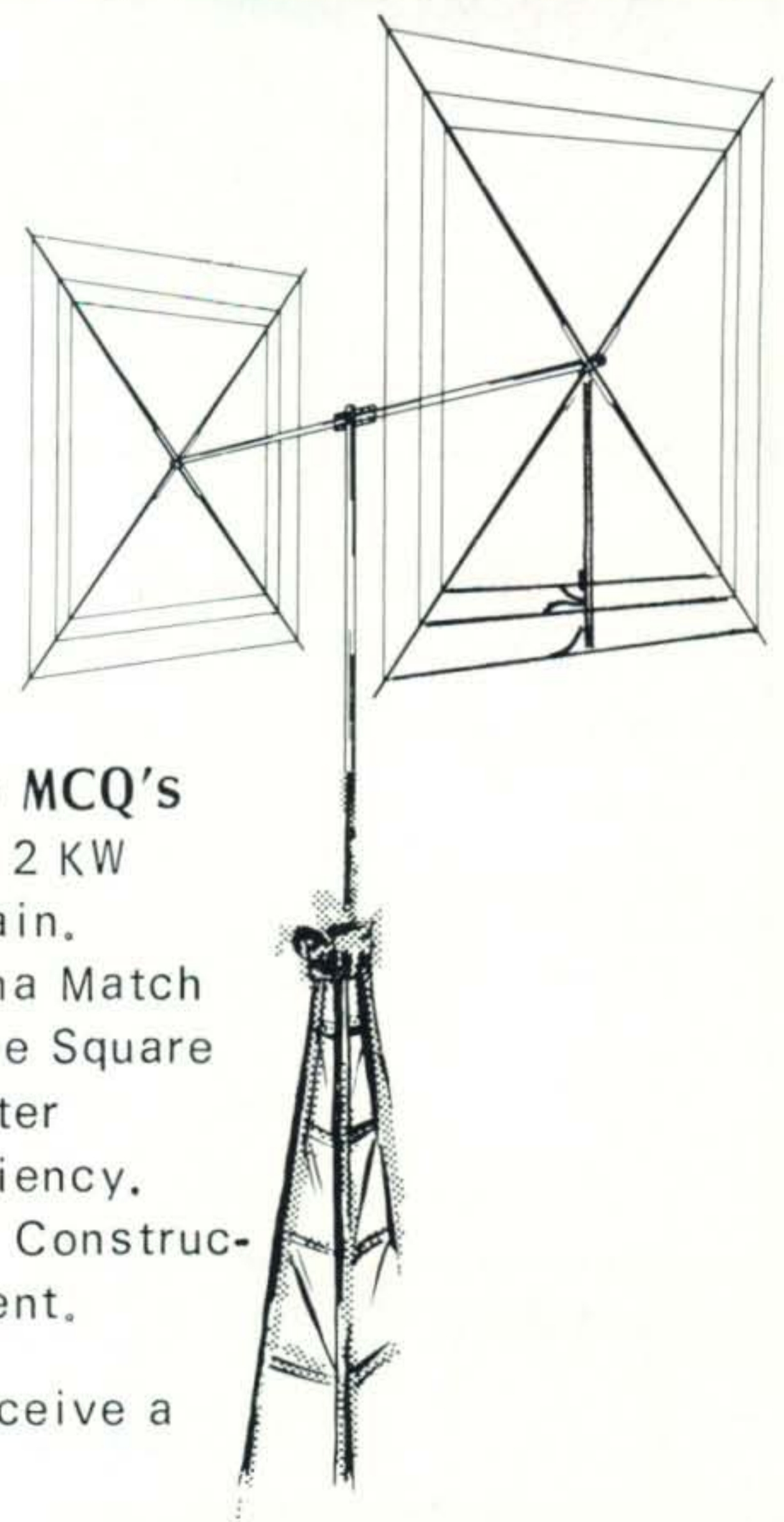
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# SCRATCHI

Feenix, Ariz.

Dear Hon. Ed:

By gollies, there ought to be a law against what sum peeples doing on the air these days—it's outrageous, that's what it is. I so disgusted with things I riting you because thinking you can do something about it.

So, hon. Ed., please taking your feets off your Hon. Desk and paying attenshun. I'm surely you wanting to rite red-hots editorial on subject before next issue of your Hon. Mag getting pressed.

Yestiday being Sunday, Hon. Brother Itchi desiding it be nice to take ride around country-side and do a little exploring of back roads. Even have XYL-to-be, Lil, pack picnic lunch for the two of us.

So, we hedding into foothills, and having pleasant morning in Hon. Jeep. Come middle of day we picking shady spot under cupple clumps of cactus and disposing of Lil's lunch, along with cupple cups of ice-cold cactus jooce.

Taking off again after lunch, and cupple hours later sky getting black, and hevvin are opening up with granddaddy of cloudbursts. If you knowing Arizona, you knowing person doesn't keep driving on back roads in cloudburst. Every dip in road getting six feets of water in it.

So, we pulling over, and Itchi suggests we have QSO on car rig to passing time until storm being over and it safe to driving again. I turning on rig and sending out snappy two minute seek-you, and feller coming rite back.

Big surprise—he Indian feller on nearby reservayshun, he telling us. Handle is Talking Bull. We exchanging signal reports, then I telling him we in middle of 1/c desert down-pour.

He coming back and saying maybe he can fixing it for us, on acct. He knowing peechy Indian chant to stopping rain. Kinda like Indian rain dance, only no dancing—he just saying words backwards. Hon. Brother Itchi getting on mike, and laffingly telling Talking

# Important E & E Books

Bull he being big kidder. Homsumever, Talking Bull saying he not kidding, and he going to prove it. He asks us exactly where we are so we telling him our exact locayshun.

Next transmission Talking Bull coming on and beginning this kind of Indian chant. Reel gibberish it sounding like, Hon. Ed. Then he saying he giving countdown, and when he gets to zero, rain stopping. He starting: Twenny, nineteen, ate-teen, and so on down to three, two, one . . . and zero.

Hokendoke Hackensaki!! Just when he saying "zero", rain letting up, and in time it takes gopher to disappear in his hole, rain are stopped!! Well, both Itchi and Scratchi mighty impressed, I telling you!

We go back on air to tell him it working, and asking him more about rain-stopping chant, but he just saying something about maybe next time we not laffing at old Indian lore, and he signing off.

As we riding back to ranch, Itchi saying maybe there are something to this Indian legend, and he wanting to find out more about Talking Bull. So, when getting home, I looking up call-letters in Hon. Callbook.

Sure enough, feller are having QTH on Indian reservayshun, only name listed are not Talking Bull, but maybe he listing his American name. Funny thing, though. He Hon. Master Sgt. in U.S. Air Force!

When Itchi heering this, he saying he having friend in Air Force, so he getting on land-line and calling him. He first asking cupple questshuns, then he laffing like furies. He explaining to friend what happening, then he laffing lots more.

After he hanging up, he still laffing, but he finely telling me what happening. It seeming this feller are 1/c honest-to-gracious Indian, but he also in charge of U.S. Air Force weather radar stayshun. It covering hole state of Arizona, and with this radar he can seeing where rain is falling anyplace in state.

So, when he QSO'ing us, he can see rain are about to quit, so he giving us olf phoney Indian chant just as rain-storm as shown on radar are leeving us.

I telling you—I pretty incensed about hole thing, and I explaining to Itchi amchoors not supposed to doing things like that. Homsumever, Itchi having last word, as usual.

He saying with handle like Talking Bull, how I expecting to get strate story. How do you answer that? I leeving hole thing in your lap!

Respectively yours,  
Hashafisti Scratchi

## Amateur Radio Incentive Licensing Study Guide



by Robert M. Brown, K2ZSQ/W9HBF, and Tom Kneitel, K2AES. Fully explains the new incentive licensing which affects both newcomers and old-timers. Covers all the new FCC Regulations and band allocations.

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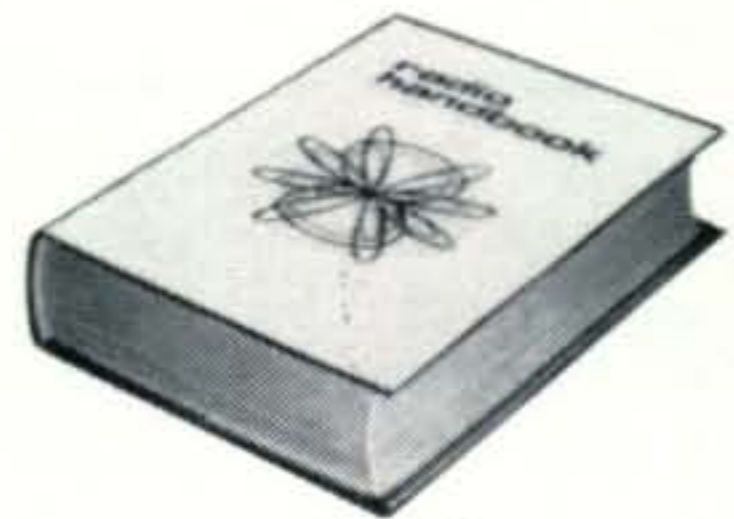
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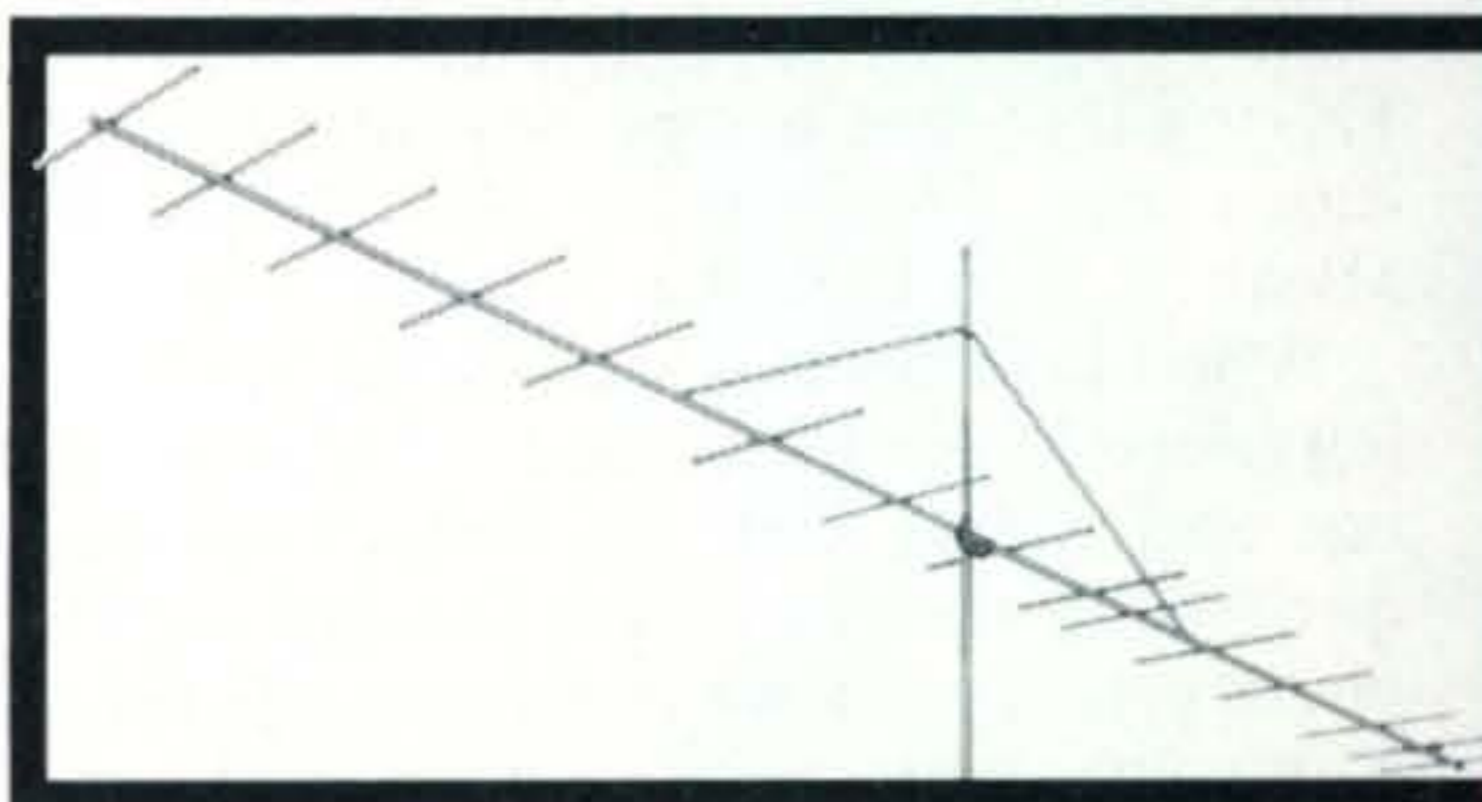
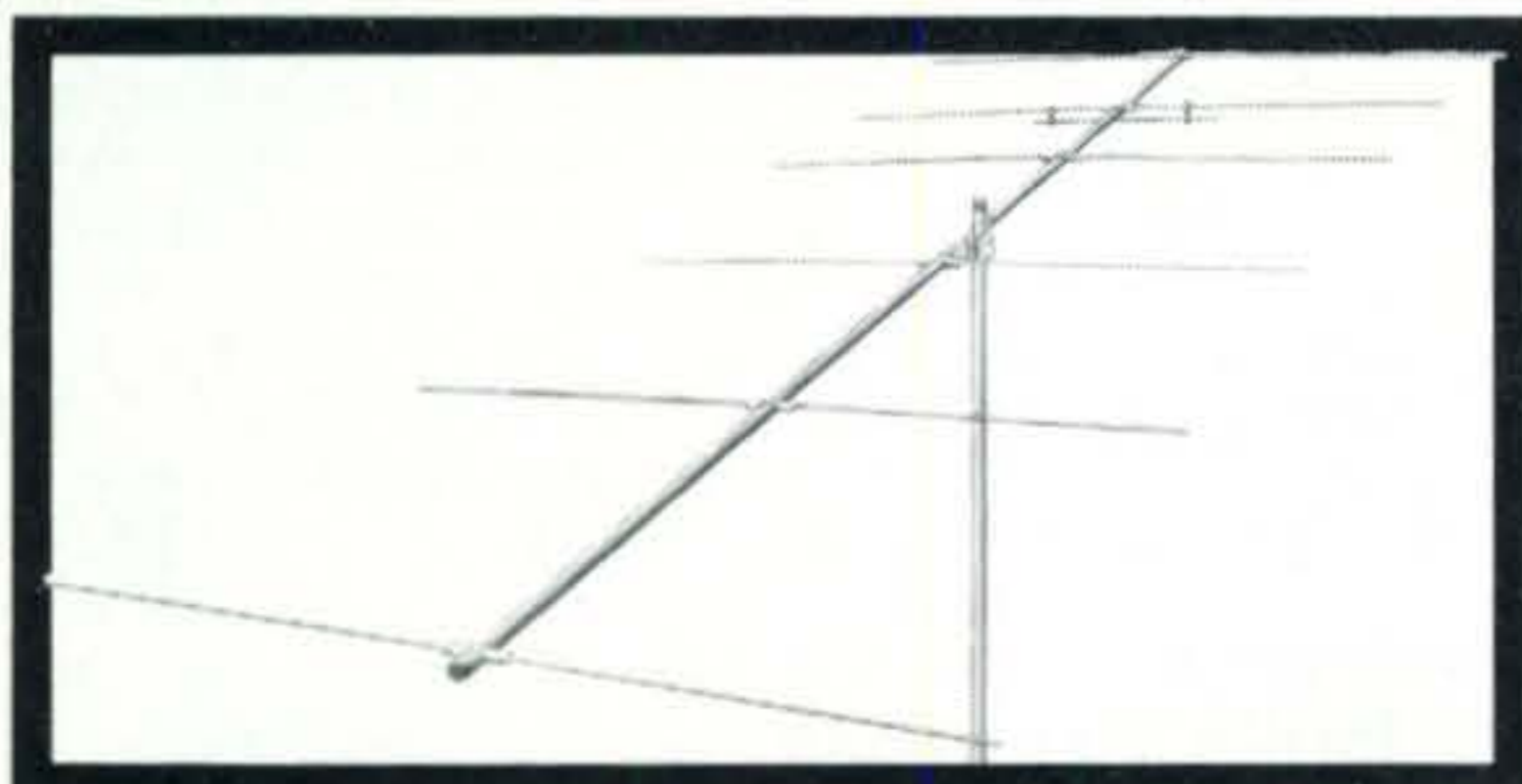
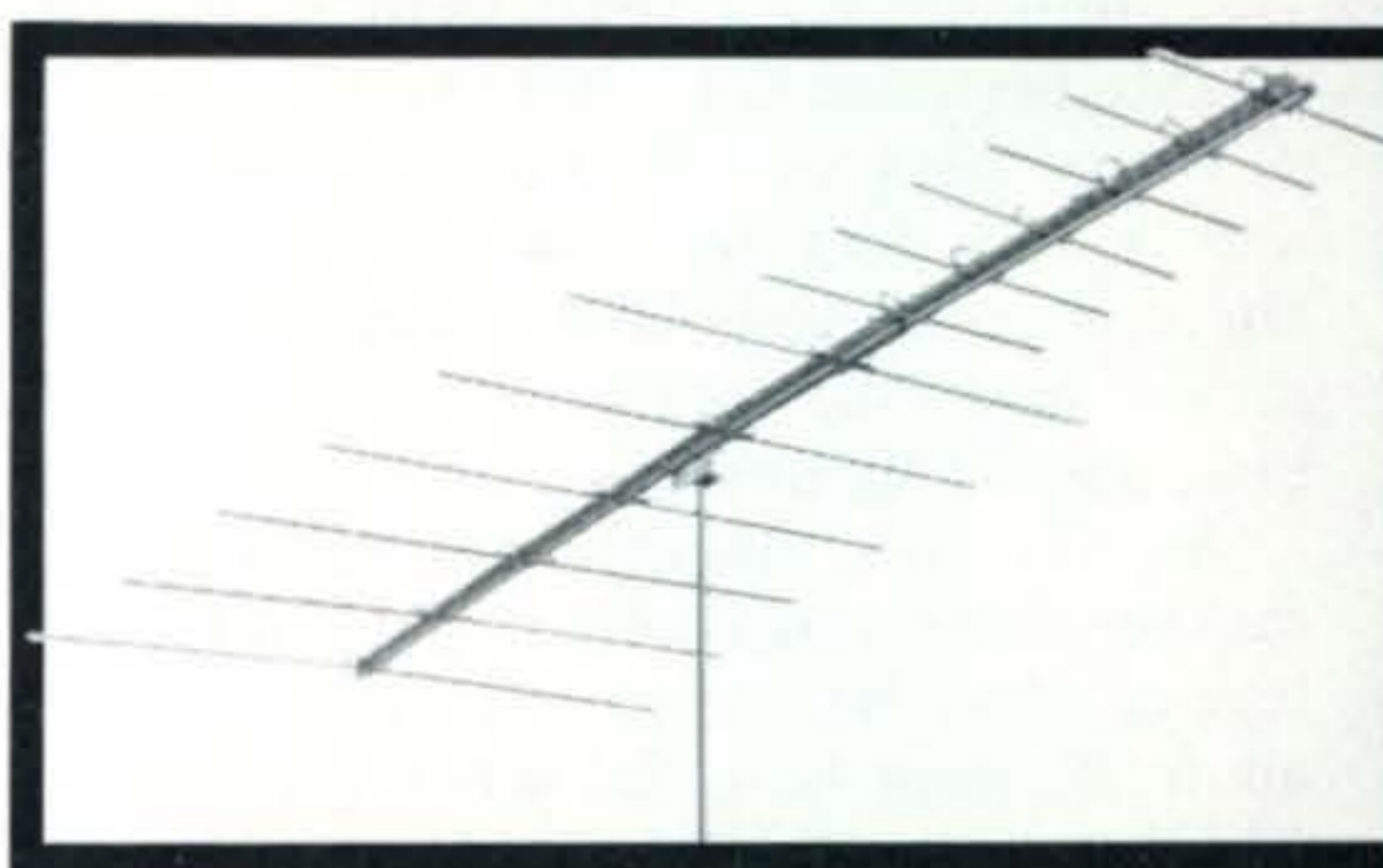
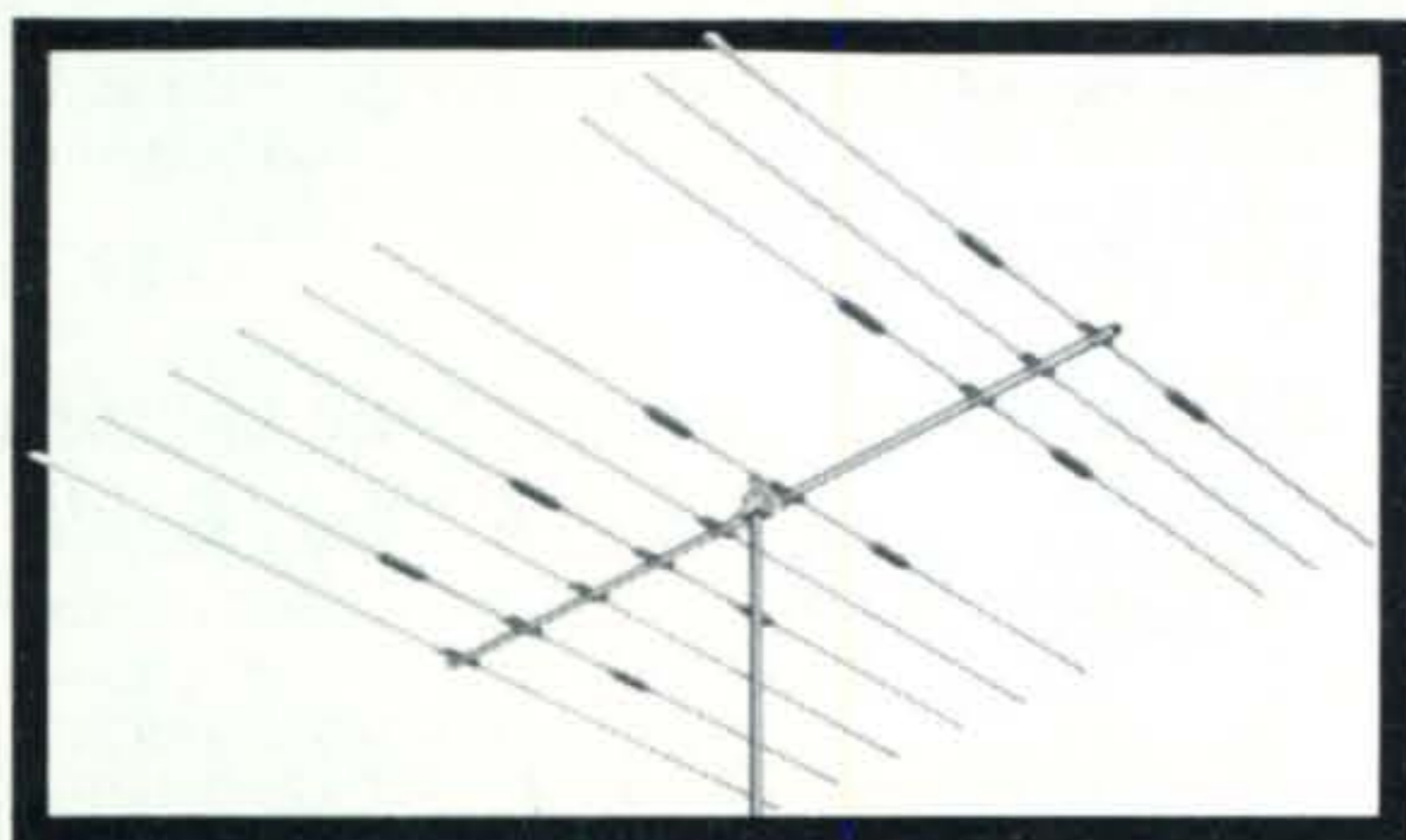
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Model	Elements	db Gain	F/B Ratio	Boom Length	Turn Radius
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64B	4	12.7	20-25db	12'	8'
66B	6	15	20-25db	24'	12'6"
611B	11	19	20-25db	47'	24'2"

Model	Elements	db Gain	F/B Ratio	Boom Length	Turn Radius
23	3	9	20	3'	4'
28	8	14.5	25-30	14'	7'6"
215	15	17.8	20-30	28'	14'

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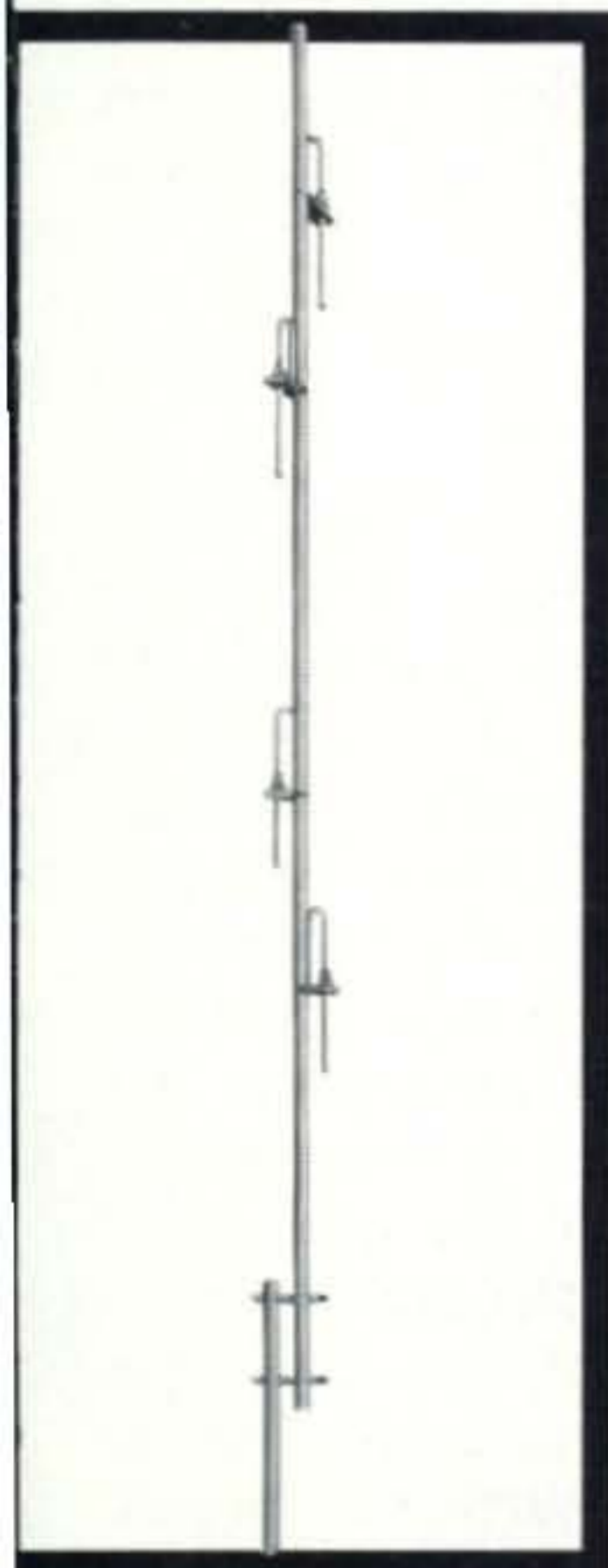
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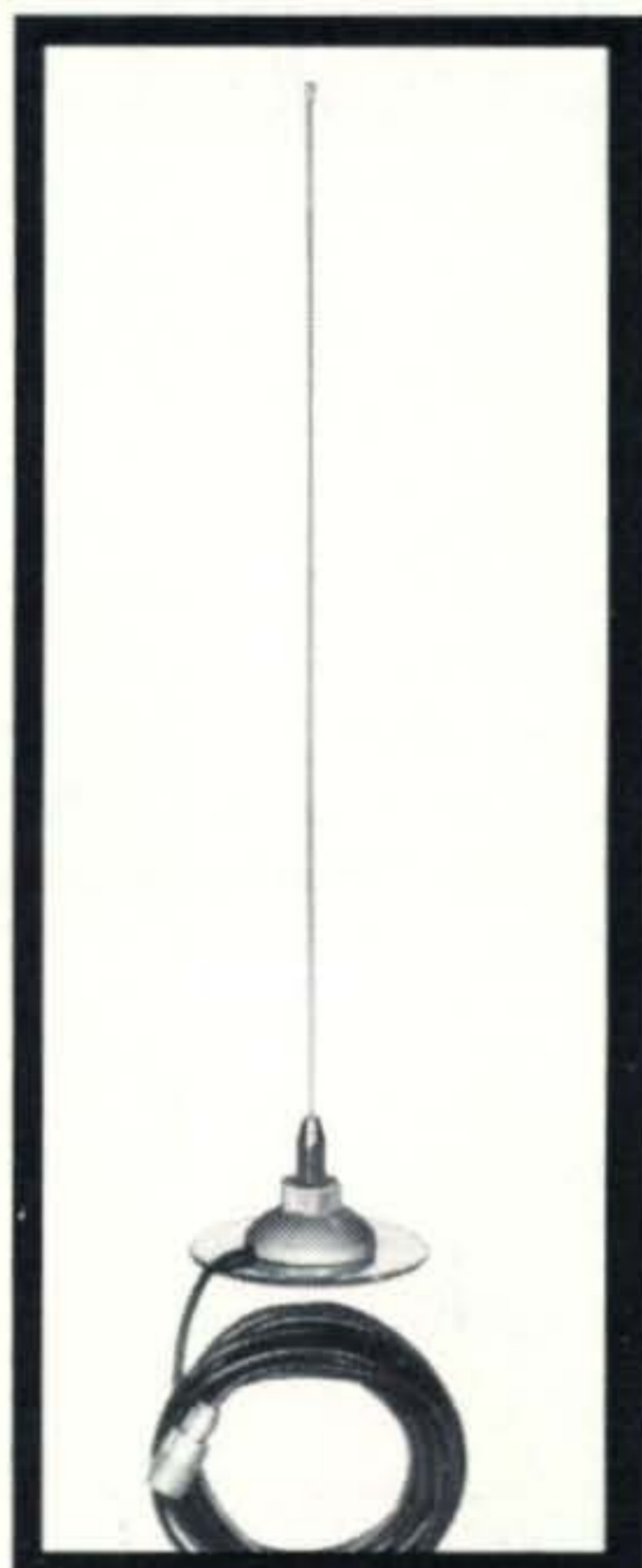
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# MODULATION UNLIMITED

## Part I

BY FREDERIC C. DOUGHTY, \*W3PHL

This two part series covers the principles and circuit techniques necessary to exceed 100% modulation without the production of undesirable side effects such as distortion and splatter. The modified final power amplifier circuit can be used for c.w., conventional a.m., d.s.b., and d.s.r.c. (double sideband reduced carrier).

**T**HIS article, in part, is a review of a circuit which was described by O. G. Villard, W6QYT, in 1947<sup>1</sup>. At that time the circuit was proposed as a modification of an existing a.m. transmitter. The modification permits the use of audio power in excess of the amount necessary for 100% modulation. The litera-

\* P.O. Box 157, Valley Forge, Pennsylvania 19481.

<sup>1</sup> Villard, O. G., "Overmodulation Splatter Suppression," *QST*, June 1947, p. 13.

ture has been well supplied for many years with ideas aimed toward this goal but the unique feature of the scheme advanced by Villard is that it alone offers a communications improvement with *no undesirable side effects*.

It is required by government regulation that a transmitter shall not be modulated beyond its capability. The modulation capability of a transmitter is determined as the modulation percentage above which the modulated circuit does not reproduce the audio modulating waveform in the output r.f. envelope. Numerous factors combine to determine the modulation capability of a particular circuit. In general, for a properly designed plate-modulated Class C r.f. amplifier, the modulation capability is considered to be limited by the negative peak of modulation. Negative peak modulation in excess of 100% of a conventional plate modulated amplifier is improper in that the unidirectional vacuum tube cannot linearly respond during the period of time that the plate voltage is negative.

### Increase Of Modulating Power

It is common practice to separate the circuits which are proposed to increase of modulation power of an a.m. transmitter into low level and high level groups. The low level group includes, in part, clippers, compressors and limiters. These devices are designed to improve the average modulation power either by shaping or by variable amplification of the audio waveforms. The high level group includes such circuits as negative peak clippers, loaders, and attenuators. These circuits are

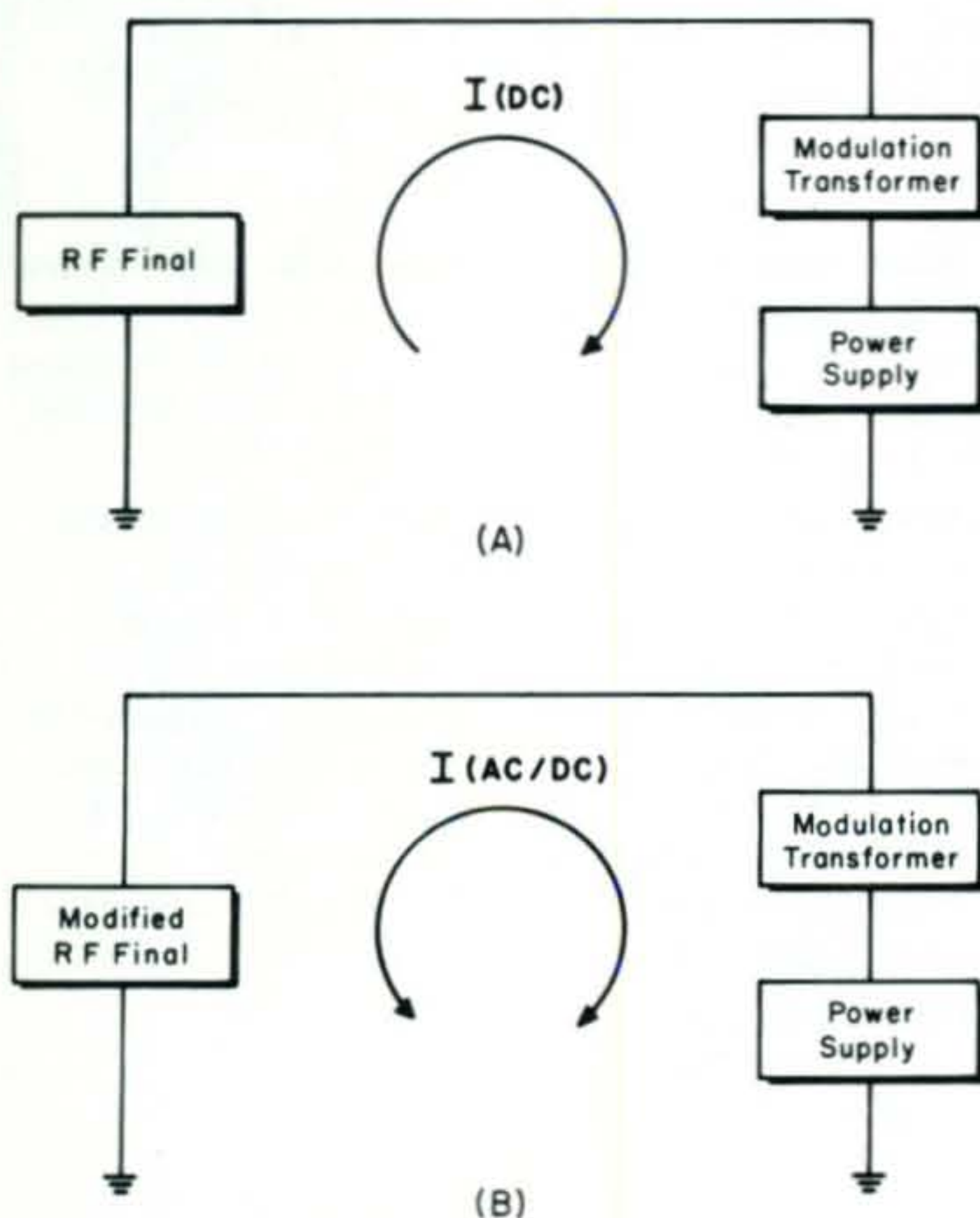


Fig. 1 (A)—D.c. current flow path in a plate modulated r.f. power amplifier. With modifications the same circuit can have an a.c. path as shown in (B).

used to limit or control negative peaks of modulation to 100%, permitting positive peaks to extend beyond 100%. There are radio transmitters with circuits of one or both groups in use in all of the radio services.

Each of the above mentioned circuits, in its own way, offers an improvement in communications capability. The low-level circuits deform the original audio waveforms in some fashion. The high level circuits alter the symmetry of the a.c. modulating voltage. All of the circuits are based on intentional distortion of the original audio waveform and create undesirable side effects. This is because each one is predicated on the use of an r.f. final amplifier which is limited to 100% modulation on negative peaks.

### The Final R.F. Amplifier

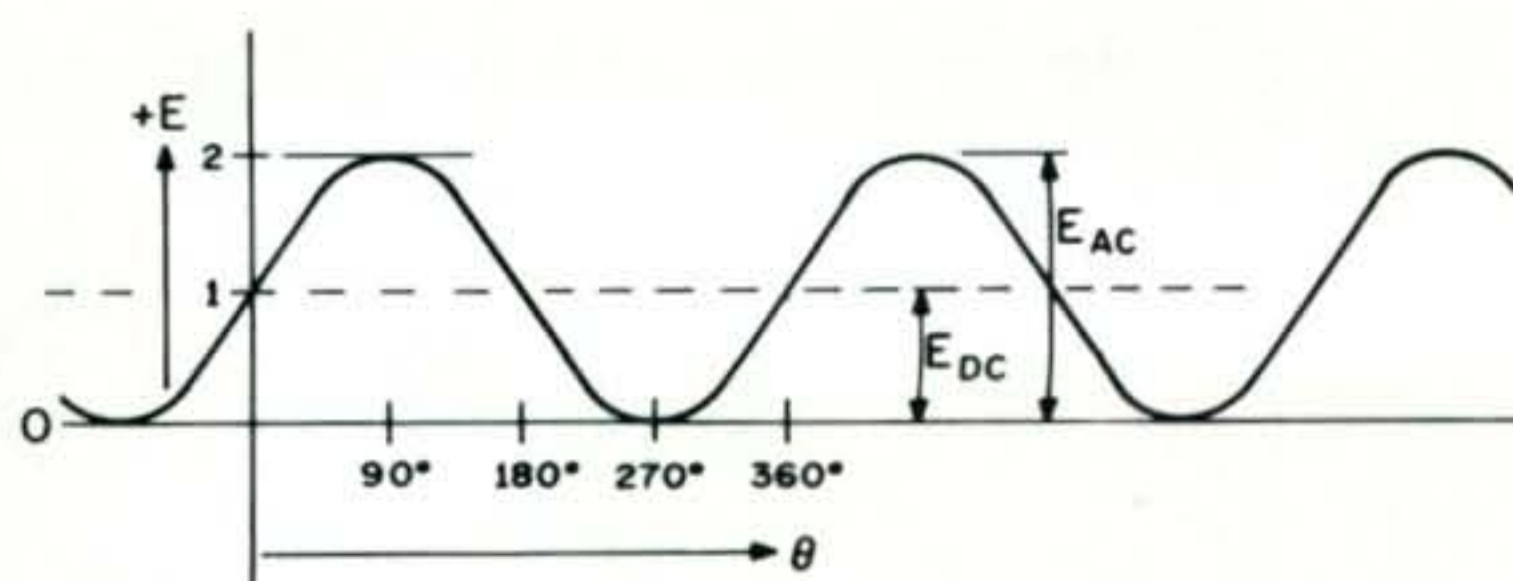
A d.c. circuit, such as a vacuum tube circuit, is one in which current is unidirectional and may vary in amplitude. An a.c. circuit is one which permits only a.c. current which also may vary in amplitude. An a.c.-d.c. circuit responds as well as both of the above circuits when subjected to the conditions pertinent to each and also to combinations of these conditions.

A conventional, properly operated, plate modulated r.f. amplifier is a d.c. circuit in which the plate current flows in one direction, in an uninterrupted continuous loop. The sequence is from ground, to r.f. final, to modulation transformer, to power supply and to ground as shown in fig. 1(A). The modification allows the same sequence and loop, and also the reverse sequence, *i.e.*, ground, to power supply, to modulation transformer, to r.f. final, to ground, as shown in fig. 1(B).

A modified transmitter may be used to generate a conventional a.m. envelope, where the carrier power is equal to two times the audio modulating power (d.c. mode); a d.s.r.c. envelope (double-sideband reduced carrier), where the carrier power is less than two times the audio modulating power (a.c.-d.c. mode), or a d.s.b. envelope wherein there is no carrier power (a.c. mode).

### Improper Negative Peak Modulation

Modulation of the plate voltage of a conventional r.f. amplifier is, in part, restricted by the unidirectional operation of a vacuum tube. If the d.c. plate voltage is modulated in excess of 100% on negative peaks, the current load, which should respond to the entire modulating waveform, is interrupted during



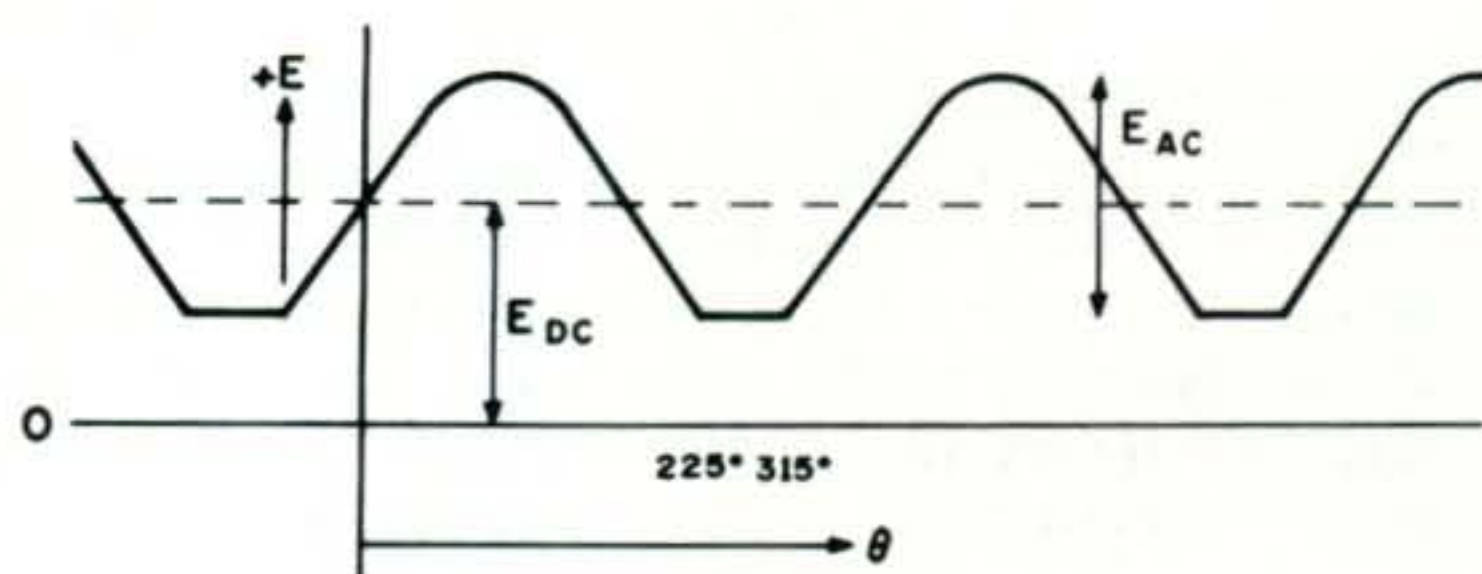
(a)

$\theta$	$0^\circ$	$90^\circ$	$180^\circ$	$270^\circ$	$360^\circ$
Sine $\theta$	0	1	0	-1	0

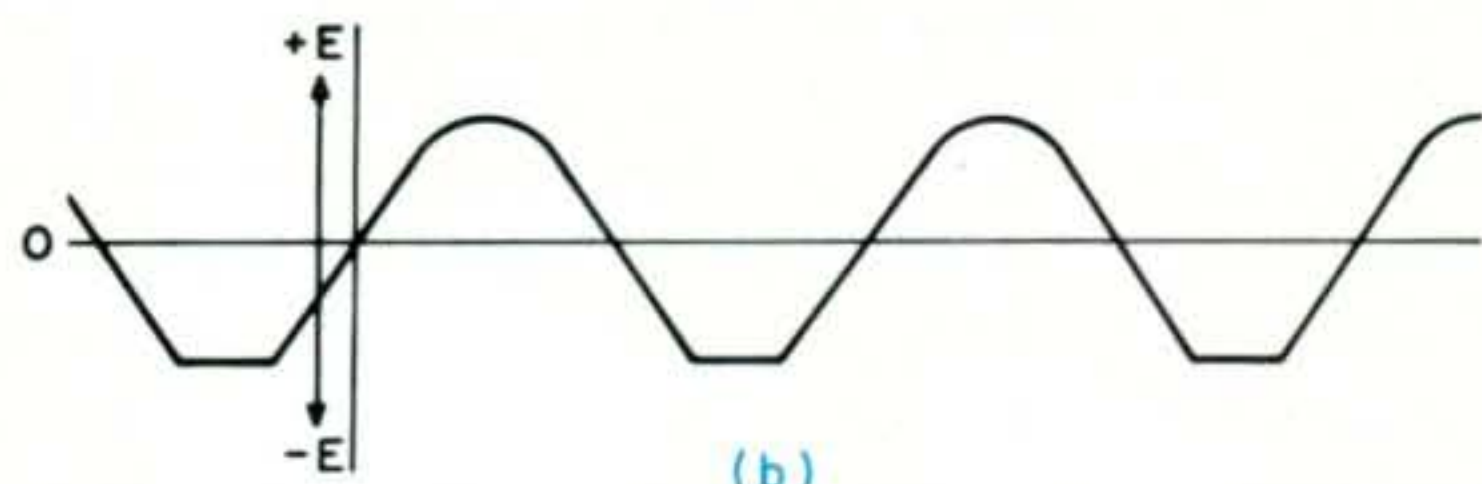
(b)

Fig. 2 (A)—A d.c. voltage modulated 100% by a sine wave. (B) The value of the sine of  $\theta$  at various angles.

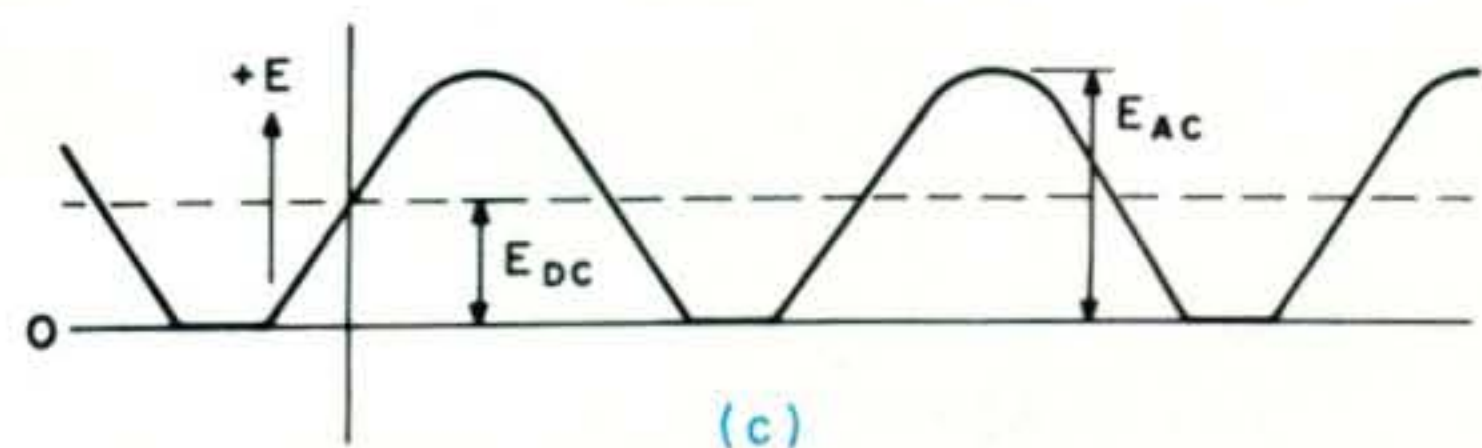
the time that the plate voltage is negative. This interruption is a distortion of the applied audio waveform and the distorted waveform cannot represent a single audio frequency. Only a perfect sine wave shape results from a single frequency. Amplitude alteration of part of a sine waveform generates other frequencies. If the instantaneous amplitudes of these other frequencies and the fundamental, in the proper phase relationship, are added at each instant of time within a cycle of the funda-



(a)



(b)



(c)

Fig. 3 (A)—A d.c. voltage modulated by the distorted wave form shown in (B). When the modulation percentage is increased, as in (C), the d.c. appears to reduce to zero volts from  $225^\circ$  to  $315^\circ$ .

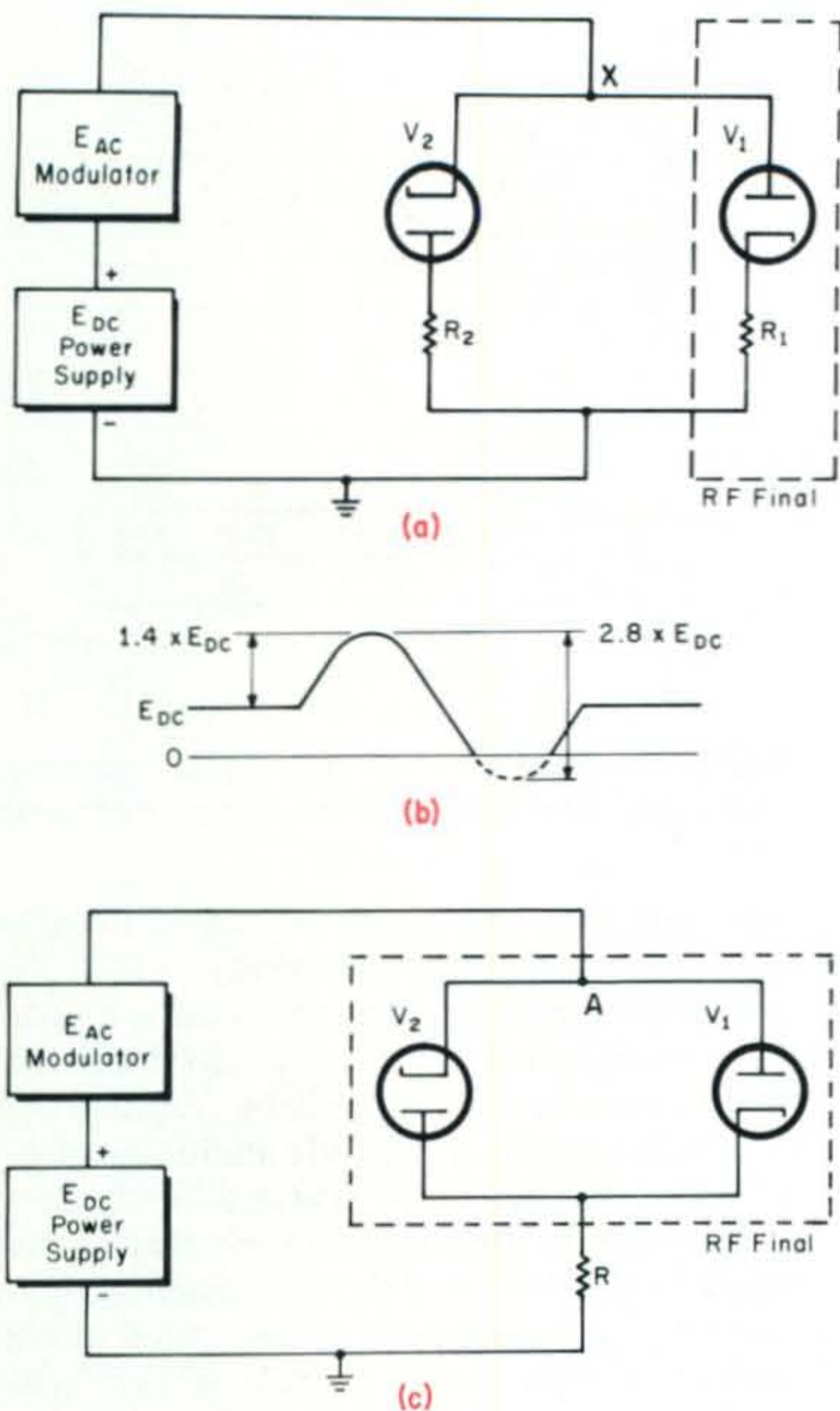


Fig. 4 (A)—Block diagram of a transmitter with an added circuit. (B) Wave form that appears at point in X when  $E_{a.c.}$  is excessive and causes overmodulation. The power dissipated by  $R_2$  is shown by the dotted portion of the sine wave below the zero line. (C) By combining the outputs of  $V_1$  and  $V_2$  in a common load distortion in the output is virtually eliminated.

mental, a single cycle of the distorted waveform results.

Figure 2 shows a d.c. voltage continuously modulated 100% by a single frequency (a sine wave). Examination of a single cycle starts at  $0^\circ$  and terminates at  $360^\circ$ . The value of the sine at several points is also given in fig. 2. It can be seen, that throughout the entire cycle, the voltage at any instant of time is equal to  $V_{d.c.}$  plus  $V_{d.c.}$  times the sine of the angle at the instant of time, or:

$$V_i = V_{d.c.} + V_{d.c.} \text{ sine } \theta$$

The d.c. voltage, fig. 3(A), is modulated with a distorted waveform which is shown in fig. 3(B). In fig. 3(C), the percentage of modulation is increased so that the d.c. voltage *appears* to be reduced to zero during the time period from  $225^\circ$  to  $315^\circ$ . The r.f. envelope

generated by the waveform of fig. 3(C) is identical to the envelope generated by a transmitter which is negative peak overmodulated during the same period. Splatter and bandwidth would cause an a.m. transmitter to *appear* to be overmodulated at *any* percentage if modulated by the audio waveform shown in fig. 3(B). This is because the audio frequencies required to generate the waveform as shown in fig. 3(A) are the same as the frequencies required for the waveform shown in fig. 3(C). Only the amplitudes of the component frequencies are changed. The formula for the waveform in fig. 2 does not apply to the waveforms in fig. 3. The formula for the waveform in fig. 3(C) must change with time or angle.

From 0 degrees to 225 degrees and from 315 degrees to 360 degrees the instantaneous voltage is calculated as indicated earlier:

$$V_i = V_{d.c.} + V_{d.c.} \text{ sine } \theta$$

From 225 degrees to 315 degrees  $V_i$  equals zero. Together, therefore:

$$V_i = \begin{cases} V + V \text{ sine } \theta & 0^\circ \text{ to } 225^\circ \\ 0 & 225^\circ \text{ to } 315^\circ \\ V + V \text{ sine } \theta & 315^\circ \text{ to } 360^\circ \end{cases}$$

It can be seen that the sine wave of a single fundamental frequency is a necessary component of the modulating waveform *and* that the components of other frequencies must be present. The addition of their respective components and the fundamental results in "zero" amplitude between  $225^\circ$  and  $315^\circ$ . These other frequencies are in the original modulating waveform, fig. 3(B), and appear as sideband frequencies in the spectrum about the carrier frequency. These "extra" sidebands are commonly called splatter.

The repeating waveform shown in fig. 3(C) can be broken down, through a Fourier analysis, to indicate what portion of the waveform is in the fundamental, second, third, fourth harmonic, *etc.* This is a complicated computation and will not be discussed here. For the waveforms in fig. 3, the power ratios of the harmonic frequencies are, if  $f_1$  (fundamental) = 100 watts:

$$\begin{aligned} f_2 \text{ (second harmonic)} &= 3.4 \text{ watts} \\ f_3 \text{ (third harmonic)} &= 0.43 \text{ watts} \\ f_4 \text{ (fourth harmonic)} &= 0.1 \text{ watts} \end{aligned}$$

### Modified Circuit

Figure 4(A) represents a transmitter with an *added circuit*. The power supply is shown as  $E_{d.c.}$  and the modulator is shown as  $E_{a.c.}$ . Diode  $V_1$  represents the r.f. final unidirec-

tional vacuum tube and  $R_1$  represents the r.f. plate load of the final. Diode  $V_2$  and  $R_2$  are added to provide the same load ( $R_2 = R_1$ ) during a period of voltage reversal. The d.c. power (carrier) is,

$$P_{d.c.} = E_{d.c.}^2 / R_1$$

When the peak-to-peak audio voltage equals  $2E_{d.c.}$ , the d.c. voltage is 100% modulated, and  $P_{a.c.} = 1/2 P_{d.c.}$ . When the peak-to-peak audio voltage equals  $2.8E_{d.c.}$ ,  $P_{a.c.} = P_{d.c.}$ , and the waveform at  $R_1$  will be overmodulated as shown in fig. 4(B). Note that this is the same as the waveform that is shown in fig. 3. The audio powers dissipated by resistors  $R_1$  and  $R_2$  are in the ratio of the areas of the waveforms impressed on each resistor.

Half of the audio power occurs during the first half cycle and it is dissipated by  $R_1$  alone. The second half cycle audio power is divided between  $R_1$  and  $R_2$  in a ratio determined by comparing the areas of the voltage waveforms impressed on each resistor. For the case shown,  $R_1$  absorbs 84.3% and  $R_2$  absorbs 15.7% of the second half cycle audio power.

For example, assume a condition where a 1000 watt input r.f. carrier is overmodulated by 1000 watts of audio output power, with the diode and resistor circuit added to the transmitter. The audio power to the final is equal to the first half cycle modulator power, 500 watts, plus 84.3% of the second half cycle power which equals 421.5 watts, a total of 921.5 watts. The resistor receives 78.5 watts (15.7% of 500). Without the added circuit, calculations are relatively complex because of the no-load condition on the modulator during periods of negative peak overmodulation. In addition, without the circuit, the modulation transformer will generate extreme voltage excursions during the no-load period, in that the modulator attempts to deliver power to a load of infinite impedance.

Figure 4(B) shows that the waveform which is impressed on the r.f. final *cannot* represent a single frequency. The modulating waveform is the same as the previous case as shown in fig. 3(C). If it is assumed that 921.5 watts is divided between the fundamental and the second, third and fourth harmonics, then:

$$\begin{aligned} P_{f1} + P_{f2} + P_{f3} + P_{f4} &= P_t \\ 100X + 3.4X + .43X + .1X &= 921.5 \\ 103.93X &= 921.5 \\ X &= 8.86 \end{aligned}$$

The powers in the fundamental and harmonics are:

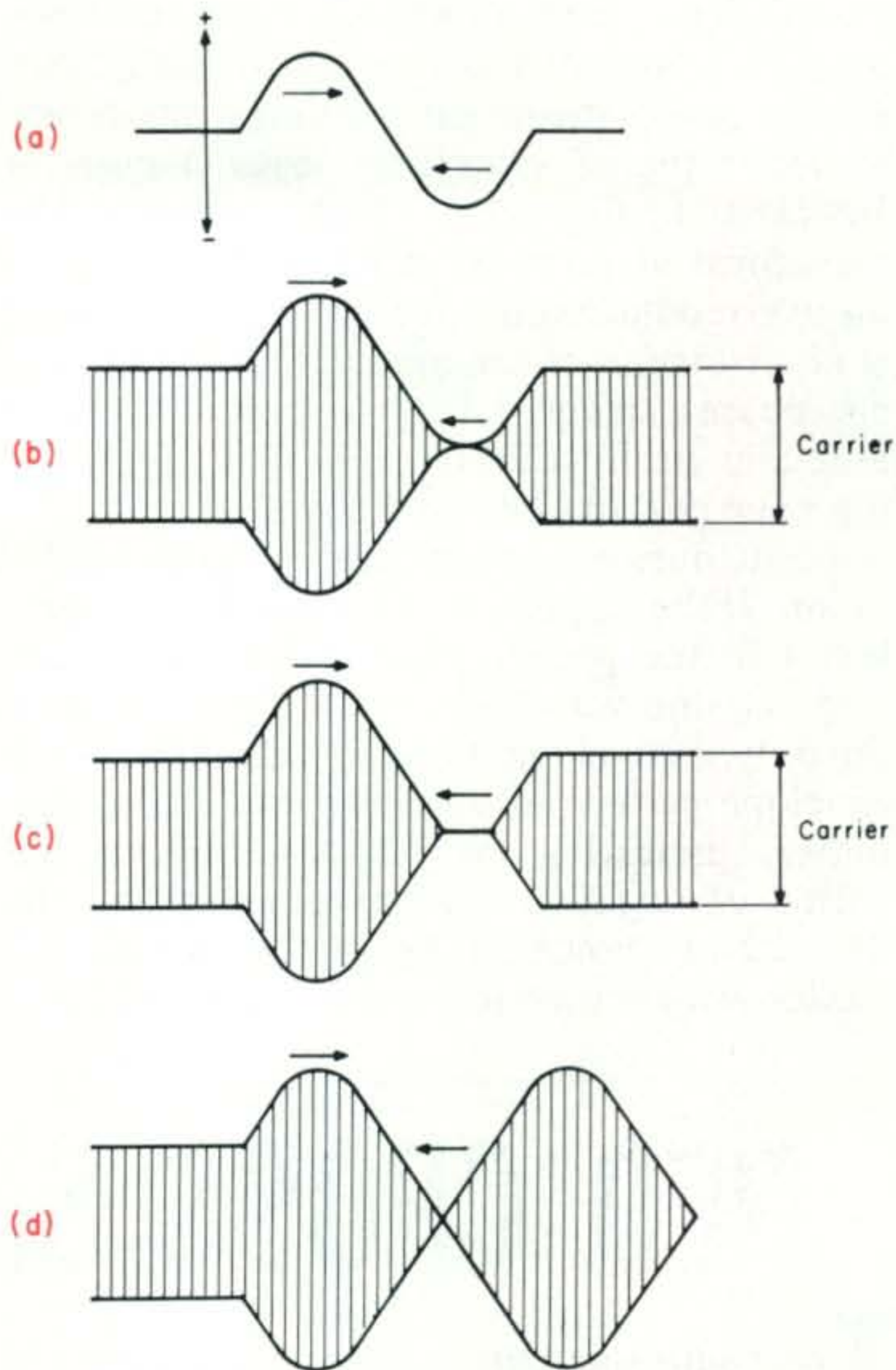


Fig. 5 (A)—The arrows indicate the phase of the two halves of the sine wave. (B) The arrows again indicate the phases of the normal modulated signal. (C) Envelope of an overmodulated transmitter.

$$\begin{aligned} f_1 &= 886 \text{ watts} \\ f_2 &= 30.1 \text{ watts} \\ f_3 &= 3.8 \text{ watts} \\ f_4 &= 0.9 \text{ watts} \end{aligned}$$

The power of 886 watts at the fundamental frequency is desirable; the power of approximately 35 watts of harmonic power is illegal, and the power of 78.5 watts dissipated in resistor  $R_2$  is wasteful. What is needed is a special circuit which will utilize the entire 1000 watts of audio output power and generate sidebands which are representative of the fundamental frequency only. The W6QYT circuit does this by properly adding the waveforms across the loads  $R_1$  and  $R_2$  in a common r.f. load, fig. 4(C). This r.f. addition of waveforms ensures the proper shape of the transmitted envelope but the circuit must also consider the *phases* of a sine wave.

### Phase

A sine waveform indicates phase as well as shape. The arrows shown in fig. 5(A) indi-

cate the two phases of a sine waveform. When an a.m. transmitter is modulated, the phases of the audio modulating voltage are represented in the r.f. output by phase changes as indicated in fig. 5(B). (Note arrows.) The waveform at point X in fig. 4(A) indicates an overmodulated d.c. voltage in which there is no distortion of the modulating signal. The r.f. phases, generated by a special r.f. final amplifier circuit, capable of properly responding to an overmodulated d.c. voltage, must be opposite during adjacent half cycles of modulation. If the responses of  $V_1$  and  $V_2$  are combined in the proper phase relationship, the original sine waveform will be generated in the output envelope. Figure 5(C) is the wave envelope pattern of an overmodulated transmitter, indicating no response during the period of negative peak overmodulation. In the circuit shown in fig. 4(C), where the diodes were shown to represent the unidirectional

response of a vacuum tube to plate voltage, diode  $V_2$  responds only during the period of negative peak overmodulation.

The r.f. amplifier tube represented by  $V_1$ , called the "normal" tube, generates a given phase during the positive peak and the opposite phase during the negative peak up to the point at which it is cut off (100%). The r.f. amplifier tube represented by diode  $V_2$ , called the "upside down tube," must generate the same phase that the normal tube was generating at the time of cutoff. The resultant waveform is shown in fig. 5(D).

The combination of the r.f. amplifier,  $V_1$ , and the upside down amplifier,  $V_2$ , in a final amplifier permits the use of audio power greater than the amount necessary for 100% modulation. A practical circuit will be shown and analyzed in Part II to be published in a subsequent issue.

[To be continued]

## RED CROSS SERVICE AWARD

**T**wo radio amateurs received the top awards presented at the annual Disaster Services Volunteer Recognition Program of the Cincinnati Area Chapter of the Red Cross. Held May 9 at the Cincinnati Red Cross Building, recognition was given persons who had assisted Red Cross for one, five, ten, 15 and 25 years. Receiving the two 25-year pins were LeRoy Dieselberg, W8SVU, and Paul Luhn, W8MXR. Both men received the awards for their activities through the Queen City Emer-



gency Net (W8VND/W8VVL), emergency communications affiliate of the Cincinnati Chapter.

Also recognized for extended service was Walter Keck, Jr., W8IIO, QCEN member who received a ten-years award. Seven QCEN'ers were presented five-years service pins. They are: Jene Gaible, WA8GPQ, John Hultgren, WA8GPX, Ralph Hultgren, WA8-ELC, Joseph Phirman, WA4-HFF, Eddie Retherford, WA8GRR, Kirk Swallow, W8-QID, and James Weaver, WA8VOA.

One-year service certificates were given to Hal Blocher, Jr., Theodore Chinn, Sr., K8NJQ, John Dann, K8OGE, John Dine, WA8DFD, Walter Gibbemeyer, WA8PRR, Ronald Hasselbrook, WA8LOW, Timothy Prince, WA8TYF, Charles Southern, W8-PNK, John Wilson, WA8CKB and Burton Wolfe, WA8ULF.

QCEN has provided communications assistance in the southwestern Ohio-north central Kentucky area in every disaster involving the Red Cross since the 1937 Ohio River flood.  
(Tnx WA8COA)

LeRoy A. Dieselberg, W8SVU, right, being presented a 25-years Red Cross service pin by Walton Bachrach. Bachrach is chairman of Volunteer Services for the Cincinnati Area Chapter of the Red Cross, and former mayor of Cincinnati.

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CQ-39



Cliff, W2CCY adjusting transmitter during EME test is shown in foreground. Right to Left in background is Roger Abson (no call), Dick, W2IMU, and Tony K2KII (back of head just shown).



Half of operating shack. In foreground R-L Tony K2KII, and Dick W2IMU. In Background L-R Ernest, WA4WDK (standing), Roger Abson at controls dish, and Cliff W2CCY at transmitter.

## SPECIAL BULLETIN ABOUT

**T**HE Crawford Hill VHF Club which has previously conducted successful moonbounce tests on 144 and 432 mc has done it again, this time on 1296 mc.<sup>1</sup> As predicted by the club months in advance on the nights of April 12 and 13 the signals of W2NFA (the present club call) were copiable by well equipped 1296 mc stations by means of the moon.

On April 12 QSO's were completed with: HB9RG at 0035-0050 z with RST 459 sent and 139 received, G3LFT at 0220-0235 z with RST 449 sent and 229 received, WB6IOM at 0300-0325 z with RST 559 sent and 339 received. A partial QSO was also made with K6MYC at 0400-0530 z, their signals being 6 db inside the noise in a 1 kc bandpass. No other signals were heard this night.

On April 13 QSO's were again completed with: G3LTF at 0100-0120 z with RST 349 sent and 339 received, WB6IOM at 0425-0445 z with RST 559 sent and 339 received. WB6IOM tried s.s.b. transmission with very poor copy at W2NFA. Another partial QSO was made with K6MYC and K6HCP was heard using the K6MYC station. No other signals were heard.

The following comments were received by

<sup>1</sup> The Crawford Hill VHF Club was the first group to work VK3ATN via the moon. At that time they used the call K2MWA.

the Crawford Hill Club. OZ8EME who was operational receiving only using a 20' dish and a TIXM103 transistor preamp reported receiving weak signals both nights with maximum S/N of +1 db in a 1 kc bandpass. G3LTF who was assisted by G3VPK, G3-ORL and R. Condon, used a 17' dish, 4-7289's in two 180° hybrid coupled amplifiers for transmission and a paramp for receiving, noted that W2NFA's signals were 10 db above the noise in a 100 cycle bandpass. HB9RG used a 17' dish, 7650 with 300 watts out and a paramp and was not operating the second day. WB6IOM who had the loudest signal of all used only a 10' dish with circular feed. His transmitter consisted of 8-2C39's in a ring giving 500 watts of output. For receiving Peter used a paramp and copied W2NFA's signals 6 db above the noise in a 150 cycle filter. K6MYC reported copying very weak signals. This group used only an 8' dish, 4-7289 amplifier and a paramp. WB6-CXF reported no signals heard. WB6CXF was a last minute group effort using a 24' home built dish. K4QIF also reported no signals heard. Rusty used a 10' dish and TIXM-103 for receiving. K2TKN received weak signals off the moon. The big problem at Bill's QTH and others was the low angle of the moon during the tests. At no time during the





Other half of operating shack. R-L W2WVA station trustee and club president standing, Ed, W2FZY at Racal receiver, and Bill W20J in front of tape recorder.



The ten foot parabolic reflector dish shown mounted on a polar mount was used by Peter Laakmann, WB6IOM, to work the Crawford Hill VHF Club, W2NFA, on April 12, 1968. Below, Peter is shown in front of the dish.

## 1296 MOONBOUNCE TESTS

night was the moon clear of house or trees. K2TKN used a home brew 20' dish and KMC transistor preamp.

The W2NFA moonbounce effort was led by Dick Turrin, W2IMU. The basic exciter/receiving equipment was supplied by Cliff, W2CCY. The final amplifier which produced 300 watts out and consisted of two dual 7289 (late version of the 2C39) amplifiers coupled together by means of 90° hybrids was constructed by W2IMU from a design of W2CCY/W2CQH. The paramp used as a preamp, was mounted on the rim of the dish on a loan from K2TKN. The dish itself was 60' in diameter and fed by a crossed dipole feed built by W2IMU. Members on hand during the tests were W2IMU, W2CCY, W2FZY, K2KII, WA4WDK, W2WVA, W20J, and Roger Abson.

Future moonbounce operation by W2NFA will be exclusively on 1296 mc. The next test will probably be in the Fall (Oct.-Nov.). Since most of the present activity is in the Northern Hemisphere and most stations have foreground clearance problems for low elevation moon orbits, every effort will be made to schedule the tests for a weekend with positive moon declination but not with new moon phase. Qualified stations desiring to participate in future 1296 EME tests may obtain

advanced notice by sending two self addressed stamped envelopes to R. Turrin, W2IMU, Box 45 RR 2, Colts Neck, N.J., 07722. ■



Peter, WB6IOM in front of his 10' dish.

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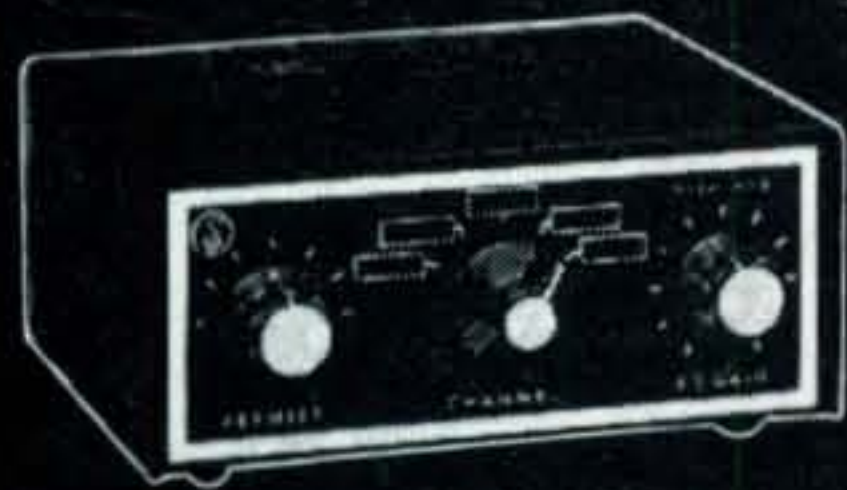
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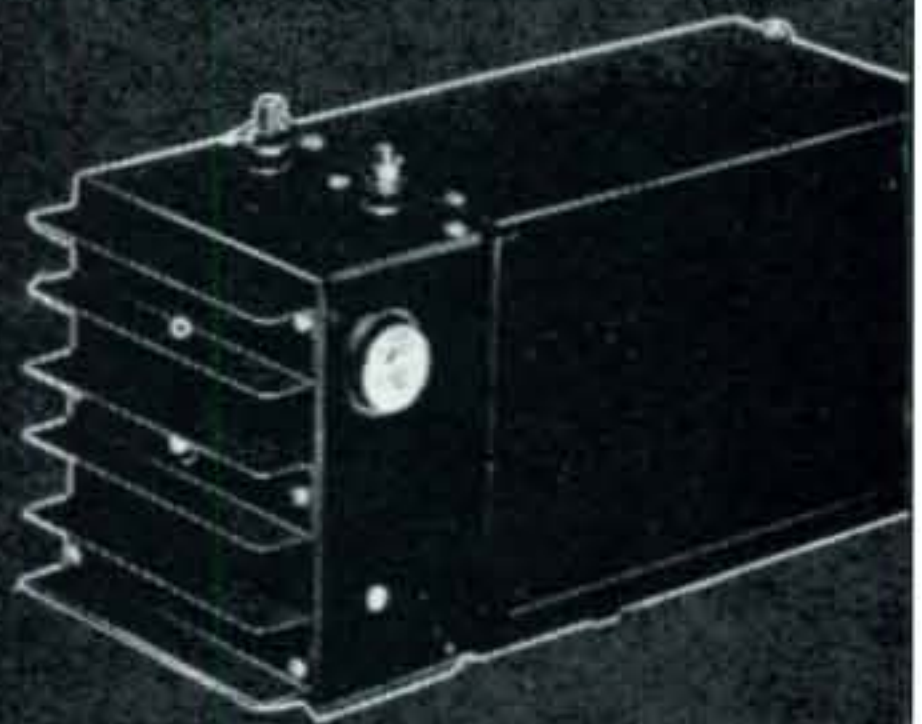
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# VERTICAL ANTENNAS

## Part II

BY CAPTAIN PAUL H. LEE, \*W3JM

*This is the second in a series of articles on a subject which has never before been treated in depth in an amateur magazine. The first chapter in last month's issue covered basic principles. This one deals with base impedances and methods of feeding and matching.*

**T**HE input (base) impedance of an ungrounded vertical antenna which is being fed against a ground plane is dependent on several factors. The one factor which has the greatest effect is of course the height of the vertical radiator. The height is usually mentioned in terms of wavelengths. In the first chapter vertical radiators of 0.25, 0.50 and 0.625 wavelengths height were discussed from the standpoint of their radiation characteristics. It is of interest, however, to plot the base impedance of vertical radiators of all heights from 0.10 through about 0.65 wavelengths height so that the variations may be noted in detail.

The second factor which affects base impedance is that of height (length) versus thickness (diameter). It is customary in texts to define this in terms of the ratio *length/diameter* ( $L/D$ ). If one considers the vertical radiator being fed against a ground plane as an open-ended, unbalanced, lossy transmission line, which it actually is, it will be realized that it must have a characteristic impedance like any other transmission line. The magnitude of this characteristic impedance is determined by the conductor size and spacing. In the case of the vertical antenna (considered as a transmission line) the spacing (position of the vertical conductor relative to the ground plane) is fixed. The only factor which can then be varied, to have an effect on the characteristic impedance, is the vertical conductor's diameter. The effect on the characteristic impedance of changing diameter can be computed. Several authors treat this, but

perhaps Schelkunoff<sup>11</sup> is one of the best references.

### Radiation Resistance

If this unbalanced transmission line could be terminated in its characteristic impedance at its far end, one would see the characteristic impedance when measuring at its input connection. However, it cannot be terminated. It must remain open-ended. Thus it has standing waves on it, and it radiates. When speaking of it as "lossy", this does not refer to its inherent  $I^2R$  losses. This refers to the fact that power put into it is "lost" or radiated into space. This power is represented theoretically as the power dissipated in a *radiation resistance*,  $R_r$ . For a good discussion of the concept of radiation resistance, see Laport<sup>12</sup>. The radiation resistance of an antenna cannot be measured. It can be computed with considerable accuracy. The radiation resistance times the square of the current at the point of reference is the radiated power. This radiated power can be determined quite closely by making field intensity measurements along

<sup>11</sup> Schelkunoff and Friis, "Antenna Theory and Practice," John Wiley and Sons.

<sup>12</sup> Laport, E. A., "Radio Antenna Engineering," McGraw Hill.

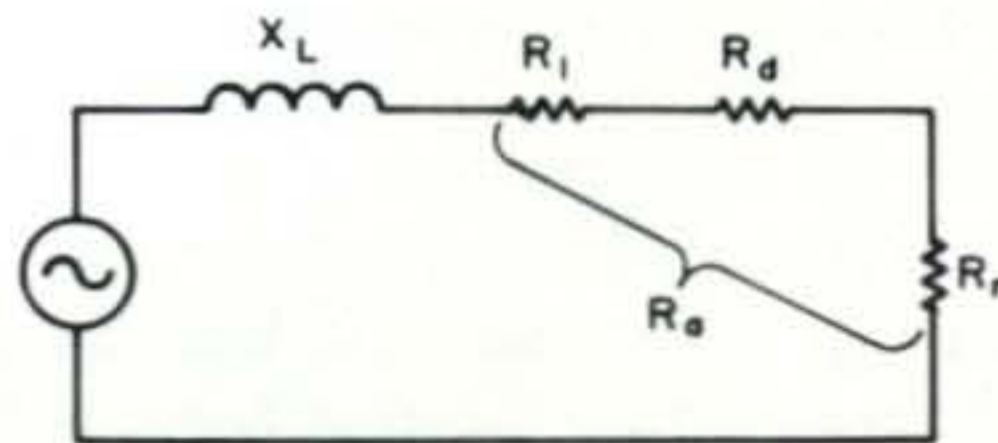
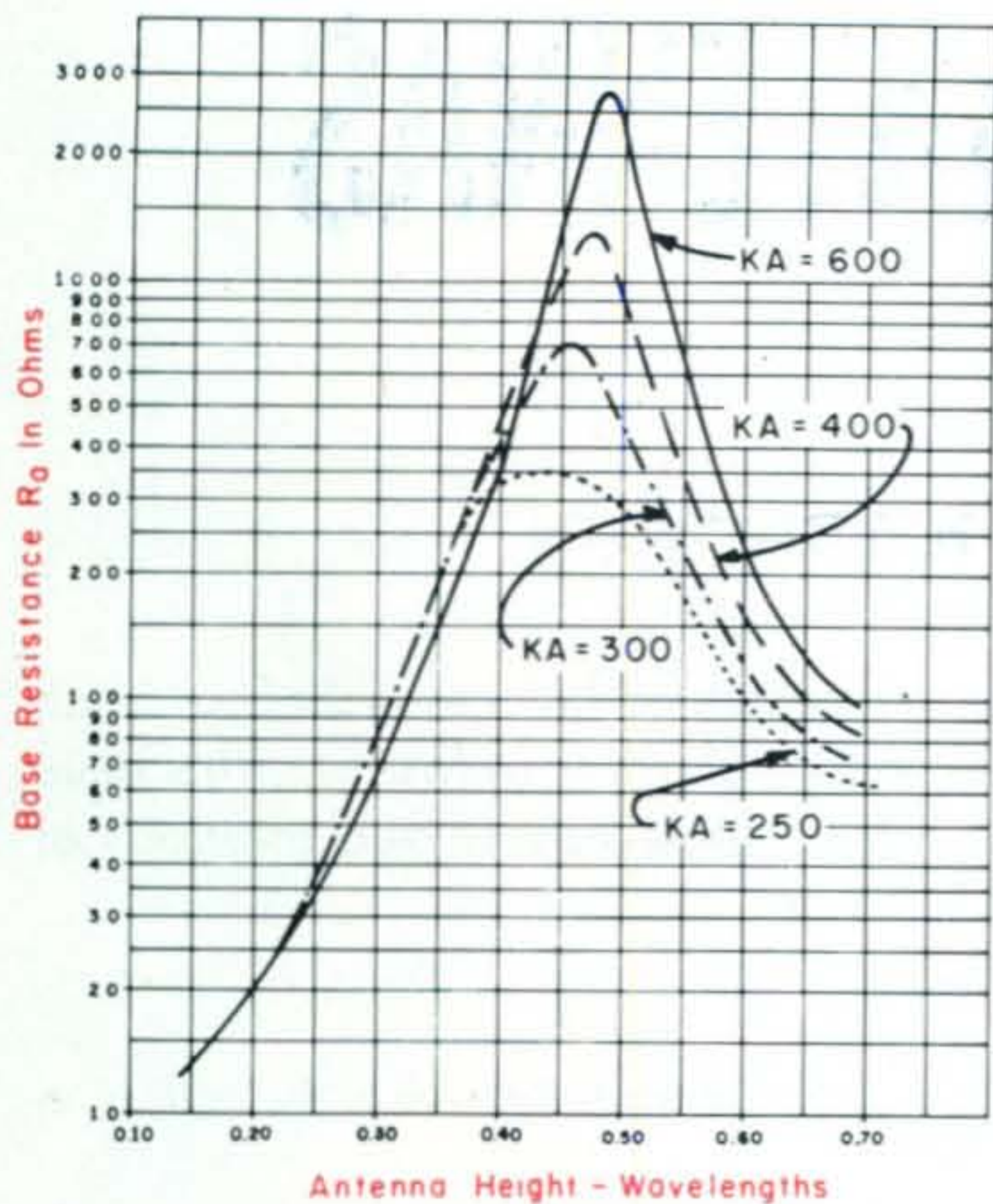
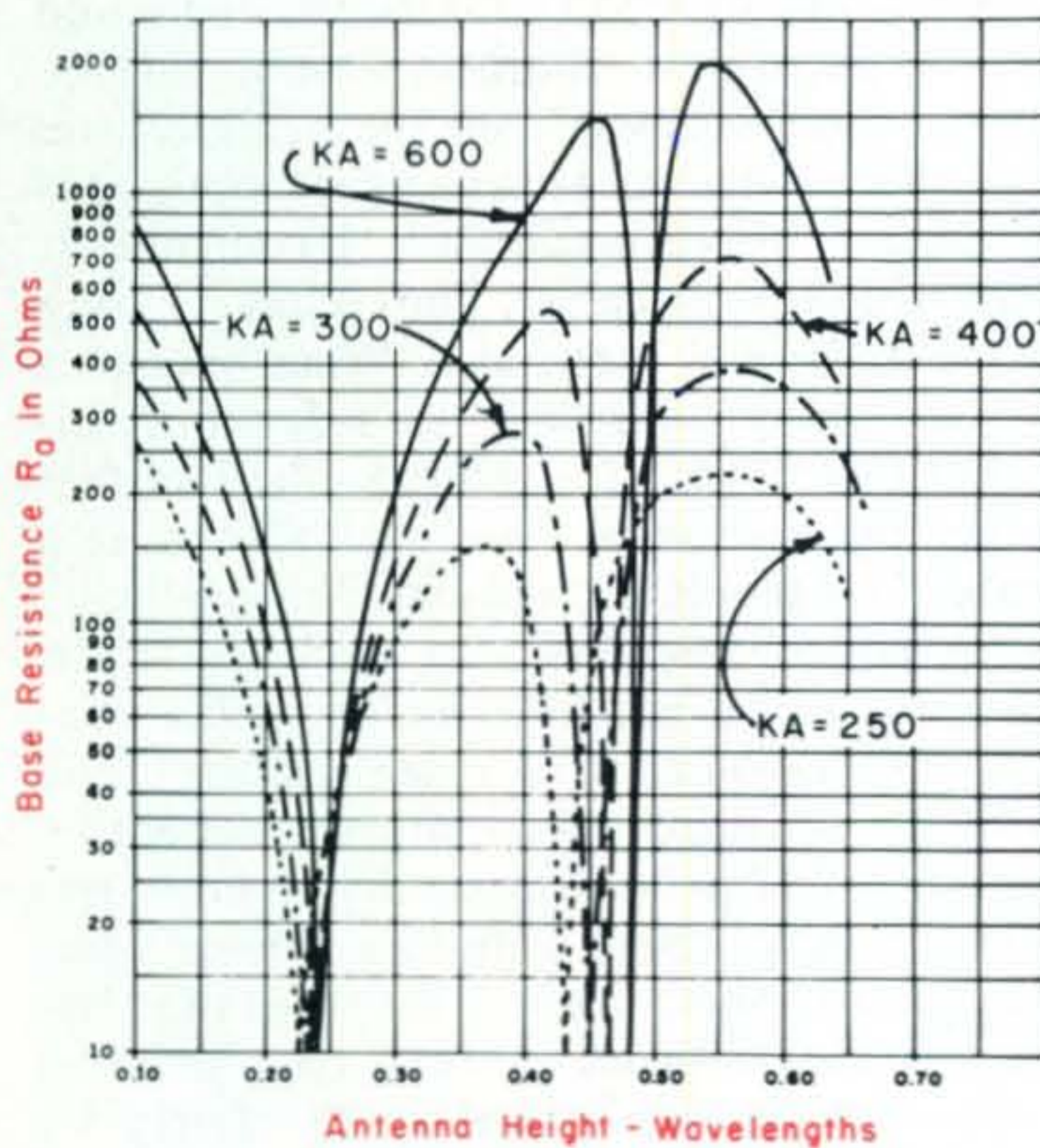


Fig. 12—Equivalent circuit of an antenna system. The total antenna resistance,  $R_a$ , is equal to the sum of  $R_L$ ,  $R_d$  and  $R_r$ .

\* 5209 Bangor Drive, Kensington, Maryland 20795.



(A)



(B)

Fig. 13(A)—Vertical antenna base resistance versus antenna height in wavelengths for different values of characteristic impedance,  $K_a$ . (B)—The plot of the base reactance versus antenna height for the same values of  $K_a$ .

radials at varying distances out from the vertical radiator, plotting them on field intensity paper, and determining the unattenuated field intensity at one mile, as discussed earlier.

When measuring into the antenna, one sees the total antenna resistance,  $R_a$ , which is composed of several parts. This is depicted in fig.

12, which shows the equivalent series circuit of an antenna possessing some inductive reactance. These parts are the radiation resistance  $R_r$ , the ohmic loss resistances  $R_1$  and the dielectric loss  $R_d$ . In the m.f. and h.f. cases, the  $R_r$  is quite large, and it makes up most of  $R_a$ . In fact, in a well designed installation, the several loss resistances are usually neglected. However, at l.f. and v.l.f., where the vertical radiator is a small part of a wavelength,  $R_r$  is very small. In fact, at v.l.f. it is often as small as a fraction of an ohm. When this is combined with fractional ohm loss resistances, efficiency is reduced considerably. At v.l.f. it requires very special care in design, plus many model studies, to obtain an efficiency as high as 50% or so. Not so at h.f., however. We are up in the range of tens and hundreds of ohms for  $R_r$ .

The standing wave configuration on a vertical radiator will depend on its height. The base input impedance will, therefore, show variations with respect to frequency. The magnitude of the peak excursions of impedance will depend on the radiator's characteristic impedance. This fact is shown in fig. 13(A) and 13(B), which are plots of  $R_a$  and  $X_a$ , respectively. They are plotted separately for clarity. The family of curves shows the effect of varying the characteristic impedance of the radiator. Characteristic impedance is denoted by the factor  $K_a$  which can be computed from the following equation:

$$K_a = 120 \log \frac{L}{D} - 120$$

Values of  $K_a$  have been computed as follows:<sup>11</sup>

L/D	10	50	100	200	300	600	1000
$K_a$	323	516	599	682	731	814	875

By reference to fig. 13(A) and 13(B) it can be seen that a thin vertical radiator exhibits greater variations of impedance than does a thick one. (This is true of any antenna.) We make use of this fact in designing broadband antennas, which will be covered later.

### Bandwidth

This brings up the subject of antenna bandwidth. The bandwidth of an antenna is dependent upon the rate of change of reactance versus the rate of change of resistance, with frequency. It may be seen that the thick antenna, the one with the lower  $K_a$ , will have a

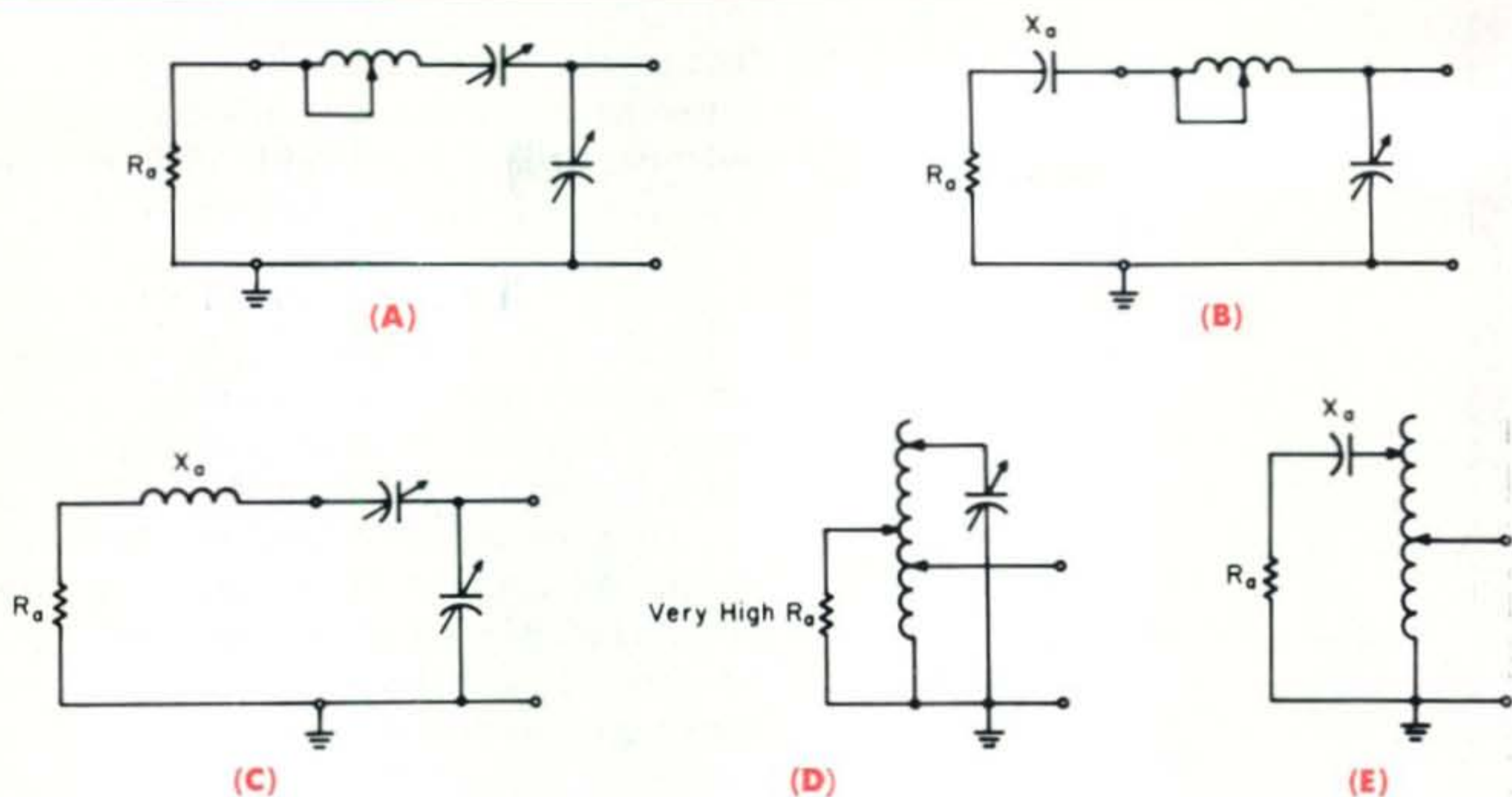


Fig. 14 (A)—Matching unit for an antenna with  $R_a - jX_a = R(\text{low}) - jX_c$ . (B)—Matching unit for a  $\lambda/4$  resonant antenna with a low  $R_a$  only. (C)—Matching unit for an antenna with  $R_a + jX_L$ . (D)—Matching unit for an antenna with a very high  $R_a$ ,  $\lambda/2$  resonance. It is difficult to match well and should be avoided if possible. (E)—Matching unit for an antenna with a high  $R - jX_c$  (higher than coaxial line impedance).

greater inherent bandwidth than the thin one. For practical purposes, operating bandwidth is the band of frequencies centered about the tuned resonant frequency, enclosed within certain v.s.w.r. limits which depend on other factors such as transmission line capabilities, transmitter v.s.w.r. tolerance, modulation r.f. passband response requirements, etc. A figure which is commonly used is the bandwidth to the "3 db down" power limits. There is a very good discussion of antenna bandwidths in Laport.<sup>12</sup>

In the l.f. and v.l.f. cases, bandwidth restrictions can seriously limit an antenna's transmission capabilities unless special designs are adopted to increase bandwidth. These restrictions are caused by the high  $Q$  of these antennas. With very high capacitive reactance and very low resistance, the l.f. or v.l.f. antenna is a high  $Q$  device. There are special designs, which will be covered later, which improve the bandwidth of these antennas, but at the expense of efficiency. One may ask why we need greater bandwidths at l.f. and v.l.f. than heretofore. The reason is that we are gradually converting to multi-channel teletype transmission systems at these frequencies, to increase our traffic handling capabilities, and such systems require greater bandwidth than the old method of single channel keyed c.w.

At m.f. and h.f. we are not worried too

much about bandwidth, except that in the case of some m.f. directional arrays, the coupling and branching networks may in some cases restrict the antenna system's bandwidth, and cause loss of sideband modulation frequency response, unless special design precautions are taken. It is for this reason that the FCC requires the consulting engineer to measure and plot  $R_{in}$  and  $X_{in}$  for a directional antenna system, versus frequency. At h.f. there is no such problem. In the h.f. case bandwidth is important from the standpoint of avoiding retuning of the antenna when shifting frequency, which is very desirable in military and commercial installations.

Reference should again be made to figs. 13(A) and 13(B). Now that we have the plots of impedance versus frequency (plotted in terms of height of radiator in wavelengths), we can state the following general rules for the kind of base impedance which will exist:

Height	Base Impedance
Less than $0.25\lambda$ resonance.	$R - jX_c$
$0.25\lambda$ resonance.	$R + j0$
$0.25\lambda$ physical length.	$R + jX_L$
$0.25\lambda$ resonance to $0.50\lambda$ resonance.	$R + jX_L$
$0.50\lambda$ resonance.	$R$ (Very high) (Not recommended)
$0.50\lambda$ physical length.	$R - jX_c$ (High)
$0.50\lambda$ physical length to $0.625\lambda$ electrical length.	$R - jX_c$

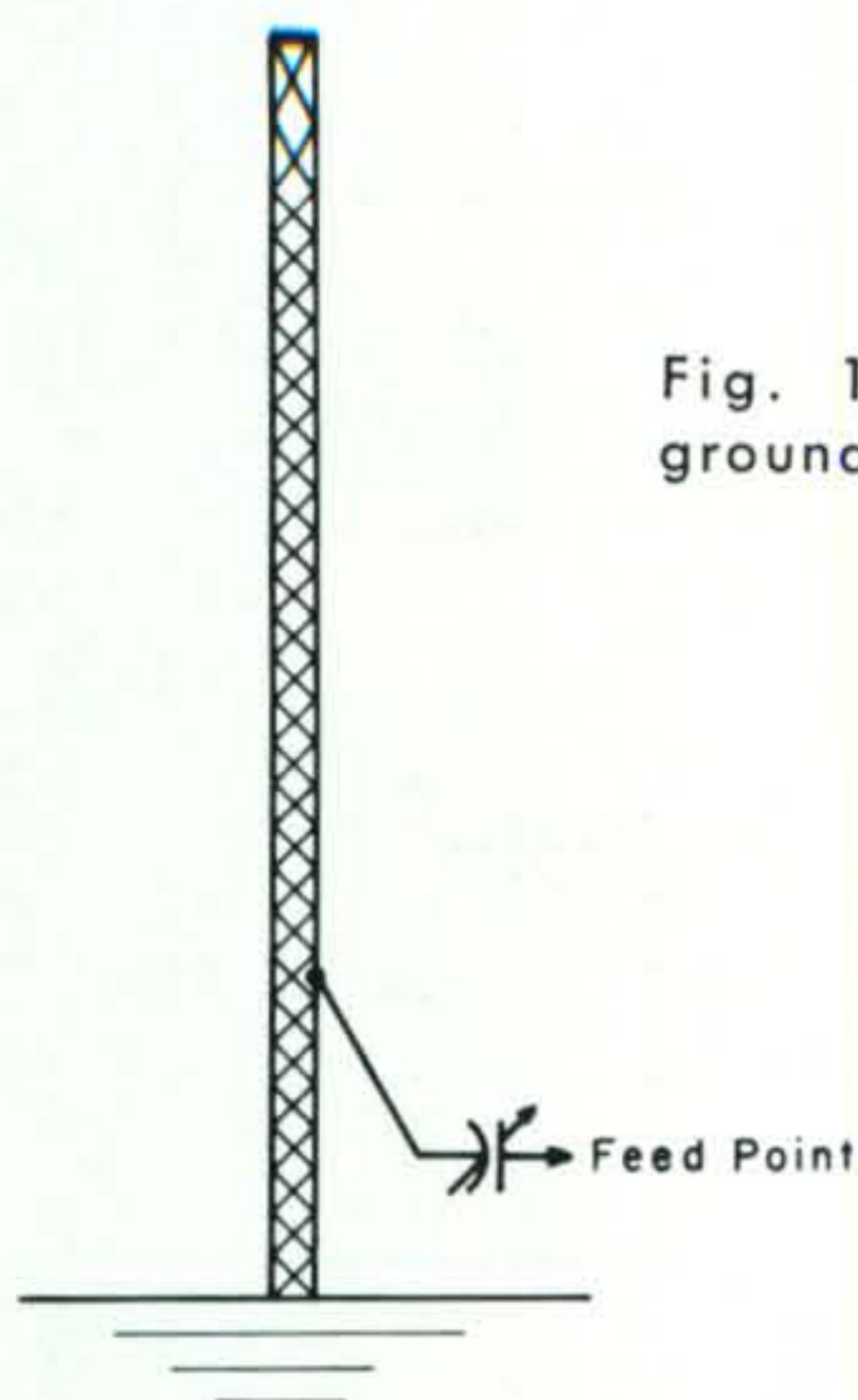


Fig. 15 — Shunt fed grounded base vertical antenna.

It will be noted that the resonant length is always less than the physical length by an amount which is inversely dependent on the  $L/D$  ratio.

### Tuning And Matching Networks

This leads to the next topic, which is the tuning and matching networks required to resonate and match the antennas of heights shown in the preceding impedance summary, to a known source. In modern times the known source has come to be the nominal 50 ohm coaxial line, although 70 ohm line is sometimes used. The matching networks are quite simple, and are shown in figs. 14(A) through 14(E). The values of the reactances required in each case may be calculated by use of r.f. network theory as shown in Terman.<sup>13</sup> In general, if the antenna input reactance is  $-jX_C$ , inductive reactance  $+jX_L$  will be required in the network to tune it, and *vice versa*. The network also simultaneously transforms the antenna input resistance into a value which matches the characteristic impedance of the transmission line.

Where an antenna is fed through a tuning and matching unit of this type, the *total antenna system reactance* must be taken into account in bandwidth computations. This total value includes not only the antenna's own input reactance versus frequency, but also the effect of the reactances in the matching unit as they vary with frequency. The computation of this is not difficult, although perhaps a bit laborious. The simplest approach is to actually tune up the matching unit with antenna attached, and then measure

<sup>13</sup> Terman, F. E., "Radio Engineering Handbook," McGraw Hill (first edition).

the matching unit's input impedance versus frequency. There are certain "tricks" with networks which can be employed to improve antenna, system bandwidth and give lower v.s.w.r. over a range of frequencies.<sup>14</sup>

### Shunt Fed Verticals

In the previous paragraph we spoke of tuning and matching a series fed, ungrounded, vertical radiator. Now let's consider the case of the grounded base, shunt fed vertical radiator. There have been several excellent articles on this subject.<sup>15,16</sup> The shunt fed configuration is shown in fig. 15. Simply stated, a tap is brought off the vertical radiator at a distance above ground and it is used as a feed point, having its input impedance matched to the characteristic impedance of the transmission line. In some cases it is possible by trial and error to adjust the tap's vertical position on the radiator so that the input impedance is  $50 + jX_L$ , thus permitting an easy match to 50 ohm line by use of only a series capacitor of equal reactance. This adjustment, however, can be quite tedious and critical, especially when hanging on the side of a tower or mast, and it is much simpler to use a matching network of proper reactance values. This type of feed has been used in many broadcast installations. It has been proven by actual full scale model studies and field intensity measurements<sup>15</sup> that use of this feed method is just as efficient as is series feed, and that the horizontal radiation pattern is not distorted by the presence of the sloping feed wire. By both mathematical analysis and actual radiator current measurements<sup>15,16</sup> it has been shown that current distribution on the shunt fed radiator closely approaches that of a series fed radiator, and that the vertical radiation pattern is not appreciably different.

A similar arrangement, and one most often used by amateurs, is the "gamma" match or "omega" match, similar to that used on the driven element of Yagi arrays. This is shown in fig. 16. This principle was used in the feed arrangements for the Mark III and the Mark IV DX antennas which were published some time ago.<sup>17,18</sup> A feed rod is connected to the radiator at a suitable point some distance

<sup>14</sup> Lee, P. H., "Broadband 80 Meter Feed for the Mark III," *CQ*, March 1964, p. 43.

<sup>15</sup> Morrison, J. F., Smith, P. H., "The Shunt Excited Antenna," *Proc. of the I.R.E.*, June 1937.

<sup>16</sup> Badoux, P., "Current Distribution and Radiation Properties of a Shunt Excited Antenna," *Proc. of the I.R.E.*, June 1940.



## **FOR THE THRILL OF A LIFETIME**

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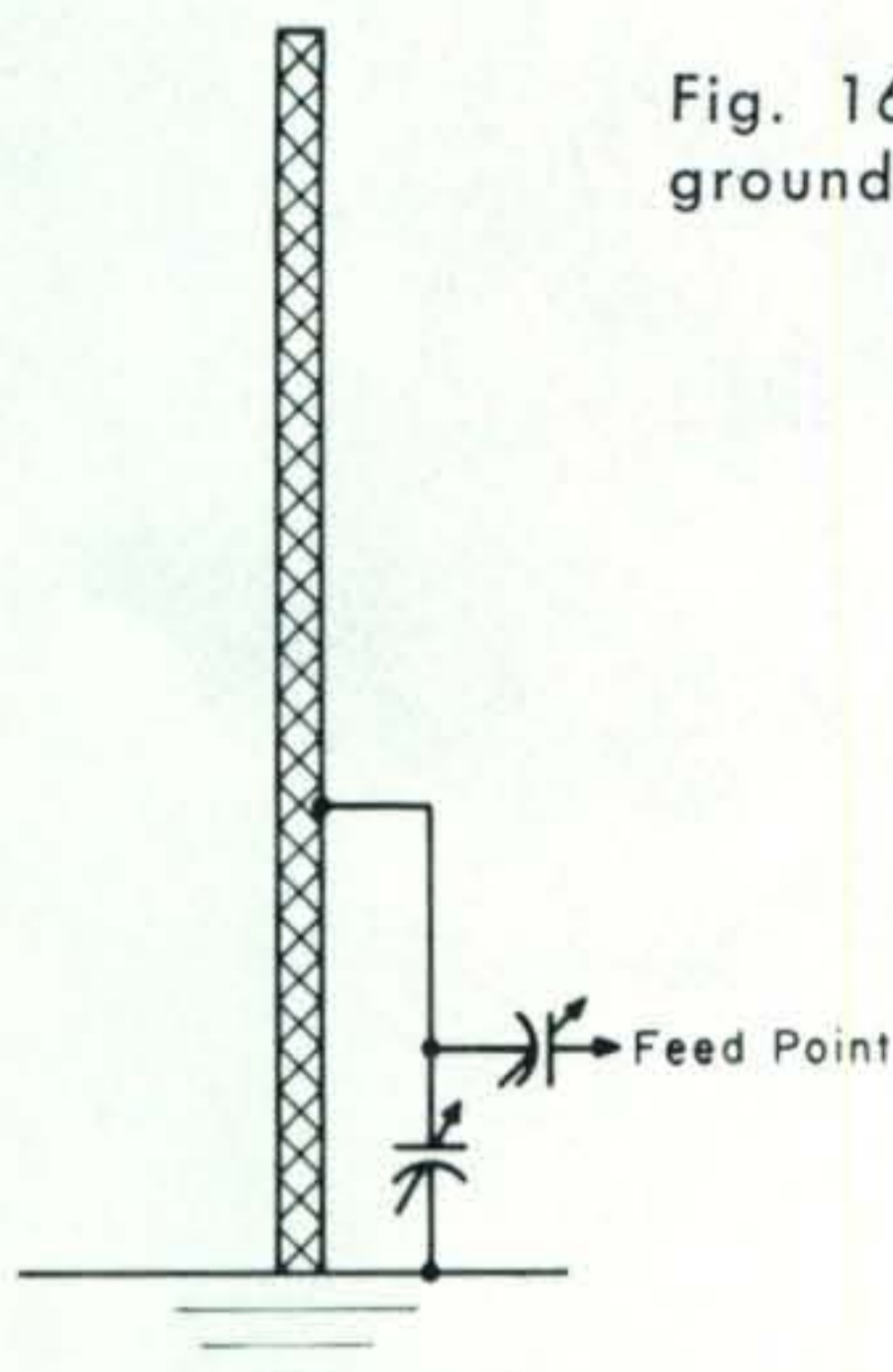


Fig. 16 — Omega fed grounded base vertical antenna.

above ground, and it is brought down the side of the radiator rigidly supported on standoff insulators. It is fed at its bottom end. It must always be considerably less than  $\frac{1}{4}$  wavelength for its input impedance to be of a reasonable value. Note my experience with the 7 mc feed on the Mark IV<sup>18</sup>. The input impedance will always measure  $R + jX_L$ , because the short section of transmission line (feed rod plus the portion of radiator concerned) thus formed is less than  $\frac{1}{4}$  wavelength and shorted at its top end. Matching then becomes a question of adjusting the several capacitive reactances in the matching unit. The  $R$  term of the input impedance may be quite low. The values in the Mark III and Mark IV articles<sup>17, 18</sup> are typical.

If the feed rod (or wire) runs all the way to the top of the vertical radiator, the whole thing becomes a folded unipole antenna and was used as a feed in the Mark IV for 2 and 4 mc.<sup>18</sup> This type will be discussed in detail later.

### Ground Bus

There is one additional point that should be made very emphatically in connection with the shunt fed and gamma or omega fed antennas. That is that the ground bus from the tuning unit to the base of the radiator should be heavy and low loss. On the Mark IV I used a  $\frac{1}{4}$ " by 1" aluminum bar (to avoid use of dissimilar metals). This bus carries considerable current, especially where the  $R$  term of the feed point impedance is low. For

<sup>17</sup> Lee, P. H., "The Mark III DX Antenna," *CQ*, December 1962, p. 43.

<sup>18</sup> Lee, P. H., "The Mark IV DX Antenna," *CQ*, February 1967, p. 60.

1 kw in the antenna (2 kw p.e.p. transmitter input), with a feed point  $R$  of 10 ohms, there would be 10 amperes current flowing in this bus (and in the feed rod as well). The capacitors in the matching unit should be large enough to withstand the voltages developed across them.

Each method of feed has certain advantages and disadvantages. The series feed has the advantage of simple matching when the antenna base impedance is capacitive, by means of a single tapped coil, as in fig. 14(E). A simple variable matching unit with a band-switching arrangement can be built to tune a series fed radiator at several frequencies. However, unless a 3-legged self-supporting tower is used, the series fed radiator must usually be guyed because it has to be insulated from ground. Of course one may use small self-supporting whips for short verticals.

On the other hand, the grounded base radiator is quite easy to make self-supporting. Short, light weight ones can be set right in the ground itself, and tall heavy ones can be set in concrete. Very tall ones must usually be guyed. The grounded base permits other circuits to be run up the tower or mast without any special choke coils or other isolation devices. Such circuits would be tower lights, rotary beam motor control cables<sup>18</sup>, and in some cases even the coaxial lines for v.h.f. or u.h.f. antennas can be run up a grounded vertical radiator without isolation. This latter idea has been used in several broadcast tower installations where a.m., f.m. and c.a.t.v. antennas utilize the same tower structure.<sup>19</sup>

Feed rod construction is simple. Even multiple feed rods are not difficult to install and adjust<sup>17, 18</sup> for feeding the vertical radiator on several frequency bands. Jasek's "Antenna Engineering Handbook"<sup>20</sup> is a veritable gold mine of information on vertical radiators (and on other types also), and especially on some of the schemes we have been discussing. It also provides an excellent source of additional references, listed at the end of each chapter.

The next installment will deal with electrically short vertical radiators, and ways of matching to them.

[To be Continued]

<sup>19</sup> Gureckis, P. V., "A Simple Method of Isolating CATV Antennas On Standard Broadcast Towers," *Broadcast Management-Engineering*, January 1968.

<sup>20</sup> Jasik, H., "Antenna Engineering Handbook," McGraw Hill.



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On 'Phone, 9 of the top 10 DX'rs...on CW, 7 of the top 10 and...on VHF, 8 of the top 10...use *RCA Tubes*

Right across the ARRL "Honor Roll"—'Phone or CW, low band or VHF—the top scorers were checked by an independent research organization. The findings: the largest percentage of the "big guns" use RCA transmitting tubes! Whether they run commercial or

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# RCA



**Introducing:  
the end of  
the good old  
ham mobile  
antenna.**



(Now all other ham mobiles under the sun are obsolete.)

Until this very minute, most ham mobile antennas were pretty good.

But with the introduction of this one, what made them pretty good, now makes them pretty bad.

This one is that much better.

To start with, we figured if you were paying a lot of money for a car, you didn't want to junk it up with an odd-looking, not very streamlined antenna. As you can see, our new one is starkly beautiful from the slick-looking corona ball down to the unique new swivel base.

And, since garages are hardly ever as tall as a car and an antenna, we built this one with a shake-proof sleeve clutch that folds over when you want to garage it.

(Which also means you can change from one band to another in a couple of seconds by simply unscrewing one complete coil and tip rod unit and screwing another onto the foldover mast.)

Compared to most other antennas, this one is Hercules. It's strong enough to take a knock without bending. And, the "turn over" mast is a hefty  $\frac{5}{8}$ " solid rod of highly polished, heat-treated aluminum.



We've also done away with the old-fashioned plastic shrink tubing. The lightweight precision-wound coils are totally sealed in an indestructible epoxy-fiberglass sleeve. (Which, by the way, is a distinctive white that'll add to the beauty of your car.) And, all fittings are heavy chrome plated brass.

That takes care of that. Now for performance.

This new ham mobile works like something beyond your wildest dreams. That's because it successfully combines higher Q with wider bandwidth performance, without using a lossy-heat generating coil like the others use.

It's also designed on a nominal 52 ohm impedance so you don't have to have any special matching. (Any length of coax will work.)

We've called this new ham mobile antenna the end of the good old mobile ham antenna.

Actually, it's just the beginning of much better ham mobiles. From Hy-Gain.

#### ELECTRICAL

- Nominal 52 ohm impedance—no special matching device needed.
- Widest bandwidth, highest power handling—Vs.—heat drift ratio available.
- Lowest VSWR in any mobile available.

#### MECHANICAL

- Turn-over mast is hefty  $\frac{5}{8}$ " dia. solid rod of highly polished heat-treated aluminum.
  - All connections are standard  $\frac{3}{8}$ -24 thread.
  - Mast folds over, swivels, and turns over. You can mount it on bumper or deck. In addition, this flexibility makes it easy and simple to change coils.
  - Coil and tip rods are a one-piece assembly. Coil diameters are constant, only lengths change.
- | BAND | COIL LENGTH |
|------|-------------|
| 75M  | 13"         |
| 40   | 6"          |
| 20   | 5"          |
| 15   | 4"          |
| 10   | 3"          |
- Shake-proof sleeve clutch facilitates quick band changeover and fold over for garaging.

### The Ham Mobile Antenna from Hy-Gain

HY-GAIN ELECTRONICS CORPORATION AC-7B  
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● THE STRONGEST SIGNAL UNDER THE SUN

# Results of the 1967 CQ World Wide DX (C.W.) Contest

BY FRANK ANZALONE\* W1WY

**T**HE c.w section of the contest this year (Nov. 1967) was somewhat disappointing after the good conditions we had had for the phone section the previous month. However we still had a good one and exceeded last year's total.

Once again I will dispense quoting figures and refer you to the various charts that give this information in details. In the single band division the top scores are listed for world wide comparison. The Honorable Mention lists the top U.S.A. stations, exclusive of those that made the world high lists.

Without a doubt PY2SO's score on 28 mc was the outstanding performance of the contest. Sonia had wanted to take it easy this year but found the band open almost around the clock, so chalk up a new world record.

And that VK8UG score was made by none other than Tubby Vale of VK5NO fame of a few years ago. Conditions on 10 are sure different in the southern hemisphere.

Honors on 21 mc were evenly divided with no records being broken. However one of the Bazley family, John Jr. put G3HCT at the top of the list. Many of last year's 15 meter buffs went to 10 this year.

This was the year that we had expected to see the 14 mc band lose its hold on the single band Trophy but PY2BGL a consistent performer on 20, handily defeated his countryman PY4OD. So Manoel gets the Cup and Talma has to admire the one he won a few years ago.

Our fellows in the US made their best showing on 7 mc in spite of the low participation on that band. It will be interesting to see if 4X4RD will be able to get a Trophy out of the Israel Radio Club. Some years ago they donated one for the highest score on 40, but after the initial award we were never able to get any confirmation for later winners.

The Europeans dominated the 3.5 mc band but no outstanding scores were made. In checking the logs we found that most all of the contacts were of the local variety with very few 3 pointers listed. The 80 meter band

## TROPHY WINNERS

Single Operator, All Band, World  
W9IOP, Larry LeKashman Trophy  
won by Katashi Nose, KH6IJ

Single Operator, All Band, Europe  
W3MSK Operators Trophy  
won by Vladimir Goncharsky, UB5WF

Single Operator, All Band, U.S.A.  
North Jersey DX Association Trophy  
won by Robert M. Knowles, K1DIR

Single Operator, Single Band (14 mc)  
K2HLB, Dr. Harold Megibow  
Memorial Trophy  
won by Manoel R. A. de Castilho, PY2BGL

Multi-Operator, Single Transmitter  
W3AOH, Dr. Anthony Susan Trophy  
won by Station 4L3A  
(Oprs: UA6DP, UQ2AO, UQ2CC, UQ2GA,  
UQ2IM, UQ2LL, UQ2MS, UQ2NX, UQ2-  
0371, UW6BA, George, Gunnar

Multi-Operator, Multi Transmitter  
K2GL. "Buz" Reeves Trophy  
won by Station PJ3CC  
(Oprs: W1BIH, W1FJJ, W1TX, W3GRF,  
W4GF, W4KFC)

## SPECIAL CQ PLAQUES

World All Band Champion  
J. R. Beck, ZD8J

Club Award  
Potomac Valley Radio Club

just did not produce the multipliers this year.

A pleasant surprise was the returns on 160. Conditions were not favorable for trans-Atlantic contacts but the Europeans had a ball between themselves. However it was ZC4RB that picked up the marbles and a new world record. Rolly took advantage of all those 3 pointers north of him, altho he found it hard work and frustrating. Said he heard several W/Ks but could not raise them or TG0AA.

The all banders surpassed most of last year's scores and in many cases established new sectional records. (See page 64, Sept. 67 CQ).

Last year's winner, ZD8J still remains the

\* 14 Sherwood Road, Stamford, Conn. 06905.

world's champion and John gets the Special CQ Plaque for his efforts.

The World (W9IOP) Trophy however goes to that perennial contender KH6IJ, Nosey finally made it. Katashi always runs up a very high QSO total but usually does not have the multiplier to make the score stand up.

The European (W3MSK) Trophy goes to another consistent contender UB5WF. Vladimir just missed making a million but did set a new record for Europe. Now, how do we get the Cup to him? Anyone going to the Ukraine?

The U.S.A. (NJDXA) Trophy found a home at K1DIR, last year's phone winner. Bob had quite a donnybrook going with W1BPW and just did nose out Peter by having a higher Zone multiplier.

The region south of the Caucasians has become a choice area for contest operation by the USSR boys. This year a group from Latvia went on a contest expedition to Georgia, set up 4L3A, and made a new world's record to win the Multi Single (W3AOH) Trophy. To date we have not received the log of 4J7B, another group that was very active in the same area.

Another contest expedition, this one to Guatemala by K4BAI and W4YWX, set a new record for North America with TG0AA. Their biggest thrill was snagging G3RPB on 160. They would have really flipped if they had heard ZC4RB who was also calling them.

The Multi Multi Big Guns really poured it on. Many stations exceeded previous records but still didn't make the Top Six.

The PJ3CC operation, a contest expedition jointly operated by a crew of six crack c.w. men from the PVRC and the Conn. Wireless clubs, handily won the Multi Multi (K2GL) Trophy. With that kind of talent and all those 3 pointers north of them, how could they miss. And you had better believe that the log was an accurate one and that all the rules were observed. It was signed by W4GF, Bill heads the Amateur Radio division of the FCC. How about that?

And you had also better believe that Freddie did some pretty close checking of the logs of the eternal rivals, K2GL and W3MSK. With a separation of less than 10 thousand points in a 4 million score, a couple of multipliers could change the margin of victory.

The CX8CZ operation must have pooled all the resources in Uruguay as there was

### Additions

The 28 mc phone score of DL7BA with a total of 220,104 697 36 72 was inadvertently left out of the results last month. This puts Guenter at the top of the list for Germany.

And the c.w. log for 5R8BA, Don Miller's operation from Malagasy, was received after we had gone to press with the results. Don's score would have been listed as follows: 5R8BA A 2,614,877 2135 132 299. This would have put him at the top of the Top Ten but unfortunately it was much too late to be used.

hardly no other activity out of there.

The club competition ran more or less true to form, with the Potomac Valley gang still King of the Roost. It was their big guns that once again proved to be the deciding factor and give them their 6th plaque over the past 10 years. (W4ZM the club's president has assured me that there are no grounds to the rumor that they are out to win a plaque for each member of the club.)

This is only the second year of competition for the Rhein-Ruhr DX group and they almost pulled the upset of the contest. Walter, DJ6QT promises an even greater effort next year so the PVRC had better look to their laurels.

Both the Frankford and Northern Calif. clubs seem to lack the big multi scores to be in real competition. While with the OH-DX-Ring it's just the opposite, all chiefs and no Indians.

As for the YV5 boys, it's still a lack of c.w. men. And the North Jerseyites have once again crawled back into their cocoon after a fine comeback last year.

You will note some fine totals from groups not previously heard from so this might be a sign of things to come.

Once again we were given an assist by some of the European organizations. The Central Radio Club of Czechoslovakia sent their logs in neat packages, sorted by bands and categories, with scoring corrections by Karel Krbec. OK1ANK and Milos Prostecky, OK1MP. The DM entries were similarly treated by Klaus Voight, DM2ATL. While Jan Osowski, SP6AAT took care of the PZK entries. We are eternally grateful fellows,

	Station	QSO's						Zones						Countries						
		1.8	3.5	7	14	21	28	1.8	3.5	7	14	21	28	1.8	3.5	7	14	21	28	
Single Operator All - Band	ZD8J		53	282	494	352	407		11	21	31	25	19		16	38	70	62	54	
	KH6IJ		45	282	437	593	500		6	16	26	22	20		5	16	39	31	21	
	K1DIR		31	202	185	330	176		7	26	32	30	29		13	57	76	75	61	
	5H3KJ		4	106	464	383	382		4	14	24	20	24		4	31	54	47	52	
	W1BPW		51	230	216	241	172		11	22	31	24	25		22	56	83	68	55	
	UB5WF		283	197	235	448	186		8	16	27	22	24		38	48	70	55	46	
	KA7AB		44	119	216	430	205		15	19	32	30	27		19	31	42	45	41	
	KX6DB				437	544	530				31	25	29				55	32	35	
	W4YHD	4	27	178	169	261	190		2	9	29	31	27	27		2	16	62	63	63
	G3HDA	1	68	236	272	276	190		1	10	20	26	25	22		1	35	55	65	51
Multi Operator Single Transmitter	4L3A		306	472	604	425	569		13	23	31	26	23		49	64	88	63	66	
	TGØAA	23	119	440	739	734	560		5	8	21	30	27	25		4	9	38	64	61
	ZS5QU		3	38	1064	363	537		3	11	29	27	24		3	11	63	52	52	
	W3WJD		26	286	316	304	226		9	30	36	30	31		16	71	107	74	73	
	W3BGN	1	37	222	319	316	237		1	7	23	34	25	26		1	18	50	80	63
	OF2TI		57	303	438	326	172		7	22	28	27	26		33	57	64	60	56	
Multi Operator Multi Transmitter	PJ3CC		191	898	1590	1553	962		7	20	29	26	28		8	46	68	64	61	
	W3MSK	16	121	580	632	591	512		5	21	32	36	33	31		6	43	80	119	
	K2GL	11	120	587	699	665	321		3	18	33	35	34	30		4	42	80	123	
	CX8CZ	3	37	225	1020	1057	957		2	11	24	34	29	31		3	13	30	87	
	OF2AM	158	383	604	862	873	437		3	12	27	36	33	31		13	49	76	101	
	W4BVV	12	77	512	543	714	449		6	17	34	35	31	32		5	32	90	109	

Top scores band-by-band breakdown.

### United States Club Scores

Potomac Valley Radio Club	22,896,335
Frankford Radio Club	14,991,482
Southern California DX Club	11,060,760
Northern California DX Club	8,394,077
Golden Triangle DX Club (Fla.)	7,843,796
Northwest DX Clubs Association	5,672,962
Connecticut Wireless Association	2,799,616
Western Washington DX Club	2,525,338
North Jersey DX Association	2,445,810
Order of Boiled Owls (N.Y.)	1,907,632
Rochester DX Association (N.Y.)	1,464,790
128 DX Contest Club (Mass.)	1,409,504
Willamette Valley DX Club (Ore.)	807,956
Central Michigan A. R. C.	735,250
Poughkeepsie Radio Club (N.Y.)	729,794
West Gulf DX Club	726,275
Hamfesters Radio Club (Ill.)	636,091
Detroit A. R. Association	626,894
Suffolk County Radio Club (N.Y.)	565,020
Angel's Roost DX Club (Texas)	438,328
Southeastern DX Club	391,952
Virginia Century Club	389,310
North Alabama DX Club	318,001
Morris Radio Club (N.J.)	306,161
Florida DX Club	295,645
Utah DX Association	254,644
Ohio Valley A. R. Association	217,296
Central Iowa Radio Club	171,264
West Side A. R. C. (La.)	136,315
Miami Valley A. R. C. (Ohio)	133,399
Baton Rouge A. R. C. (La.)	114,121
Northeast DX Association	78,540
West Allis A. R. C. (Wis.)	55,540
Oak Park A. R. C. (Mich.)	34,686
QCWA DX Club (N.Y.)	26,508

### Foreign Club Scores

Rhein-Ruhr DX Association	20,463,644
OH-DX-Ring-Ry. (Finland)	13,089,316
Radio Club Venezolano	11,335,475
DM-DX Club (East Germany)	3,114,955
Latvia DX Radio Club	3,084,536
E. T. A. DX Radio Club (Sweden)	2,950,243
Uruguay DX Club	2,761,816
LVOV DX Club (Ukraine)	2,186,757
Saar-Pfalz Radio Club (Germany)	2,083,742
Far East DX-Ploiters (Japan)	1,959,564
Far East Auxiliary R. C. (Japan)	1,804,439
Kiel Canal Radio Group (Germany)	1,655,500
Moscow Radio Club (USSR)	1,300,009
Lampertheim Radio Club (Germany)	1,221,854
Crimea Radio Club (USSR)	1,081,031
Tallinn A. R. C. (Estonia)	1,068,164
Venezuelan DX Club	1,039,148
Sakhalin Island A. R. C. (USSR)	977,218
Gateway A. R. C. (Germany)	889,801
SP-DX Club (Poland)	884,875
Swiss DX Club	831,656
Mashonaland A. R. C. (Rhodesia)	749,070
Calagary A. R. Assoc. (Canada)	729,985
Leningrad A. R. C. (USSR)	714,180
Leipzig Contest Team (Germany)	570,486
Kamiseya A. R. C. (Japan)	566,104
Vasteras Radioklubb (Sweden)	545,509
RAF Troodos A. R. C. (Cyprus)	543,582
Anglo American Contest Group (England)	451,605
Czechoslovakian DX Team	429,535
Nagoya DX Club (Japan)	280,210
Radio Club of Budapest (Hungary)	278,710
Waggeryds DX Club (Sweden)	248,404
Hammarbyhoejden A. R. C. (Sweden)	204,161



















Bob Snyder, WØGTA can always be expected to turn up in a contest from some distant location or other. At present he is in Norway signing LAØAD, which is quite an improvement over some of the long calls he has had to use.

LZ2KBI : Club.  
 LZ2KEF : Club.  
 LZ2KIM : Club.  
 LZ2KRZ : Club.  
 OE4SZW & OE4WBW, OE7VV.  
 OF2TI : OH1QP, OH2BO, OH2BCP, OH2XI, OH3PC, OH5SE, OH9RF.  
 OF2ZD & OH2BEM, OH2BHM, OH2VB, OH5WL.  
 OF3AG : OH3LG, OH3LO, OH3MK, OH3MN, OH3SM, OH3TM, OH3VJ, OH3WW, OH3YU.  
 OF3TR : OH1YO, OH1ZQ, OH6VC, OH7RJ, OH8RI.  
 OF6AA : OH6NH, OH6YA.  
 OH1VR & OH3YI.  
 OK1KHL : Club.  
 OK1KKS : Club.  
 OK1KOK : Club.  
 OK1KTL : Club.  
 OK1KWR : Club.  
 OK2KJU : Club.  
 OK2KMR : Club.  
 OK2KOV : OK2BJR, OK2BOB.  
 OK3KAG : Club.  
 OK3KGW : Club.  
 OK3KWK : Club.  
 OY6FRA : Club.  
 PIIPT : Club.  
 SL5ZL : Club.  
 SM6CKV & SM6BJI, SM6DXK.  
 SPØHIL : SP9APR, SP9BCB, SP9CEM.  
 TGØAA : K4BAI, W4YWX.  
 TY2KG : W6DOD, W6KG.  
 UA1KAE : Club.  
 UA1KAL : Gene, Victor.  
 UA1KBB : George, Wowa, Yuri D., Yuri S.  
 UA1KMF : UA1UG, UA1UH.  
 UA1KUA : Club.  
 UA1KUB : Club.  
 UA3KBO : DM2BOG, UA3-27308.  
 UA3KGA : Valera, Valery, Victor.  
 UA3KHA : Club.  
 UA3KTV : Ed, Tola, Vlad.  
 UA3KUS : Nick, Willi, Yuri.  
 UA3KYA : Club.  
 UA4KSA : Club.  
 UA9KFS : Club.  
 UA9KHA : Club.  
 UA9KJA : Club.  
 UA9KQA : Club.  
 UA9KWA : Club.  
 UAØKBA : Club.  
 UAØKCA : Alex, Jacob.  
 UAØKCG : Oleg, Sergei, Vlad.  
 UAØKFG : UAØEH,

UAØER, UAØFM, UAØFR, UAØFK, UAØFM, UWØFP.  
 UAØKIA : UAØIL, UAØIX, UAØIZ.  
 UAØKKT : Club.  
 UAØKSB : UAØSE, UAØTD, Vlad.  
 UB5KAB : Alex, Vlad, Yura.  
 UB5KBV : Club.  
 UB5KCA : UB5AY, UB5FH, UB5-4155.  
 UB5KFF : Club.  
 UC2KMZ : Al, Oleg, Vlad.  
 UD6KAB : Boris, Edward, Ramiz.  
 UG6KAA : UG6AV, UG6WJ, UG6-6832.  
 UL7KAR : Club.  
 UL7KBK : UL7CA, UL7CJ, UL7CT, UL7-0281.  
 UL7KCB : Slava, Valery.  
 UQ2KBC : UQ2MR, UQ2MU, UQ2-22395.  
 UQ2KBL : Andy, Genady.  
 UQ2KCR : Anatoly, Artur, Gunar, Juri, Sergei.  
 UR2AT : Club.  
 UR2KCR : UR2AL, UR2AW, UR2LO.  
 UT5KDP : UB5-5969, UB5-5973, UB5-45017.  
 UT5KKA : UB5FY, UY5RR, UB5-5398, UB55587.  
 UW3KQE : Club.  
 UW9KQQ : Club.  
 W2PCJ & W2CKS.  
 W3BGN & K3FPY, W3YUW.  
 W3MWC & W2APG.  
 W3WJD & K3FGO, K3JCT, K3MCO, W3DQG.  
 W6BIP & WA6DJI.  
 W6NJu & W6FRZ, WB6IQI.  
 W8BQH & W8CXN, K8DBW.  
 W8UM : K2SIL, K8MFO, W8CQN, W8FAW, WB2FIT.  
 W9EXE & K9YOE.  
 W9YT : K9LBQ, K9ZMS.  
 WØAII & KØIJL, KØZXE, WØLOL, WØTKX, WØYCR.  
 WØHTH & KØKKU, WØCDP, WAØJRW.  
 WA2BLV & WB2MOQ.  
 WA6EPQ & WA6IPY.  
 WB6UDC & WB6NRK.  
 YØ3KSD : YØ3AAJ, YØ3AAO, YØ3AAU, YØ3GU.  
 YØ6KAF : YØ6ADW, YØ6EH.  
 YØ8KGC : YØ8AGZ, YØ8AHA.  
 YU1DKL : Club.  
 ZE1S : ZE1AE, ZE2JD,

ZE2KV, ZE3JJ, ZE3JO, ZE5JJ.  
 ZS5QU & ZS5DC.  
 3C2DCW : VE2BOW, VE2DCW.  
 4L3A : UA6DP, UQ2AO, UQ2CC, UQ2GA, UQ2IM, UG2LL, UQ2MS, UQ2NX, UQ2-0371, UW6BA, George, Gunar.

### MULTI-OPERATOR Multi-Transmitter North America

W3MSK	4,063,920	2452	158	416
K2GL	4,054,092	2403	153	425
W4BVV	3,714,048	2307	155	403
W4KXV	2,605,590	1768	143	367
W4ETO	2,239,380	1655	133	335
W6RW	1,804,168	1444	150	286
W3VKD	1,342,575	1133	122	283
W7SFA	1,256,520	1175	133	237
W4ZXI	764,088	713	112	260
WA2CFG	539,460	567	107	226
WA3EPT	458,784	461	117	237
W3RRV	374,312	459	98	186
W6RGG	298,655	412	106	159
W6GQK	282,030	415	98	140
WA3EPB	145,734	247	87	127

### Africa

ET3FMA 1,387,680 1476 105 231

### Asia

UA9KCE 1,395,663 1571 97 242

### Europe

OF2AM	3,829,375	3317	142	415
DJ6QT	2,001,660	2196	116	322
SM5BPJ	1,795,752	1795	141	368
OH1AA	1,657,350	1954	117	333
DLØKF	1,655,500	1796	126	347
LZ1KPG	1,611,744	2359	117	295
UB5KKA	1,081,031	1723	109	280
UA4KPA	780,325	1537	91	252
DJ5LE	694,600	1527	90	212
OZ5DX	691,114	1169	90	224
DM7M	570,486	1252	86	203
DM7L	506,362	1186	82	199
YU3APR	386,744	891	70	198
SL6AL	361,560	747	80	196
DLØRO	181,353	487	62	121

### South America

PJ3CC	5,527,788	5194	110	247
CX8CZ	3,851,645	3299	131	264
YV5RV	384,921	771	71	100

### The Operators at the Multi-Transmitter Stations

CX8CZ & CX1AAC, CX1BY, CX1DZ, CX2AL, CX3BH, CX7CO, CX8BU.  
 DJ5LE & DJ2JE, DJ2MS, DJ8PU, DJ9KZ, DK1DO, DK1VN, DL2OM, DL3YQ, DL8RE, DL9VN.  
 DJ6QT & DJ1QP, DJ1VP, DJ6TK, DJ7IK, DJ8SW.  
 DLØKF : DJ3UL, DJ4FZ, DJ4SO, DJ5AZ, DJ7SW, DL1FL, DL2ZT, DL8PY.  
 DLØRO : DJ3XP, DJ8SI, DK1IZ, DK2RX, DL3VE, DL3ZI.  
 DM7L : DM2AQT, DM2ATL, DM3MEL, DM3ML, DM3OML, DM3UL, DM3ZUL, DM4EL, DM4YEL, DM5CL, DM5ZCL.  
 DM7M : DM2BFM, DM2CCM, DM2CDM, DM2CEM, DM2CFM, DM2CIM, DM2CLM, DM2DXM, DM3DBM, DM3EBM, DM3NM, DM3RM, DM3SBM, DM3SNM, DM3UNM, DM4JM, DM4ZOM.  
 ET3FMA : K4FMA, K9KBW, W6HOH, Bill.  
 K2GL & K2KUR, K2UYG, KØLFY, W1GYE, W1MDO, W2DNG, W2GLM, W2IWC,

W2JAE, W2VCZ, W6KFF, Alex.  
 LZ1KPG : LZ1BC, LZ1CC, LZ1IB.  
 OF2AM : OH2BBR, OH2BBM, OH2BC, OH2BCZ, OH2BH, OH2BQ, OH2BS, OH2KH, OH2QV, OH2SB.  
 OH1AA : Club.  
 OZ5DX & OZ4UN, OZ5WQ, OZ7X.  
 PJ3CC : W1BIH, W1FJJ, W1TX, W3GRF, W4GF, W4KFC.  
 SL6AL : SM6ALM, SM6ATP, SM6BBM, SM6BWD, SM6CPR, SM6CST, SM6CTQ, SM6CZZ.  
 SM5BPJ : SM5ARR, SM5BDY, SM5BLA, SM5BXT, SM5CZQ, SM5DRW, SM5RC.  
 UA4KPA : UA4PA, UA4PW, UA4PY, UA4PZ, UA4QM, UA4QP, UA4-09410.  
 UA9KCE : Azari, Boris, Leo, Vadim, Vlad, Valentin, Yuri.  
 UB5KKA : Club.  
 W3MSK & K3EST, W3EIS, W3PYS, W3MCG, W3MFJ, W3TMZ, W3ZKH, W9SZR.  
 W3RRV & W3ECR.  
 W3VKD & W3AOH, W3LMM, W3UHN.  
 W4BVV & K3NPV, K3OAE, K4VDL, W1BGD, W3BQV, W3DPJ.  
 W4ETO & K4HF, W4CHA, W4JDR, W4LCP, W4ZCB, WØLNE, WA4PXP, WB4DBZ.  
 W4KXV & K2UFT, K2VGR, K4BVD, K4PQL, K4MXF, K4WUY, WA4JFY.  
 W4ZXI & K4WIS, W4BJ, W4FRO, W4HOS.  
 W6GQK & W6SR.  
 W6RGG & K6ALH.  
 W6RW & K6UMV, K9ELT, W6BXL, W6DGH, WB6OLD, WB6TMC.  
 W7SFA & K7HAY, W7DL, W7DZO, W7VY.  
 WA2CFG & W2LWI, W2YWO.  
 WA3EPB & W3EVW.  
 WA3EPT : K3CUW, K3GJD, K4GSU/3, W3BOQ, W3WZL.  
 YU3APR : YU3ER, YU3EY, YU3TBM, Leon, Lojze.  
 YV5RV : YV1MG/1, YV5AEP, YV5AN, YV5AZG, YV5BCN, YV5BHR, YV5BOG, YV5CET, YV5CGV.

Our thanks to the following stations who sent us their chec logs:  
 DL9BW, DM2ADC, DM2AHM, DM2AJG, DM2AMF, DM2AWF, DM2GUØ, DM3NPA, DM3YPD, DM4UG, DM4ZCF, F2SQ, HA1ZH, HA5FA, HA7PM, HA8KUX, HAØLL, HAØ515, HB9IX, LZ2-193, LZ2-K-49, LZ2-C-4, OF4RH, OF6NH, OK1AKQ, OK1ALU, OK1ALU, OK1APB, OK1ASE, OK1AYY, OK1DJ, OK1KBI, OK1KPA, OK2ABU, OK2BBJ, OK2BCJ, OK2BFT, OK2BJJ, OK2KFK, OK2QX, OK3CEG, OK3CIK, OL6ADD, OZ3PO, OZ7DX, OZ7KV, PAØMIB, SP1BLE, SP2AØB, SP3BES, SP3BTS, SP4-6102, SP4-6127, SP6ARE, SP6RT, SP6XA, SP9EC, SM2DHC, SM3CJD, SM5BGK, SM5BHW, SM5BNX, SM5DUT, SM5UH, SM6CKU/mm, SM7ASN, SM7BEX, SM7DMT, VE1ARJ, VE3ATF, VE7HQ, VU2MD, W2WZ, W3CTE, W4DGJ, WA4OZM, ZL1ACW, UA3BR, UW3CY, UA4AE, UA4BB, UA4BO, UA4SG, UA4KHW, UA9MY, UA9FI, UAØTN, UB5ES, UB5FL, UB5VX, UT5BH, UT5NA, UY5UI, UL7JI, UA3-27185, W3CTE.

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# CQ Reviews:

## The Drake Solid-State VHF Equipment

BY WILFRED M. SCHERER,\* W2AEF

**T**HE Drake line of solid-state v.h.f. gear consists of two f.e.t. converters, the Model SC-6 for the 50 mc band, the SC-2 for the 144 mc band; the Model SCC-1 v.h.f. Crystal Calibrator and the CPS-1 Power Supply. All the units can be plugged into the Model CC-1 Console to comprise an integral package for a complete v.h.f. setup in one cabinet. Switching between the different units for various functions is accomplished by selectors on the panel for the cabinet. This provides rapid operating convenience without necessitating cable changes between individual units and the associated receiver or antennas; while the installation of the equipment into one functional console makes a neat station layout, eliminating the usual unsightly arrangement of converter chassis' along with cables drooped hither and yon.

The individual units also are arranged so in the event you are a one-band operator or do not have the console, they may be plugged into one another to form one piece of equipment.

\*Technical Director, CQ.



The Drake Model CC V.H.F. Console

### The Converters

Both converter models employ field-effect transistors in the r.f. and mixer stages for the optimum in solid-state performance with low noise, high sensitivity, minimization of overload and cross modulation.

Bandpass coupling between stages provides an essentially uniform response over the full 4 mc range for the particular band. The i.f. output is 14-18 mc for full band coverage and the output impedance is designed to match into 50 ohms. Voltage regulation with a Zener diode is provided for ensuring stability of the crystal-controlled oscillator and reverse-polarity protection is provided with a diode in the supply lead which also is filtered for r.f. to minimize stray-signal pickup.

Two crystals, selected with a slide switch, are supplied with each converter. Those for the 6-meter model provide coverage starting at 50 or 50.5 mc when used with a 14 mc and-up i.f. range. With the 2-meter model the coverage starts at 144 and 145 mc for the same i.f. range.

If the associated receiver is a ham-band-only job limited to a 500 kc spread (14-14.5 mc), continuous coverage of just the lower 1 mc portion of the 50 mc band will be available with the two crystals.

On the other hand, with the same receiver conditions, the available coverage on the 144 mc band with the supplied crystals will be 144-144.5 and 145-145.5 mc, leaving a 500 kc gap between 144.5 and 145 mc; however, the units evidently were initially intended for use with the Drake 2C and R-4B receivers (or others where an extended coverage may be had) wherein an additional receiver range of 14.5-15 mc may be obtained using accessory



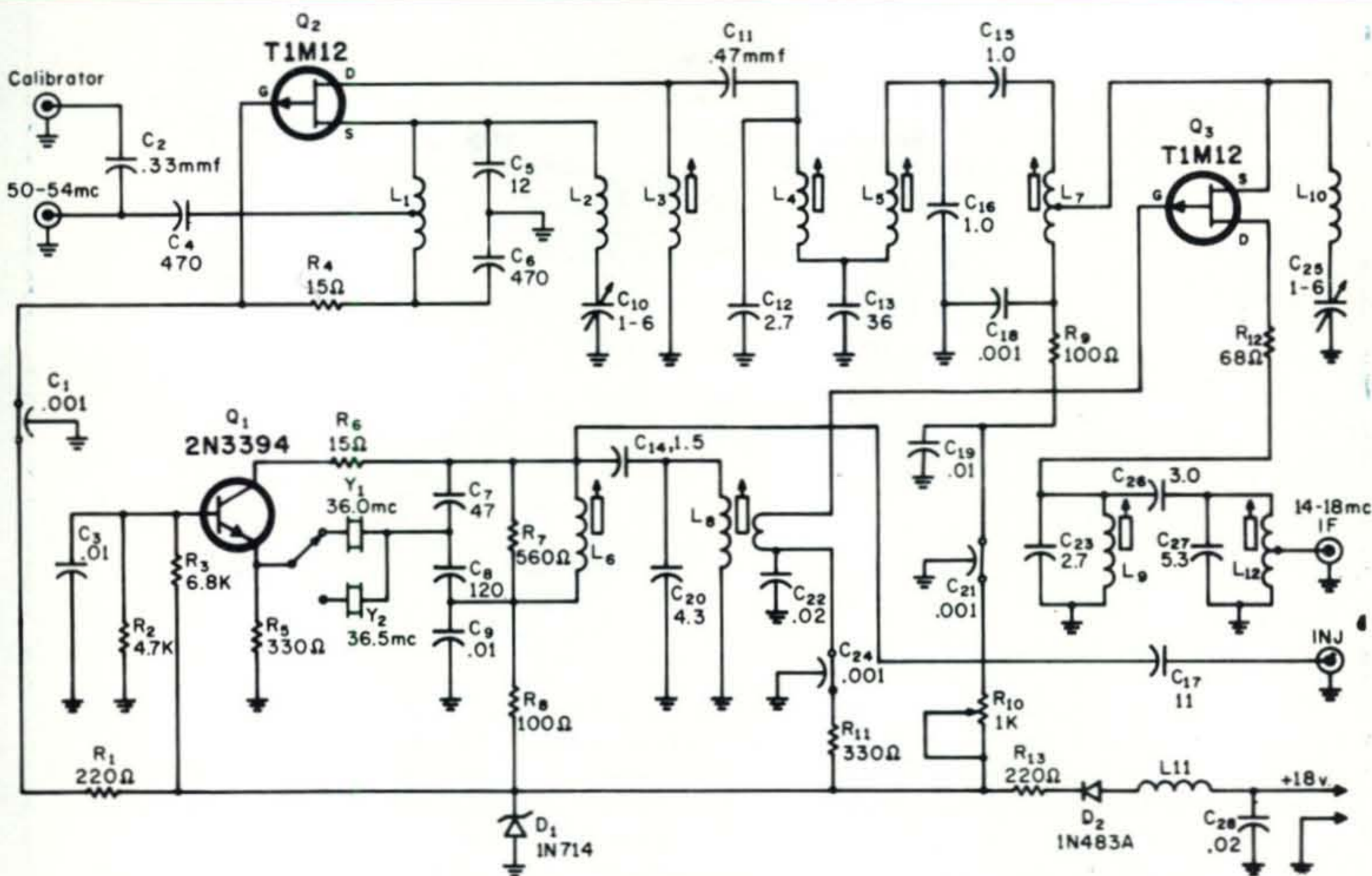


Fig. 1—Schematic diagram for the Drake SC-6 50 mc Converter. See text for details.

plug-in crystals, thus providing the needed i.f. to fill in the gap.

We suspect that this setup with the 2-meter model might have been instituted to avoid the possibility of spurious birdies when the SC-2 is used with the particular receivers.

It also might be noted that with these receivers, complete coverage of the 50 and 144 mc bands may be had by further extending their ranges with the provided auxiliary facilities, as this will furnish the tunable i.f. range as needed for such coverage with the converters.

### Converter Circuitry

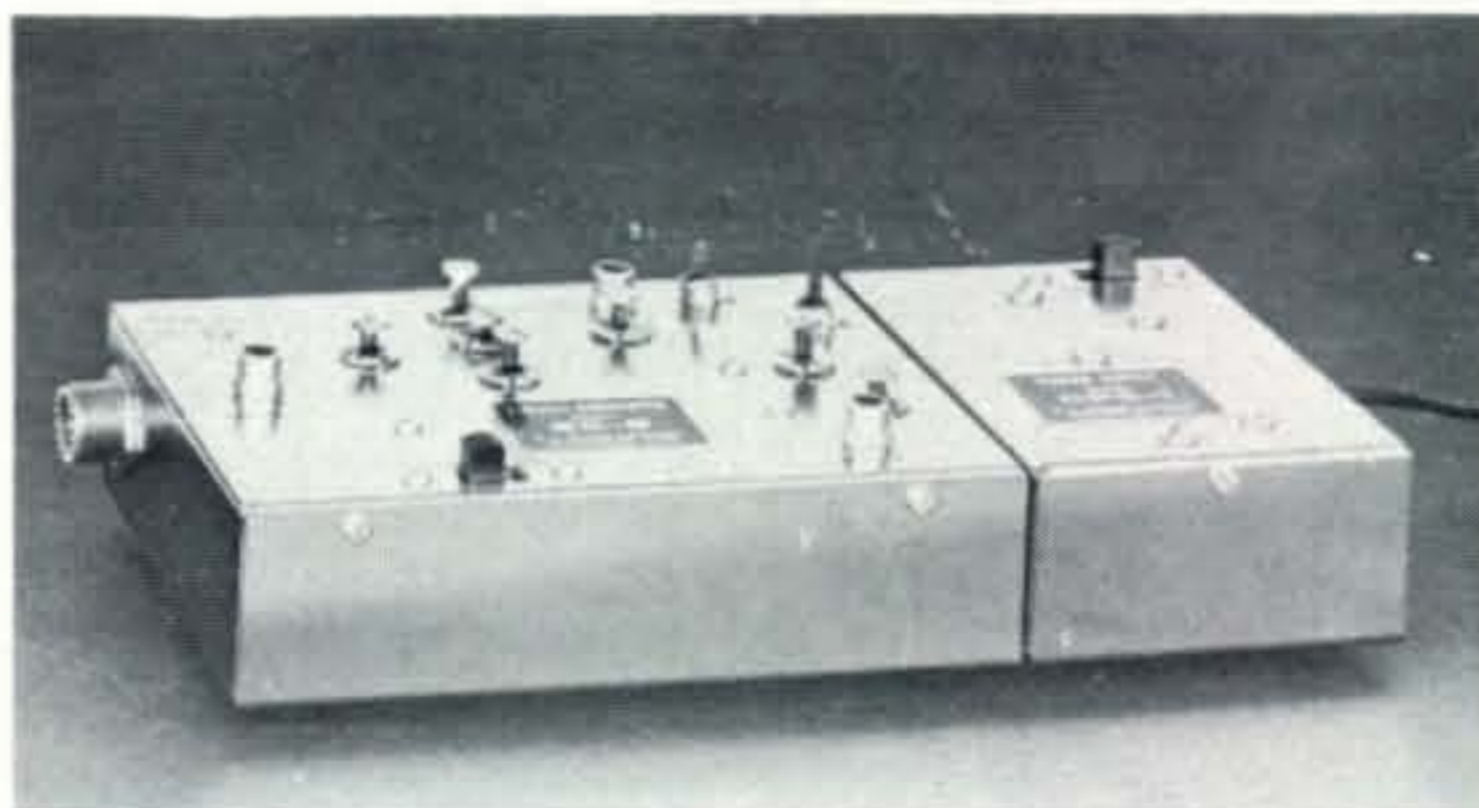
Referring to the schematic at fig. 1, the SC-6 50 mc job employs TIM12 f.e.t.'s in grounded-gate amplifier and mixer stages with a series-resonant 36 mc crystal-controlled oscillator using a 2N3394 conventional type transistor. Bandpass coupling is utilized at the i.f. output as well as between the r.f. amplifier and mixer.

$L_2-C_{10}$  and  $L_{10}-C_{25}$  are 57.750 mc traps used to minimize interference from Channel-2 TV stations. Where such local TV signals are exceptionally strong, interference due to intermodulation products generated by components of the TV signals near 54 mc, may

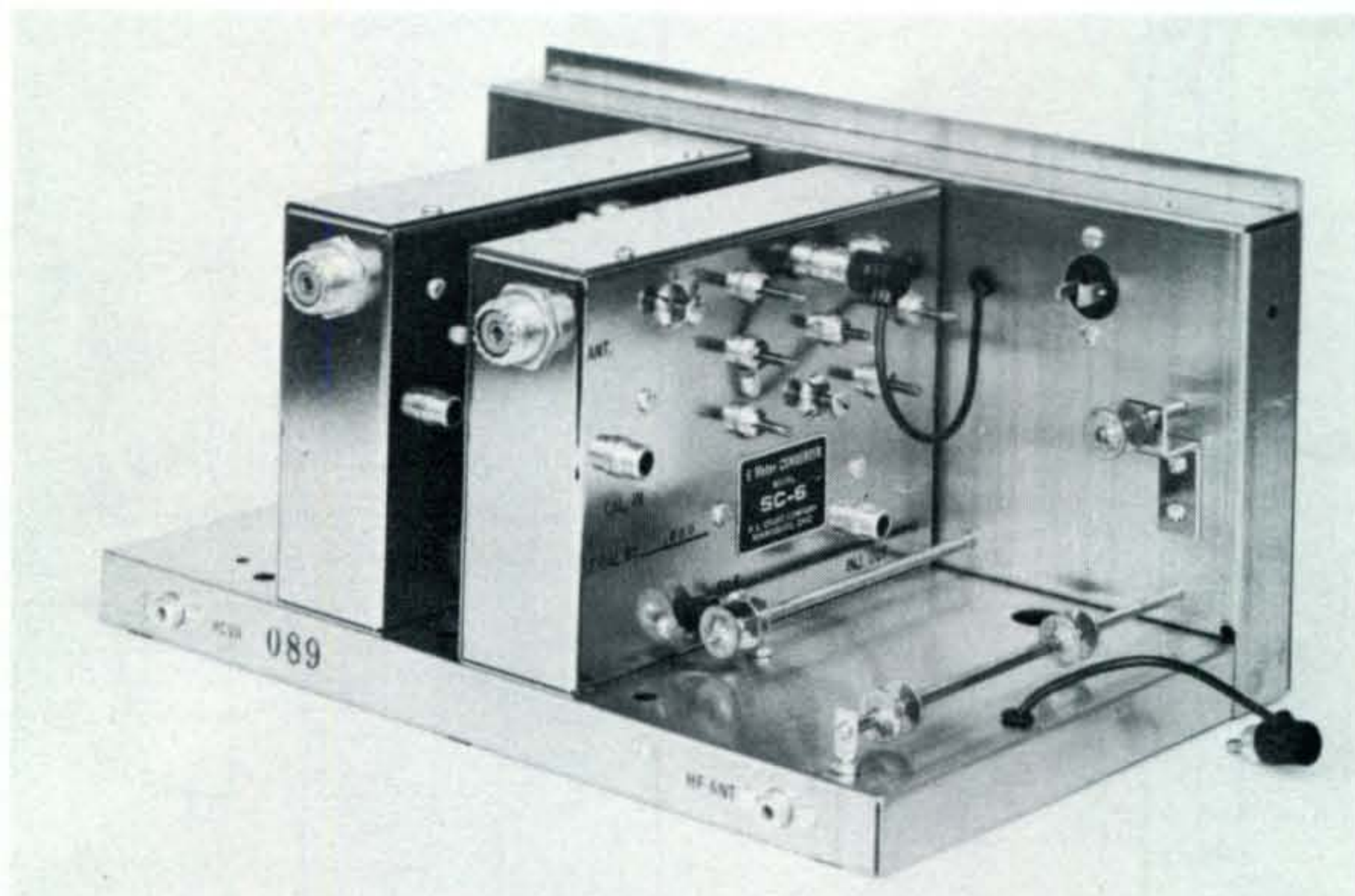
be further attenuated by readjusting the  $L_{10}-C_{25}$  trap to 55.250 mc and if needed, may be accomplished without the use of a signal generator simply by rotating  $C_{25}$  one turn clockwise.

The SC-2 144 mc model employs TIS34 f.e.t.'s with grounded-source r.f. amplifier and mixer circuitry along with bandpass interstage and i.f. output configurations. A 2N3394 comprises a 43.333 mc crystal-controlled oscillator which is inductively coupled to a 2N3663 tripler that is similarly coupled to the gate of the mixer.

In both converter models, output from the oscillator may be obtained from a jack to provide a heterodyning-injection signal for a



One of the Drake converters and the power supply coupled together to form one unit.



Top-chassis view of the Drake Console with two converters installed. A third converter position is at the left end. The power supply and calibrator are coupled together (not shown) and plug in at the right. Mating connectors may be seen at the rear of the panel. One of the mechanical linkage arrangements for the slide switches is attached to the right-hand converter. It consists of a sliding rod with two discs on it that grip the slide-switch arm. The switch links for the power supply and the calibrator are resting in the foreground.

transmitting converter. There also is a jack for injecting the calibrator signal at the input to the r.f. amplifier. It is coupled through only a 0.33 mmf capacitor, thus enabling the calibrator to be left connected without affecting the r.f. input characteristics.

### Construction

The converters are assembled in nickel-plated-steel chassis size  $4\frac{1}{8}'' \times 5\frac{7}{8}'' \times 1\frac{1}{2}''$  high. The antenna connector is an SO-239 u.h.f. type. Phono jacks are provided for other r.f. connections. A supply potential of 18 v.d.c. (@ 40 ma) is obtained through a two-prong Jones plug at the side of the chassis and which mates with a Jones receptacle on the power supply, allowing the two units to be ganged together without interconnecting cables. A small bracket is supplied to mechanically lock the two units together.

### SCC-1 Crystal Calibrator

The SCC-1 V.H.F. Crystal Calibrator provides accurate frequency markers at 50 kc intervals up to 432 mc. It consists of a TIS34 f.e.t. 100 kc crystal oscillator that drives a 2N3394 trigger for an integrated circuit 2:1 frequency divider. High harmonic output is obtained from an i.c. harmonic generator/amplifier.

Four outputs are provided with individual

phono jacks and may be simultaneously connected to separate pieces of gear. One output is peaked for 50 mc, another for 144 mc. The other two allow the calibrator signals to be fed either to a spare converter or directly to the associated receiver. Since the calibrator signals are applied at the input to the converters, frequency calibration therewith takes into consideration both the frequency of the v.h.f. converter's oscillator and the i.f. receiver setting.

The unit is built in a  $3'' \times 4'' \times 1\frac{1}{2}''$  high chassis like that of the converters. It has an on-off slide switch and at one side is an access hole to a trimmer for bringing the crystal on frequency against a standard such as WWV. On another side is a Jones plug for power and mounted on the opposite side is a Jones receptacle that is bridged across the power-input plug. This enables the calibrator to be connected between the power supply and a converter with all three units coupled together as one. Power requirements for the calibrator are 14-18 v.d.c. @ approx. 40 ma.

### CPS-1 Power Supply

The power supply is built on the same size and type chassis as is the calibrator. It furnishes 17.5-15 v.d.c. @ 50-100 ma and operates from a 120 v.a.c., 60-cycle, source using a step-down transformer and silicon-

diode rectifiers in a full-wave bridge with  $R/C$  filtering. Overload protection is provided by a 200 ma fuse in the primary circuit. Power is turned on or off with a slide switch and the d.c. output is fed to a Jones receptacle for mating to plugs on the other units as already described.

### Model CC-1 Console

The Model CC-1 Console consists of a shallow copper-plated chassis with a panel mounted in a  $5\frac{1}{2}$ " H.  $\times$   $10\frac{3}{4}$ " W.  $\times$  8" D. cabinet that has a black scuff-proof finish. Plugs or receptacles allow the converters, calibrator and power supply to be installed in the console when they are placed vertically and pushed in from the rear to mate with the console connectors at the back of the panel.

A unique arrangement is that a mechanical linkage is slipped onto the slide-switch arms of the modules so that they may be operated from the front of the panel, as shown in the photo.

Another feature is that the units may be secured to the console chassis by screws, removed from one side of the individual units prior to installation. Corresponding holes are already provided in the console and the modules. An opening also is furnished for the trimmer-access hole on the calibrator.

Positions are provided for a 6-meter converter, a 2-meter one and a spare. A fourth position holds the power supply and the calibrator which are coupled together.

Interconnecting cables are supplied for the crystal-calibrator outputs and three additional cables for the i.f. outputs of the three converters go to a selector switch on the panel by which any one converter output may be switched to the associated receiver or which bypasses the converters and automatically connects the h.f. communications antenna directly to the receiver. Power for the individual units is likewise transferred by the switch.

Phono jacks are used at the rear for the i.f. output and the h.f. antenna. The v.h.f. antennas are connected directly to each converter, since a separate antenna normally is used for each v.h.f. band.

### Operation and Performance

The converter console makes not only a clean-looking installation, but it also is most desirable from a functional standpoint, especially if you operate more than one band. Switching back and forth between each v.h.f. band or for direct operation with the receiver alone on the lower frequencies is instantaneous.

The mechanical links (operated by push-pull knobs on the panel) to the slide switches of the individual units complete the flexibility of the setup, also allowing the converter crystals to be switched or the calibrator to be turned on or off.

As to performance, the converters measured according to the related specifications which follow, except where otherwise noted in parenthesis:

**SC-2**—Noise Figure: Rated 2.5 db (measured 2.8 db). Image Rejection: 70 db @ 115 mc. I.F. Rejection at 14 mc: Rated 80 db (measured 95 db). Gain: 20 db.

**SC-6**—Noise Figure: 4.0 db. Image Rejection: Rated 75 db @ 22 mc (measured 81 db). I.F. Rejection: Rated 80 db (measured 86 db). Gain: 14 db  $\pm$  0.5 db across band.

The sensitivity is not rated, due to possible variations according to receiver bandwidths, but readings taken with the SC-6 were as follows: 0.1  $\mu$ v for 10 db S+N/N on c.w. and s.s.b. using receiver bandwidth of 2.1 kc; 0.25  $\mu$ v for 10 db S+N/N on a.m. with 30% 400 c.p.s. modulation and using receiver bandwidth of 4 kc.

A sensitivity test was not made on the SC-2, but according to the noise figure, it should be slightly better than with the SC-6 under the

[Continued on page 110]

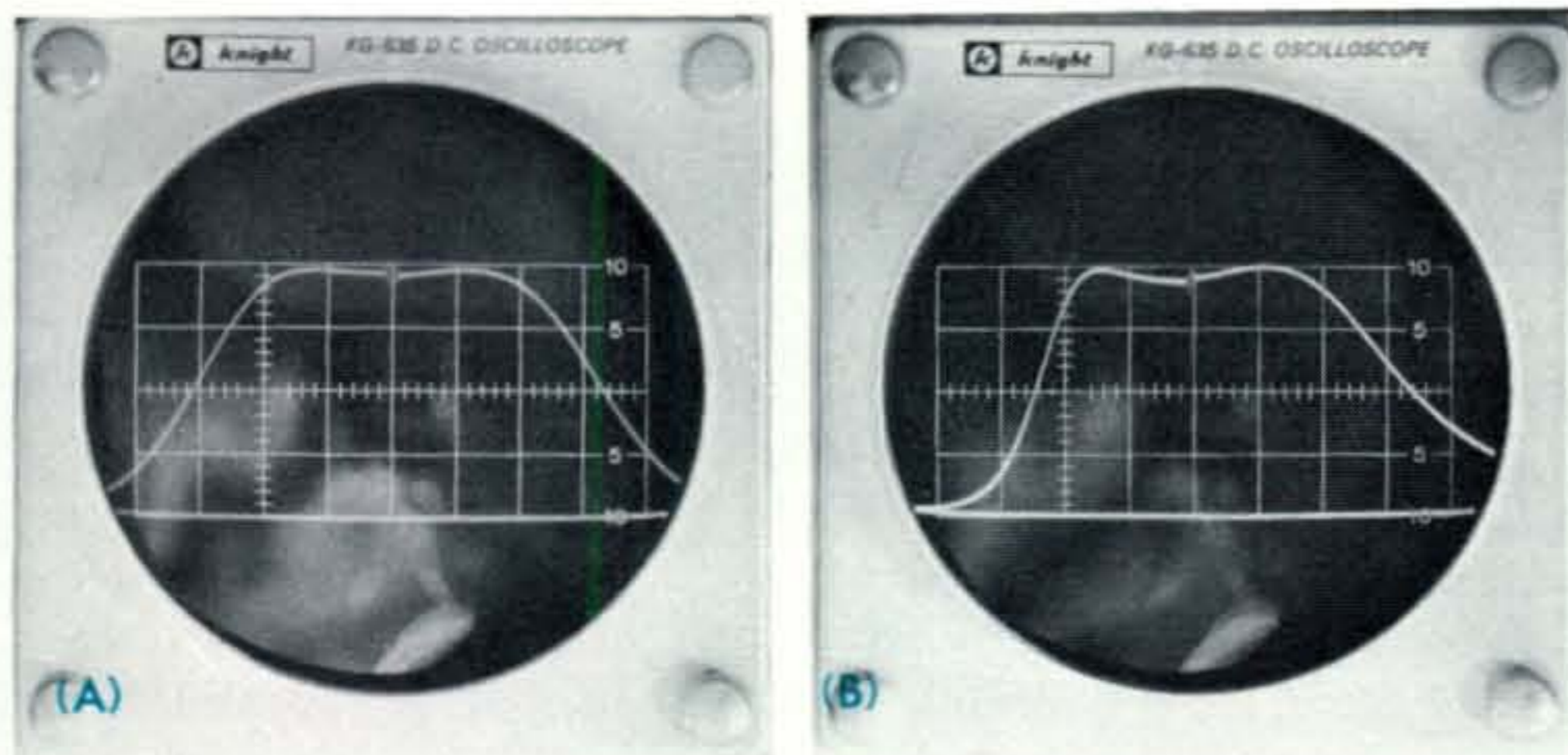


Fig. 2—Sweep-generator display on c.r.t. showing band-pass characteristics of the SC-6 at (A), the SC-2 at (B). The major horizontal-scale divisions are 1 mc apart. The vertical scale is linear with respect to voltage. The band edges and the band center (indicated by the marker pip) are less than 1 db below maximum for a response of better than  $\pm 0.5$  db over the entire 4 mc bandwidth.

# HOW LINEAR IS A LINEAR AMPLIFIER?

BY JOHN J. SCHULTZ, \*W2EEY/1

Many terms can be used to measure the performance of s.s.b. exciters and linear amplifiers. One of the most useful terms available to measure performance is Intermodulation Distortion or i.m.d. Unfortunately, the i.m.d. is rarely given for most amateur equipment.

**T**HE terms carrier suppression and sideband suppression are familiar to everyone who works with s.s.b. gear. The objective is to produce as great carrier and unwanted

\* 40 Rossie Street, Mystic, Connecticut 06355.

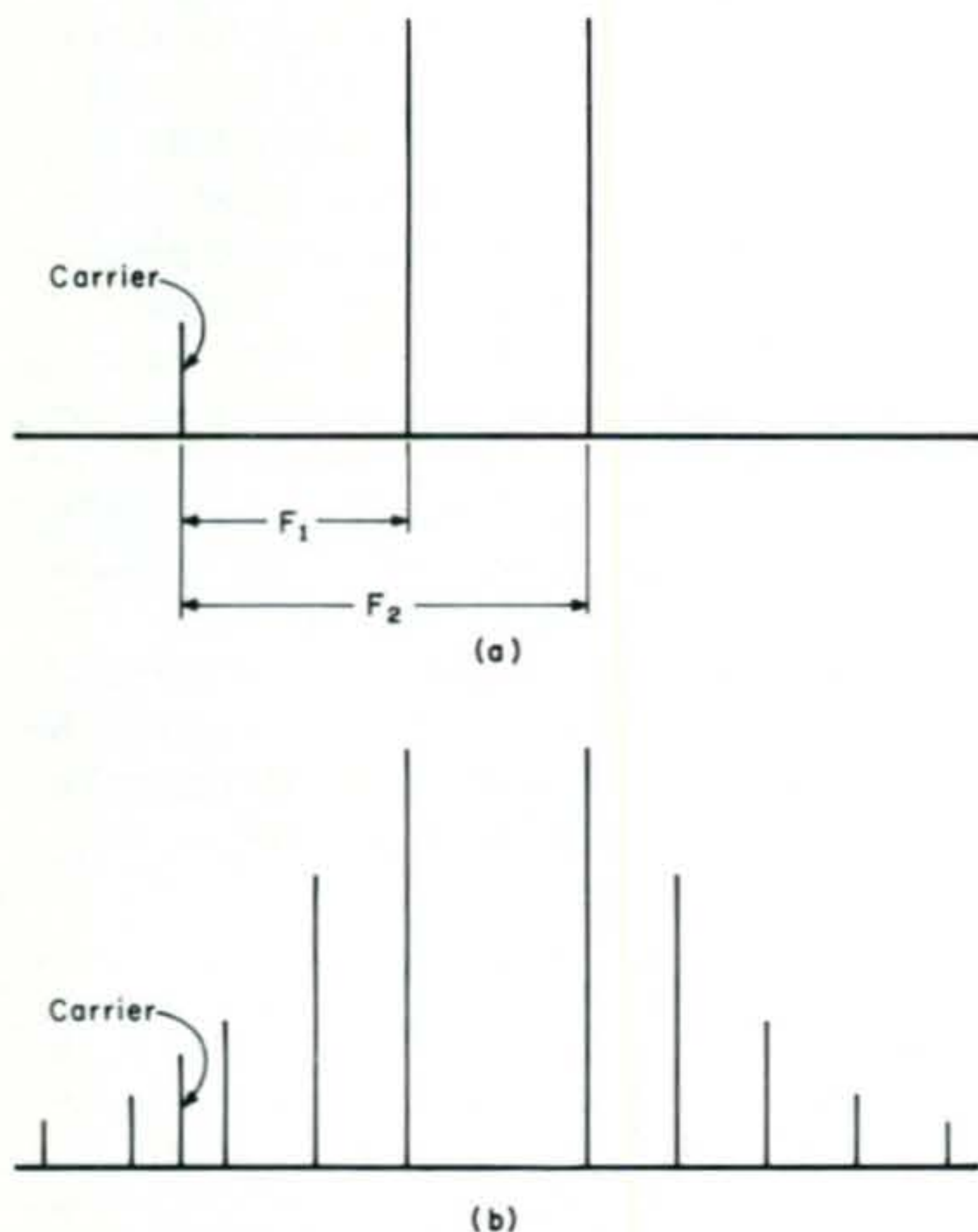


Fig. 1—Perfect linear fed two-tone signal would have output as at (A) containing only original two frequencies, each displaced from carrier by its frequency. Practical exciter or amplifier contains many more output frequencies (B).

sideband suppression as possible, with  $-40$  to  $-50$  db for both being easily achieved with most circuits in use. However, one of the most interesting terms of measurement of the actual *linearity* of a s.s.b. transmitter or linear amplifier, Intermodulation Distortion, is rarely quoted by either manufacturers of amateur equipment or by most amateur builders. There may be good excuse for the latter group since they may not have the equipment available to measure i.m.d. while carrier and sideband suppression is relatively easily measured. However, there is no reason why manufacturers cannot quote i.m.d.; they probably don't do so because most amateurs aren't acquainted with the term.

I.m.d. is quoted very carefully for commercial and military s.s.b. equipment sales, however. The purpose of this article is to explain the importance of i.m.d. and how it can be measured. Even if one doesn't have the equipment to measure i.m.d., understanding the term is useful and provides the amateur with another important factor to be used in comparing the relative worth of different pieces of equipment.

## Linearity and I.M.D.

Non-linearity in the operation of s.s.b. stages can be due to many causes: improper bias operating point, poor voltage regulation, overdrive, improper loading conditions, etc. No amplifier stage or linear amplifier is

perfect and the result is that all produce some distortion to the input signal. Intermodulation distortion is a term that is used to measure the extent of this distortion or, put another way, it gives a quantitative means of knowing how linear a linear stage really is when operating at its rated power level. If a stage were perfectly linear, one would obtain an amplified output that is a exact reproduction of the input signal. A tone of 1,000 cycles/second would be reproduced as a pure 1,000 cycle/second tone and if two tones or more of different frequencies were amplified, the output would contain only the original or input frequency tones.

In practice, however, when two or more tones of different frequencies are fed into a linear, the output contains frequencies that were not present in the input signal. These additional tones in the output are due to intermodulation distortion which is a function of the linearity of the stage. Figure 1 shows the frequency spectrum display of an ideal and a practical linear both driven from a two-tone source.

Speech, of course, is a complex waveform of multiple frequencies. High levels of i.m.d. simply create other output frequencies which serve no useful function in conveying the original desired intelligence. How much distortion can be tolerated and still not affect intelligibility is a complicated question. The human ear can accept a signal with a great deal of distortion and still process it to make it intelligible partly because our brain uses its knowledge of language to logically fill in distorted sounds or even whole words. Without this knowledge of language, far less distortion in a signal can be tolerated and still produce reasonable intelligibility. Also, under poor signal conditions, QSB, QRM, etc., an amplifier with high distortion will give poorer service than one with low distortion.

Other important reasons for keeping i.m.d. low is that high distortion simply clutters up the bands with useless signals thus causing QRM and the transmitter power which is necessary to create the distortion products could more profitably be used to amplify the original input signal.

### I.M.D. Levels

I.m.d. level is usually stated in terms of how far below the level of the original tone signal a spurious tone signal is measureable. Unless very unusual conditions exist, the spurious tone signal nearest the original tone

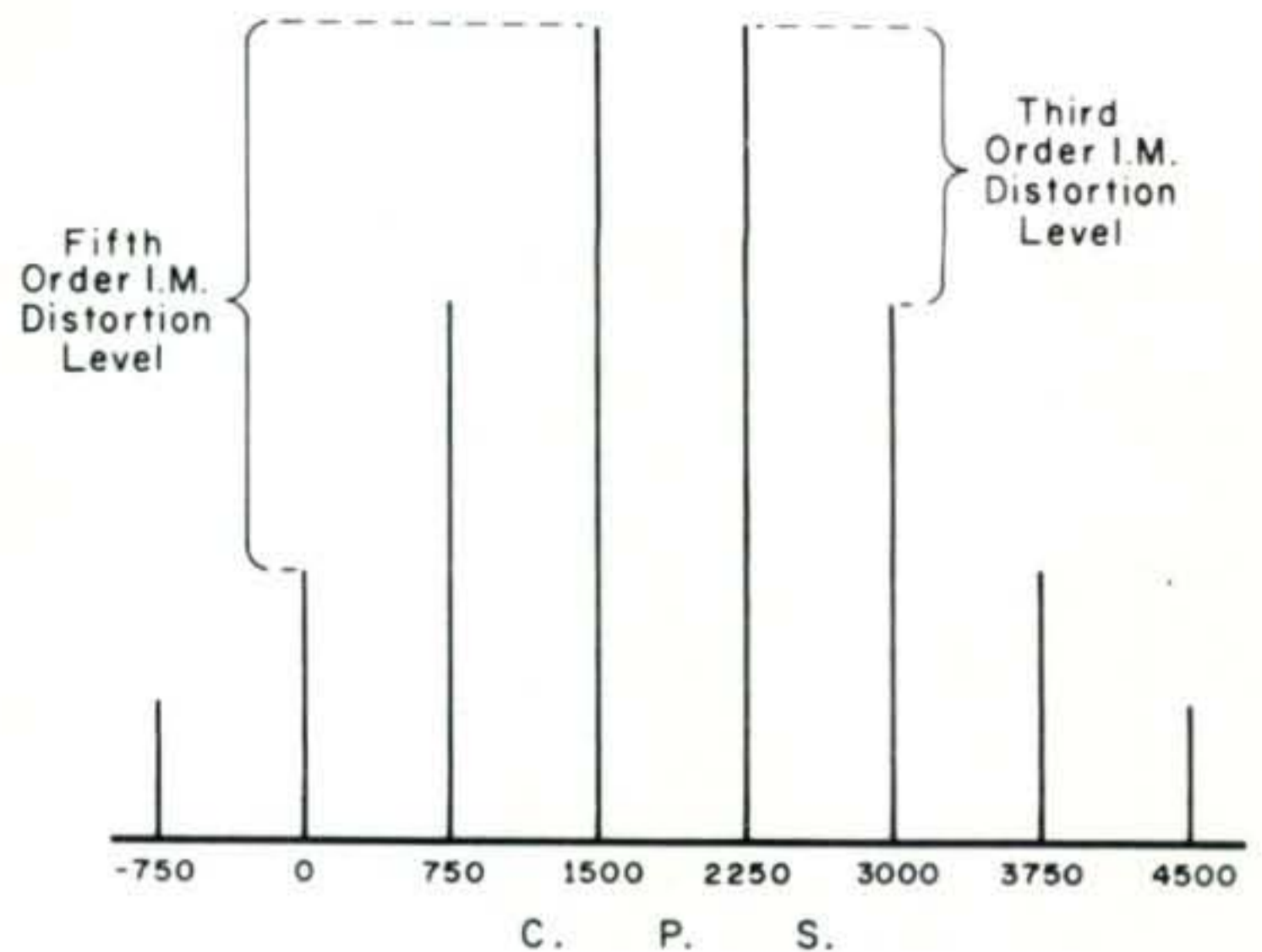


Fig. 2—Two-tone test signal of 1500 and 2250 c.p.s. produces distortion frequencies as shown. Carrier frequency is added to above frequencies to obtain r.f. output frequencies.

signal will be the greatest in amplitude while the succeeding tone signals will be progressively lower in amplitude. Therefore, i.m.d. is sometimes stated in terms of the level of the first spurious signal or sometimes in terms of the level of the first two spurious tones. The amplitude must be quoted with the amplifier operating at its rated input.

A  $-35$  to  $-45$  db level for the first spurious tone is considered a generally reasonable standard for most commercial and military voice communications s.s.b. exciters and amplifiers. Higher quality systems strive to reduce i.m.d. even further, with specialized military systems aiming for a  $-80$  db or more value. Manufactured amateur equipment varies widely with some gear having a level of  $-20$  to  $-25$  db which is probably the lowest that should be considered acceptable. It should be noted that i.m.d. can be quoted for a single stage if desired, however, the most useful figure for an s.s.b. transmitter is the overall i.m.d. Feedback or automatic load control systems serve to reduce severe i.m.d. and the figure should also be measured with these features in operation.

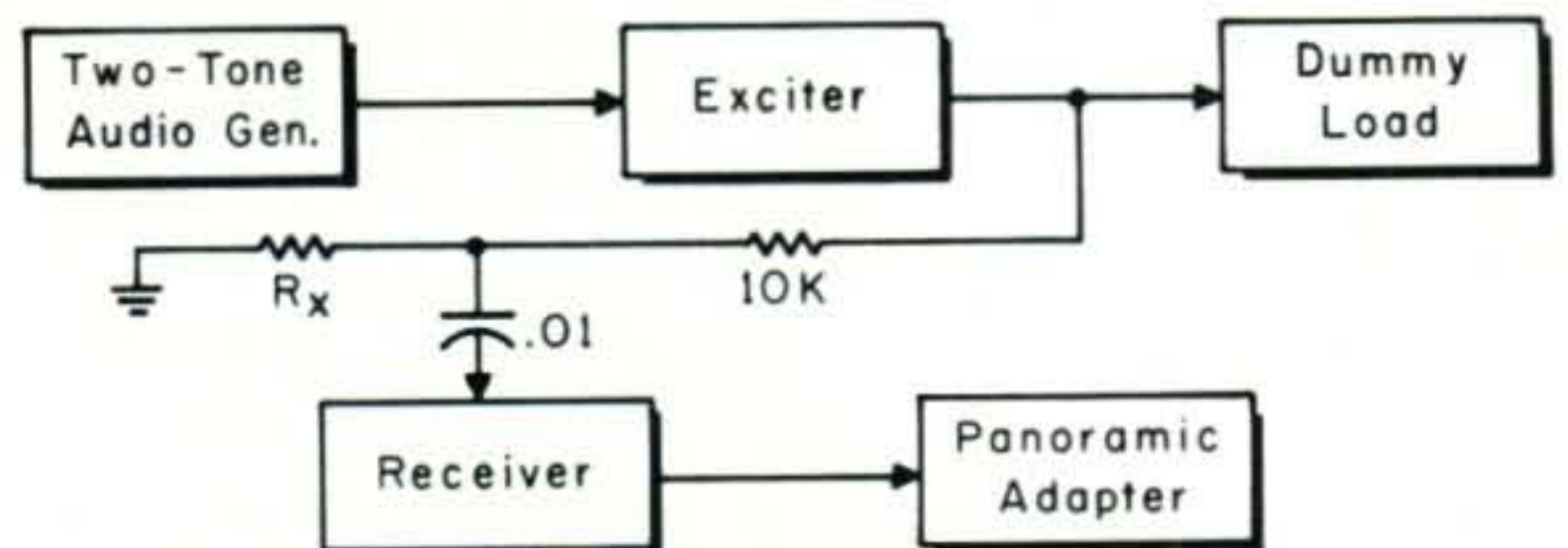


Fig. 3—I.m.d. test setup. Receiver must be isolated from exciter signal other than by direct r.f. connection shown. The value of  $R_x$  is selected to produce a signal that will not overload the receiver.

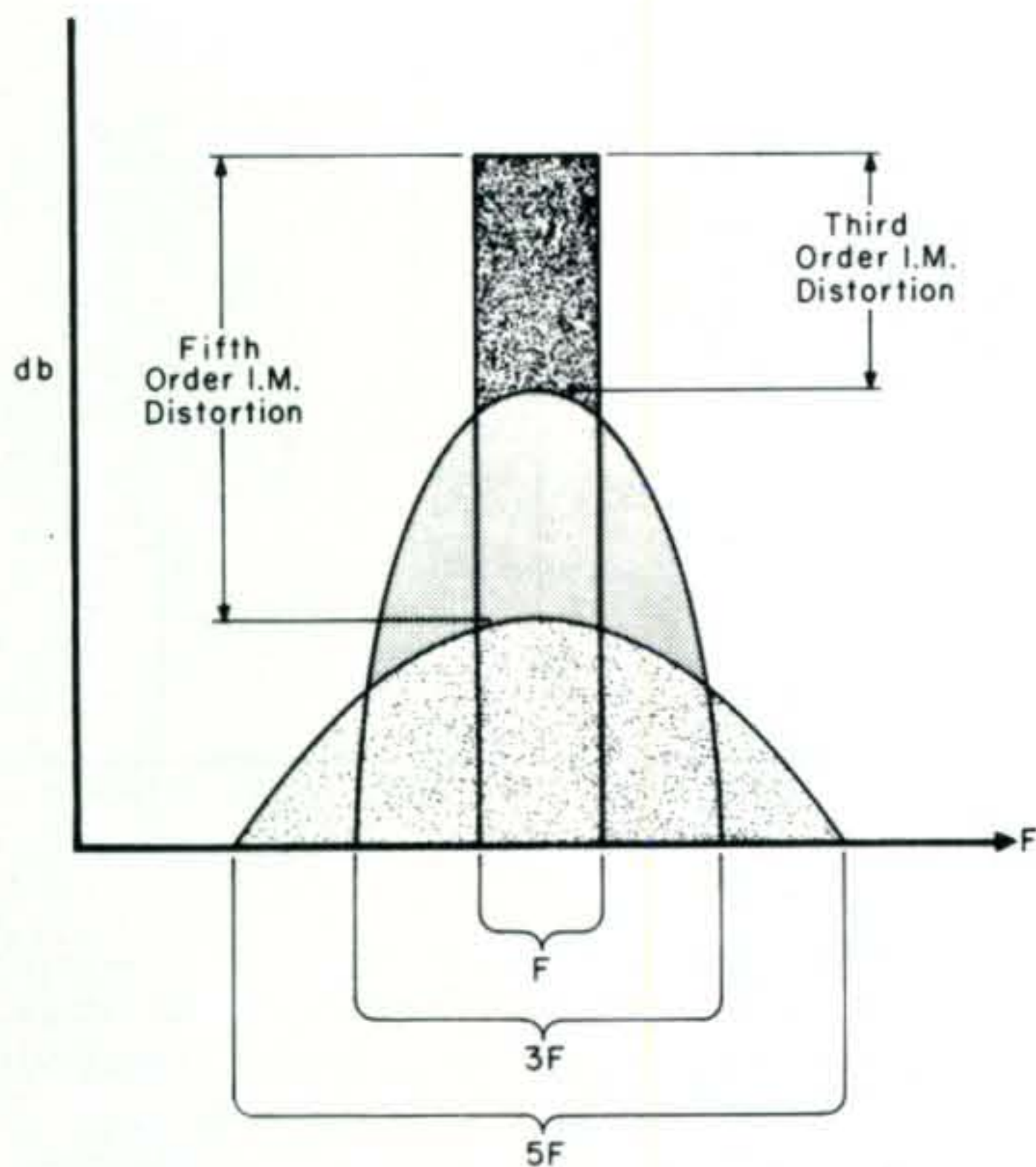


Fig. 4—Using audio bandpass limited noise signal at input, output frequency display is as shown.

### Measurement of I.M.D.

In order to measure distortion signals one has to, in a sense, first create them. The standard two-tone test procedure has probably become the most accepted way to perform the measurement. One test tone is not usable since i.m.d. signals will not be created and the use of more than two tones makes for the creation of so many spurious signals that measurement of individual frequencies becomes very difficult. Any two equal amplitude test tones can be used but some frequency relationships will produce harmonics that may obscure i.m.d. signals. Therefore, two tones are usually used that have a 3 to 5 frequency ratio (1500 to 2250 c.p.s., for example). The resulting i.m.d. products are all odd order, as shown in Fig. 2. The first spurious tone, on either side of the two original tones, is the 3rd order product and is equal to twice the frequency of one tone, minus the frequency of the other tone. The next signals are the 5th order products and are equal to three times the frequency of one tone minus twice the frequency of the other tone. Generally only the 3rd and 5th order products are of interest and significance.

Figure 3 shows a test setup for measuring i.m.d. when a spectrum analyzer or receiver panoramic adapter is available. Since the analyzer and receiver or panoramic adapter can themselves produce i.m.d. on their input signals, it is necessary to know their approximately i.m.d. level. Generally, it will be low,

particularly for analyzers. However, some allowance should still be made. If the analyzer or adapter has an i.m.d. of  $-45$  db, measurements of i.m.d. around the  $-40$  db level can be expected to be in error by about 2 db. It is also important that there be no intercoupling between the two oscillators that produce the two-tone test signal and that each tone be of low harmonic content. An oscilloscope check should be made of the output waveform to ascertain this.

When viewing the oscilloscope display on an analyzer or panoramic adapter, other spurious displays besides i.m.d. may be seen on either side of the carrier frequency due to incidental modulation (power supply ripple, mechanical vibration, etc.). Since the input frequencies are known, one can calculate where to expect the i.m.d. products to appear. Also the individual audio tones can be individually switched on and off to identify their distortion products. Of course, if other spurious displays obscure the i.m.d. frequencies it may well be that other difficulties deserve attention first.

The value of the 3rd and 5th order products below the two tone level can be read directly from a calibrated display. The selectivity, sweep width and sweep speed on the display unit are varied to obtain the best pattern. One should check that different sweep speeds do not change the signal amplitude relationships. Also, the input signal should be varied to be sure that the signal relationships do not vary because of overloading the display unit.

### Receiver Method

If one does not have a panoramic display unit but a well calibrated and sharply selective receiver, it can be used to tune to each of the frequencies as would be displayed on a spectrum view. The selectivity must be sharp enough to separate individual frequencies down to at least the  $-40$  to  $-60$  db level on the i.f. response. If the receiver "S" meter is used to measure relative single frequency strengths, its calibration must be known. Also, the measurements should be made at different input levels to preclude overload and comparative signal amplitude ratio distortion.

Another receiver method would be to use audio selectivity on the output of the receiver rather than i.f. selectivity to separate individual input frequencies. With a two-tone generator of specific frequencies, one could build audio filters to just pass the 3rd order

i.m.d. products and, therefore, have an easy means with a receiver to check how adjustments affect i.m.d. The precautions concerning receiver overload must, of course, still be observed and the receiver operated without a.v.c. action.

### Noise Measurement Method

Still another, but less frequently used, i.m.d. measurement technique tries to stimulate actual voice frequency input conditions. Instead of a two-tone test signal, a noise generator is fed through a bandpass filter (with a flat response within the voice frequency band and with sharp attenuation outside this band) and into the transmitter input. A receiver is used as a measurement device and uses three filters of identical characteristics. One filter passes only the transmitter audio bandwidth and the others pass frequencies outside the audio bandwidth. The transmitter audio bandwidth filter output is used as a reference and the other filter outputs indicate the 3rd and 5th order i.m.d. levels. This method works because the noise input produces an output spectrum as shown in fig. 4. All the 3rd order distortion products will appear in a bandwidth equal to three times the transmitted noise bandwidth, 5th order products in a bandwidth equal to 5 times the noise bandwidth, etc.

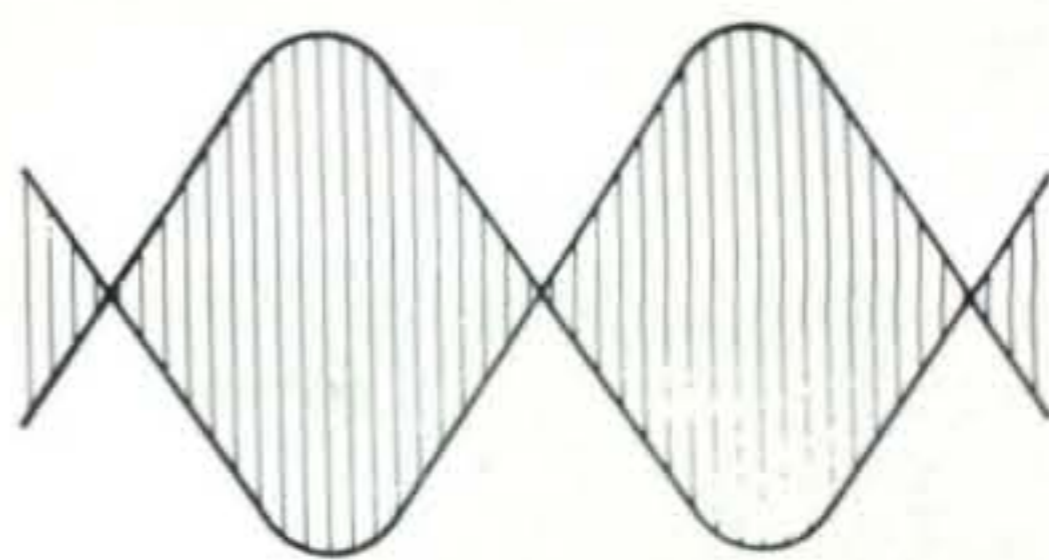


Fig. 5—Conventional two-tone signal input oscilloscope display to check linearity is useful for adjustment but provides no measure of degree of non-linearity.

### Summary

It is seen that the foregoing tests, particularly the well-known two-tone test, are linearity checks. But, as was mentioned before, i.m.d. gives a quantitative measure of how linear an amplifier really is in operation. If a two-tone test is used to produce the normal oscilloscope test pattern of fig. 5, non-linearity can be noted in various ways but there is no way to express the *degree* of non-linearity or to accurately compare different amplifiers.

Most amateurs will probably never make any i.m.d. measurements but understanding the term helps to better evaluate s.s.b. equipment. When someone next says that an amplifier is really "linear", why not ask him how linear? ■

## R.S.G.B. "London Festival" Station, GB2LO

**J**ULY 8-20, marks the dates of the 1968 City of London Festival. To help commemorate the event, the Radio Society of Great Britain will have a station (GB2LO) operating at the *Daily Mirror* Building, Holborn, London, E.C.1.

This location, within the 1.03 square miles of the City of London, is about 200 yards from the premises at 107 Hatton Garden, where some of the earliest meetings of the R.S.G.B. were held during the summer of 1913, when the group was called the London Wireless Club.

World-wide contacts are anticipated, especially one scheduled with VE3LON, the Exhibition Station callsign for the London (Ontario) "Fortnight Festival," whose theme is "The British Are Coming!"

GB2LO will be on view to the public and visitors are invited to visit.

(Tnx Sylvia Margolis)



The *Daily Mirror* Building where the R.S.G.B. station, GB2LO will be located. (*Daily Mirror* photograph)



GM3BST receives Nimbus weather satellite photo at his home in Stranraer, Scotland.



A bulletin board serves as plotting board for satellite passes.

## GM3BST Rides Nimbus To US



Working with this home-brew Az-El-mounted antenna system, GM3BST regularly copies Nimbus signals.

In recognition of his state-of-the-art in receiving weather pictures from the built Nimbus weather satellite, a CQ was recently treated to an 18-day tour of Cape Kennedy, Washington, D.C., Los Angeles, San Francisco, Philadelphia and New York. John B. Tuke, GM3BST of Stranraer, Scotland, was the lucky fellow who, with wife, was flown through the lightning courtesy of GE, and met with several Space Program officials in Washington, D.C., as well as being commended personally by Vice-President Hubert H. Humphrey on his achievements. Also highlighting the six-city visit was his first-view of the launch of Nimbus B from Vandenberg Air Force Base in California.



Vice President Hubert H. Humphrey congratulated Mr. John B. Tuke of Stranraer, Scotland, for his achievement of constructing a ground-monitoring station to receive weather photos transmitted by Nimbus II. Looking on are Mrs. Tuke and Mr. L. E. Daley Davis, Vice-President and General Manager of GE's Defense Program Division. (Photos courtesy of Dee Logan, GE).



# IMPROVED F.M. OPERATION

BY DAVID J. GOODMAN, \*WA8UIT

*Proper maintenance of two way f.m. equipment can improve the number of contacts in mobile operation.*

**N**OT everybody operating amateur f.m. is in the two-way radio business. (It just seems that way!) It's well known that those who do work with mobile radio as a part of their job usually have enough knowledge of commercial two-way equipment to assure that their amateur f.m. gear is in proper working order. But, what about those of us who never got closer to f.m. mobile equipment than the back seat of a taxi, until deciding to go amateur f.m.?

The truth is that f.m. two-way equipment is pretty strange to a lot of fellows; even those who have been active hams for years. The f.m. transmitters are generally easily understood, and being a comparatively simple device, they give the average ham little trouble. He can easily tell if he is getting the proper output, he can tune the transmitter, and in general, he knows what to do to make it work properly.

## The Receiver

Unfortunately, the f.m. receiver is another story. Comparatively few amateurs have ever had much experience in critical receiver alignment, since no other popular amateur operating mode requires the ham to understand his receiver and to have to fiddle as intimately with its total alignment as does f.m.

The result of this situation is a transmitter that works, a receiver that doesn't and an apologizing operator. Time after time, the writer, along with other local stations, has responded to mobiles who were on their way through town, asking for a contact. Enough r.f. is heaped upon these fellows to cook a

turkey, but alas, comes back the typical reply, "Sorry, Old Man, can't get your call there. We'll have to make it another time. Don't think this receiver is working quite right."

The answer to this situation is not difficult, if we consider how the receiver got sick in the first place. Most f.m. gear being operated by hams today is obsolete commercially manufactured equipment that is between 10 and 20 years old. If it's mobile equipment, the chances are good that it has been in and out of perhaps as many as 15 different vehicles and has been worked on by scores of different people. It may have come directly out of service to the ham, or it might have been obtained from another ham who used it himself. In any case, since its ancestry and health history are unknown, the safest approach is pure skepticism. "The equipment is presumed to be in as bad a condition as possible until proved otherwise," should be your motto. There is no reason to assume that those who worked on your unit left it in good order, even if it came right from commercial service, so you can be skeptical in that case, too.

We are going to discuss some of the steps to be taken to insure that a receiver is doing the job that it should be. The references are based on experiences with equipment for 2 meters f.m., but the techniques are directly applicable to 6 meter gear, as well.

## Tubes

It's commonly known that close to 99% of the trouble in tube-type electronic equipment is the result of tube faults. The typical high band receiver has about 16 tubes, so it is mandatory to make sure that all the tubes are in satisfactory condition. This should be done

\* 3305 DeSota Avenue, Cleveland Heights, Ohio 44118.

before ever applying power for the first time. Test every tube in a dynamic mutual conductance tube tester. Test carefully for intermittent shorts and observe the emission level. Be critical. If a tube is marginal, shows a partial or solid short, or its emission falls off, throw it away. You might end up needing six or eight new tubes. If this shocks you, remember that our objective is *a receiver that works properly*. If you are going to replace tubes with spares from your junk box, test the spares, too. Be sure that all the tube types agree with the labels on the chassis for each socket. If a late-number tube has been substituted for the original, check to see that it is a compatible substitution.

### The Relay

One thing that we are going to suspect right off the bat and are not even going to give a chance to prove its innocence is that nefarious malperformer, the antenna relay. This ghastly mechanical contrivance, ridiculously simple though it be, is subject to continuous use and because it carries respectable current and voltage, it arcs, pits, attracts dirt, gets tired physically, *etc.* Because it exists under these conditions, it very often ends up doing a pretty poor job of conducting r.f. in and out of your set, by the time you become owner. Receiving losses of up to 20 db, for example, due solely to antenna relay trouble, are not at all unusual. To insure yourself against having later trouble with the relay, burnish the contacts carefully with a relay burnishing tool. If you don't have a tool, use white bond paper strips. Insert the paper between each contact and the transfer leaf, compress the leaf gently and work the paper in and out until no residue is visible when using a clean paper. Check the relay for correct overtravel in both the operated and unoperated positions. If necessary, adjust. Do this same cleaning and inspection job on the transmit-receive relay, as well. This relay contains the receiver B plus continuity contacts and often contributes to low B plus as a result of poor conductivity in these contacts. (In some sets, the antenna and power switching is combined on one relay).

### Tuning And Alignment

Next, we must make sure that the receiver front end will really tune into the ham band. In the case of high band equipment, many receivers will not tune down from their intended 150 mc range to 146 mc without modi-

fication. But the unsuspecting ham, observing what he thinks is a peak when adjusting the stages of the receiver which operate at channel frequency, is, in reality, seeing the drop-off as the slug passes out of the coil, *without ever reaching resonance*. This probably accounts for more sick receivers on 2 meters f.m. than any other single cause. A grid-dip meter check of each tuned circuit that operates at channel frequency will resolve your doubts on this issue. It's usually a simple matter to add 2 mmf or so of capacity across a coil externally, where needed, to bring the can down onto the ham band.

Precise alignment of the receiver is paramount for correct operation, and it is the next step. Correct alignment of commercial f.m. two-way receivers can be bothersome without having the benefit of proper test equipment, but it is possible. In receivers having a fixed low i.f. filter, the discriminator and the i.f. chain must be tuned with a precisely accurate signal source. The BC-221 frequency meter, loosely coupled just ahead of the stage being adjusted, will do this job quite well. The BC-221 is superior to most signal generators that the average ham may have at his disposal because of its accurate dial setting capabilities and its relative freedom from drift. The signal level can be kept below saturation by adjusting the coupling. The same procedure can also be used for alignment of the high i.f. and the front end of the receiver, even on 2 meters. A rough tuning of the front end may first have to be made with a local transmitter serving as the signal source, in order to get an ample amount of signal. After this has been done, there should be sufficient sensitivity in a healthy high band receiver to allow a harmonic from the BC-221 (set at around 14.6 mc) to quiet the receiver when applied at the antenna input. For a final alignment of the front end, the frequency setting of the BC-221 should be adjusted to match the discriminator reading of a signal from a transmitter known to be on-channel, and the front end stages re-peaked.

### Power Supply

If the receiver is to be used in a mobile installation, the power supply must be checked as the next step. Vibrators have disappointingly short lives, so we'll want to make sure that the one that came in the set can be trusted. A partial test of its condition may be made by simply checking the receiver

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### Preamplifiers

Let's assume that your receiver has now passed all the tests and is as sensitive as the day it left the factory. Have you done everything you can to insure good reception? No; because the day your receiver left the factory was a long time ago, and a great deal of progress has been made in the state-of-the-art since then. At the time your receiver was made (if it's high band) the classic first r.f. amplifier tube was the 6AK5. It's a reliable tube, but it suffers from having a high noise figure. That is, because of certain structural considerations, it continuously generates noise internally. So, while it is amplifying an incoming signal, it is also amplifying its internal noise. If the incoming signal is greater than the 6AK5's internal noise, it will be amplified and detected. But, if the tube's internal noise level is greater than the signal, the noise will mask the signal and you'll never know it was there. A 6AK5 has a noise figure of about 10.5 db, at 144 mc.

In the 1950's, the introduction of the Nu-visitor was a big step in the development of low noise v.h.f. amplifiers. Nominal noise figures for Nuvistors are on the order of 2.5 db. But the last five years have really seen a breakthrough in v.h.f. amplifiers with the availability of a host of inexpensive bipolar and field effect transistors (f.e.t.'s) having noise figures of around 1.5 db at 144 mc.

A look at fig. 1 will help to understand the relationship between the noise figure of the first r.f. amplifier in a receiver, and its sensitivity. In the pictured example, there is a given signal with strength greater than the internal noise level of an f.e.t., but below that of the noise levels of both a Nuvistor and a 6AK5. In this case, we can expect the signal to be amplified and detected if the f.e.t. is serving as our first amplifier device, but it will never be heard if a Nuvistor or a 6AK5 is used. From this, it is easy to see the vast improvement in weak signal detection that can be obtained by substituting a low noise figure f.e.t. for a 6AK5 first r.f. amplifier.

The easiest way to make this substitution

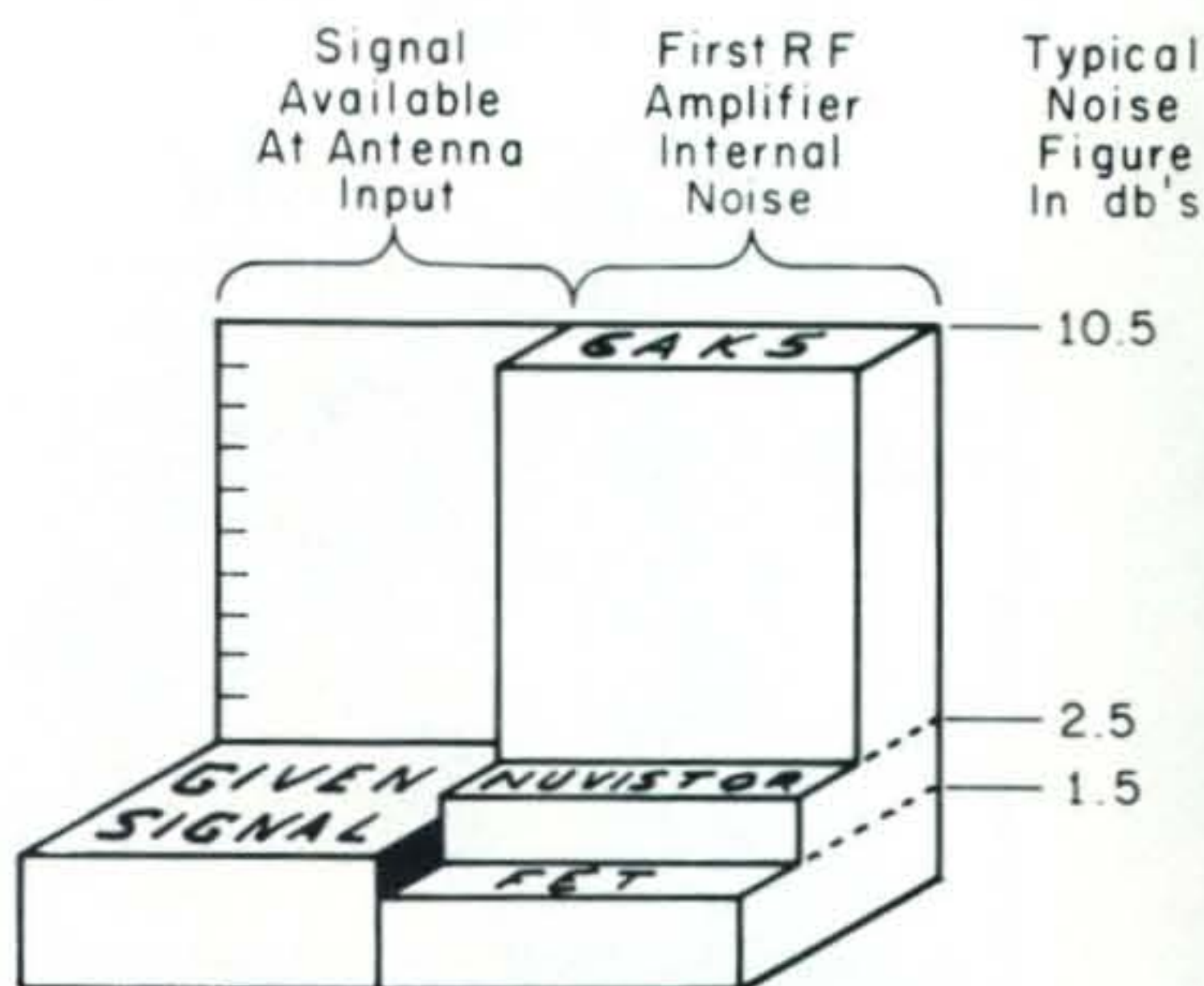


Fig. 1—Relationship between the noise figure, receiver sensitivity and the various r.f. amplifiers discussed in the text.

is to add an f.e.t. preamplifier between the antenna relay of your set and the antenna input jack on the receiver. The current literature is filled with simple f.e.t. preamp circuits for 144 mc that you can easily build. Usually, a single transistor is all that is needed, as only enough gain to overcome the noise of the original first r.f. amplifier tube (most likely a 6AK5) is required; 15 to 18 db ought to do it. If you are not a builder, such a preamp can be purchased, ready to go, for around \$12.00.

### Antenna Feedlines

While of interest mainly to the operators of fixed stations, perhaps a word should be said about antenna feedline, as it affects the reception of signals. For the benefit of those v.h.f.-f.m. newcomers who are refugees from the "low bands" (and there are more of these converts every day) it should be pointed out that feedline considerations that could be treated casually below 10 meters become absolutely critical at 146 mc. The two most important of these factors are directly related; attenuation and length.

The two types of 50 ohm coax that are best known to the ham are RG-8/U and RG-58/U. The published attenuation figures show that RG-8/U has a loss of 2.1 db per 100 feet at 100 mc, while RG-58/U has a loss of 4.2 db under the same conditions. A lot of operators give these figures little attention and, because they have a length of RG-58/U around, or because it's cheaper, they use, say, 100 feet of it in their 2 meter feedline. Doing so means a loss equal to more than 1/2 the power. Even this fact doesn't

[Continued on page 101]

# SOLID STATE COUPLING METHODS

BY JOSEPH TARTAS, \*W2YKT

*The whys and wherefore of coupling circuits in solid state i.f. amplifier design.*

**A**BOUT seven years ago, I made a prediction in some material I was writing about TV servicing, that, "Undoubtedly transistors will eventually replace tubes in all of the TV circuits but the c.r.t. itself." Not only has this prediction come true, but at some future date, this may well be remembered, not as the Space Age, but as the *Semiconductor Age*. Each new development in the transistor line presents a different problem to the circuit designer; the bi-polar transistor, the f.e.t. and the i.c.

As the usable frequency spirals upwards, the input and output circuits must be altered to compensate for different input and output impedances. Input, output and feedback capacitances (by whatever the name) and methods of coupling to achieve the desired gain and bandpass characteristics also change.

## Comparison To Vacuum Tube I.F. Circuits

The transistor has been considered as essentially a current amplifier. As an i.f. amplifier, however, its sole purpose is to pro-

vide a sufficiently high *voltage* level at the detector input. It may be regarded, except for the considerations to follow, to be similar to vacuum tube voltage amplifier circuits.

Tubes have relatively high input *and* output impedances. Bi-polar transistors, in the more useful configurations, have *high output* impedances (although considerably lower than that of tubes) but, unfortunately, have quite low input impedances. F.e.t.'s on the other hand, have semiconductor characteristics, but with impedances higher even than vacuum tubes.

Because the transistor is basically a power amplifier, the maximum transfer of power occurs when the coupling network is matched, both to the output of one stage and input of the next stage. In addition to impedance matching, the resonant frequency of any tuned circuit connected to the transistor must be considered. The output capacity of most transistors is low, but the input capacity is often higher than those of tubes, as much as 30 mmf in some types. These capacities must be considered since they are part of the total tuning capacity across the coils in i.f. amplifiers.

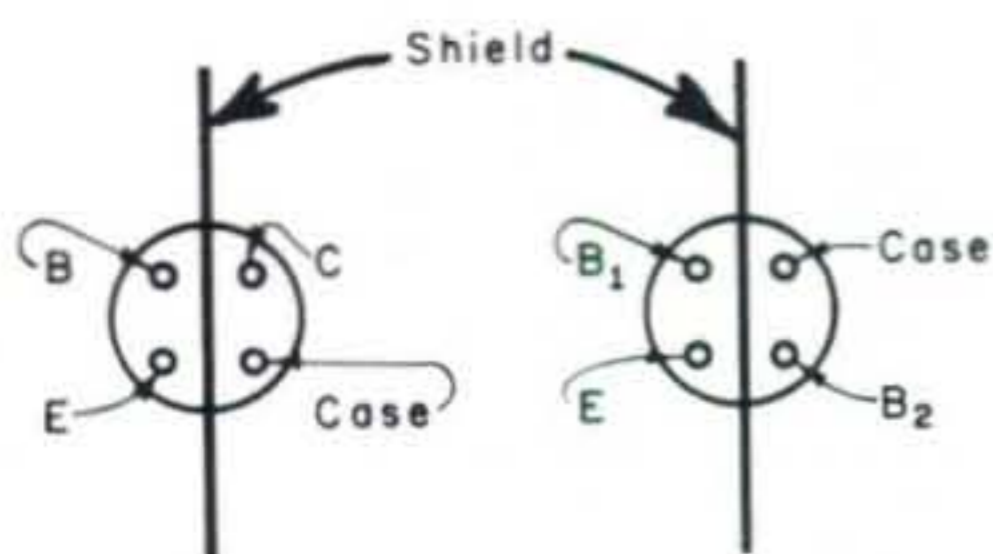


Fig. 1—Basing diagrams of most transistors are alike except for the ground lead or the extra base connection in the tetrode.

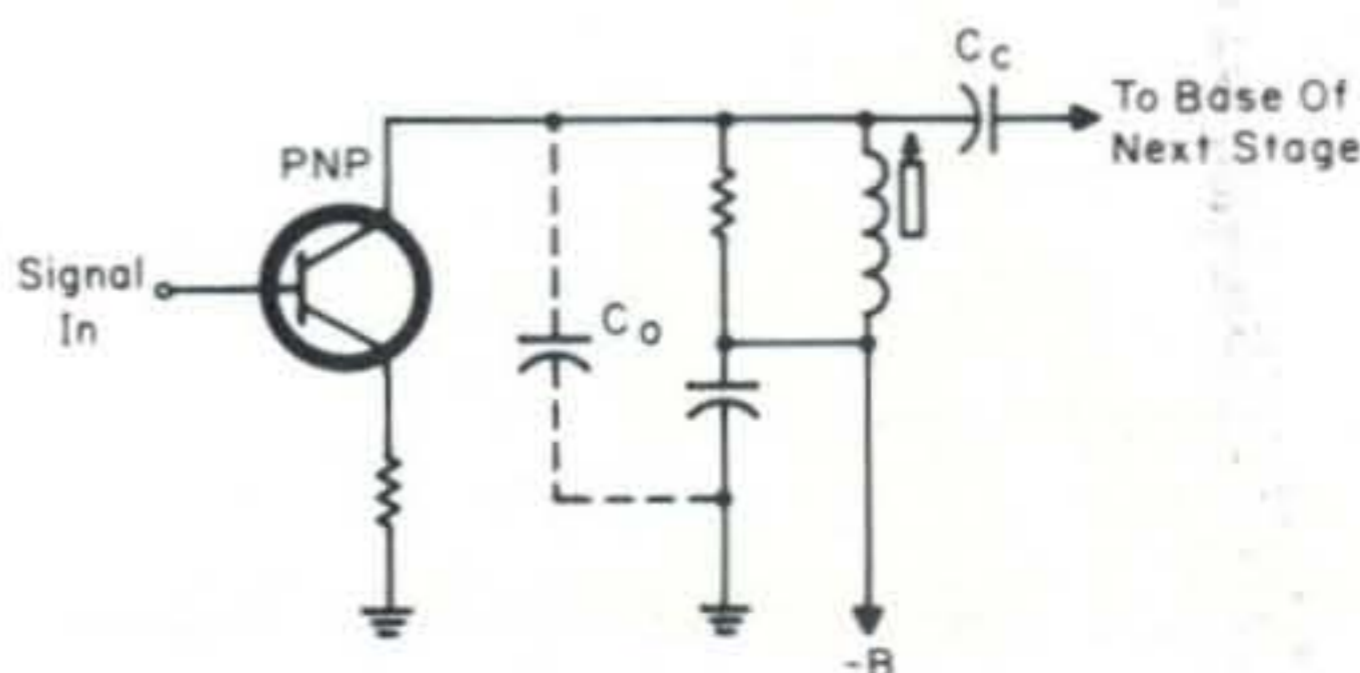


Fig. 2—Output circuit of a transistor i.f. stage. The output capacity is identified as C<sub>o</sub>.

At Resonance:  
 $X_L = 2\pi FL = X_C = \frac{1}{2\pi FC}$   
 Unloaded  $Q = X_L/R = X_C/R$   
 $Z_{Resonance} = X_C I_C / I_G = X_L I_L / I_G$   
 $Z_{Resonance} = QX_L = QX_C$

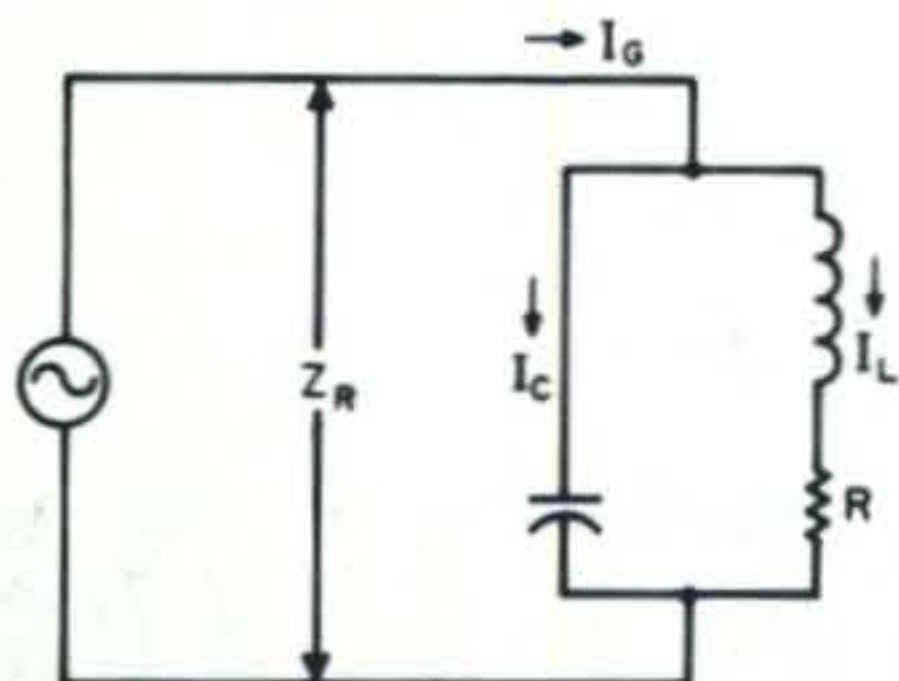


Fig. 3—A parallel tuned circuit and its various current, voltage and impedance relationships.

Of the three possible circuit configurations, common-base, common-emitter, and common-collector, the common-emitter circuit is almost exclusively used for i.f. circuitry. It is the common emitter circuit that produces a high voltage gain as well as the greatest power gain of the three configurations. Another advantage in using the common emitter circuit is the possibility of isolation due to the physical layout of the transistor terminals. Reference to fig. 1 shows that a shield partition may be used to completely isolate the input circuit consisting of the base circuit (which is also the collector or output circuit if another stage precedes it) and the emitter circuit, from the output, or collector circuit. In tetrode transistors the additional lead does not prevent use of the shield, but also provides a separate element for a.g.c. control that is completely isolated from the active r.f. circuit elements.

Until recently, the collector of a triode transistor was tied to the case and presented

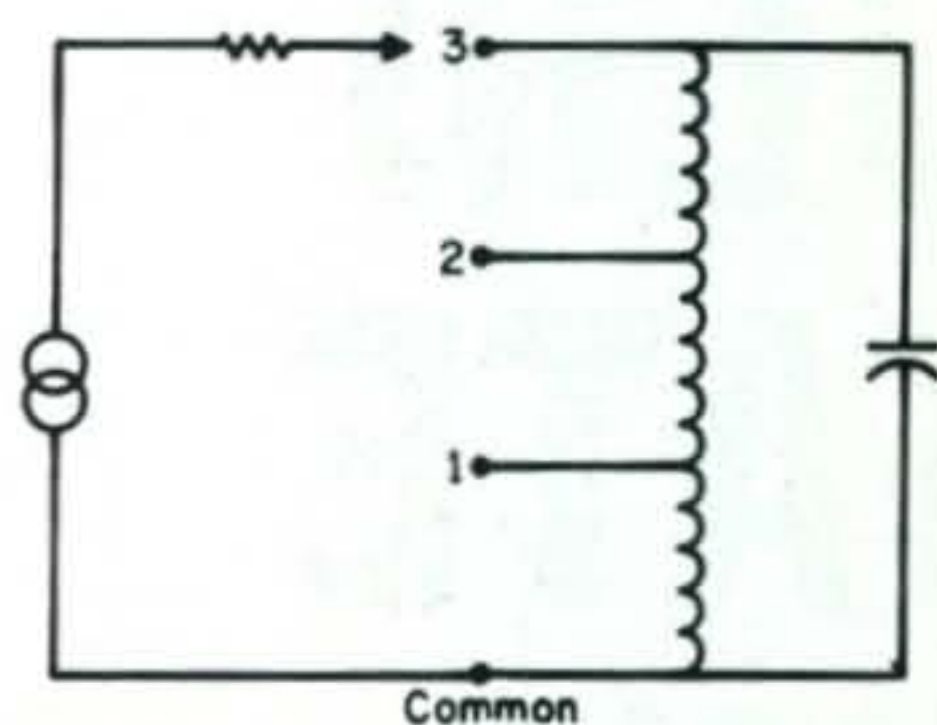


Fig. 4—Impedance matching by means of a tapped inductor. The tap impedance =  $Z_R ((N_T/N)^2$  where  $N_T$  is the number of turns from common and  $N$  is the total turns.

a problem in shielding. Now, many r.f./i.f. types have the case isolated from the transistor elements and it can be grounded through a fourth lead connected to the case.

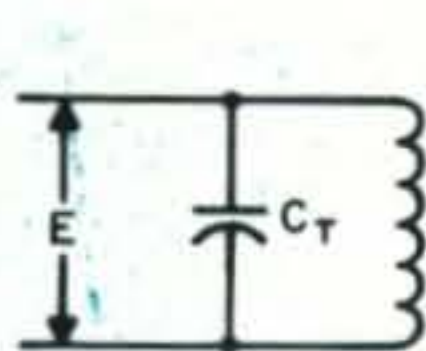
### Output Circuits

The output impedance of the transistor in an  $L-C$  tuned amplifier is sufficiently high that the tuned circuit could be represented as in fig. 2, and is essentially the same configuration as for a vacuum-tube circuit. The value of  $R$  would be higher than the impedance of the  $L-C$  circuit or omitted, depending upon the desired loading, the loading effect of the collector, and the means by which it is coupled to the following base.

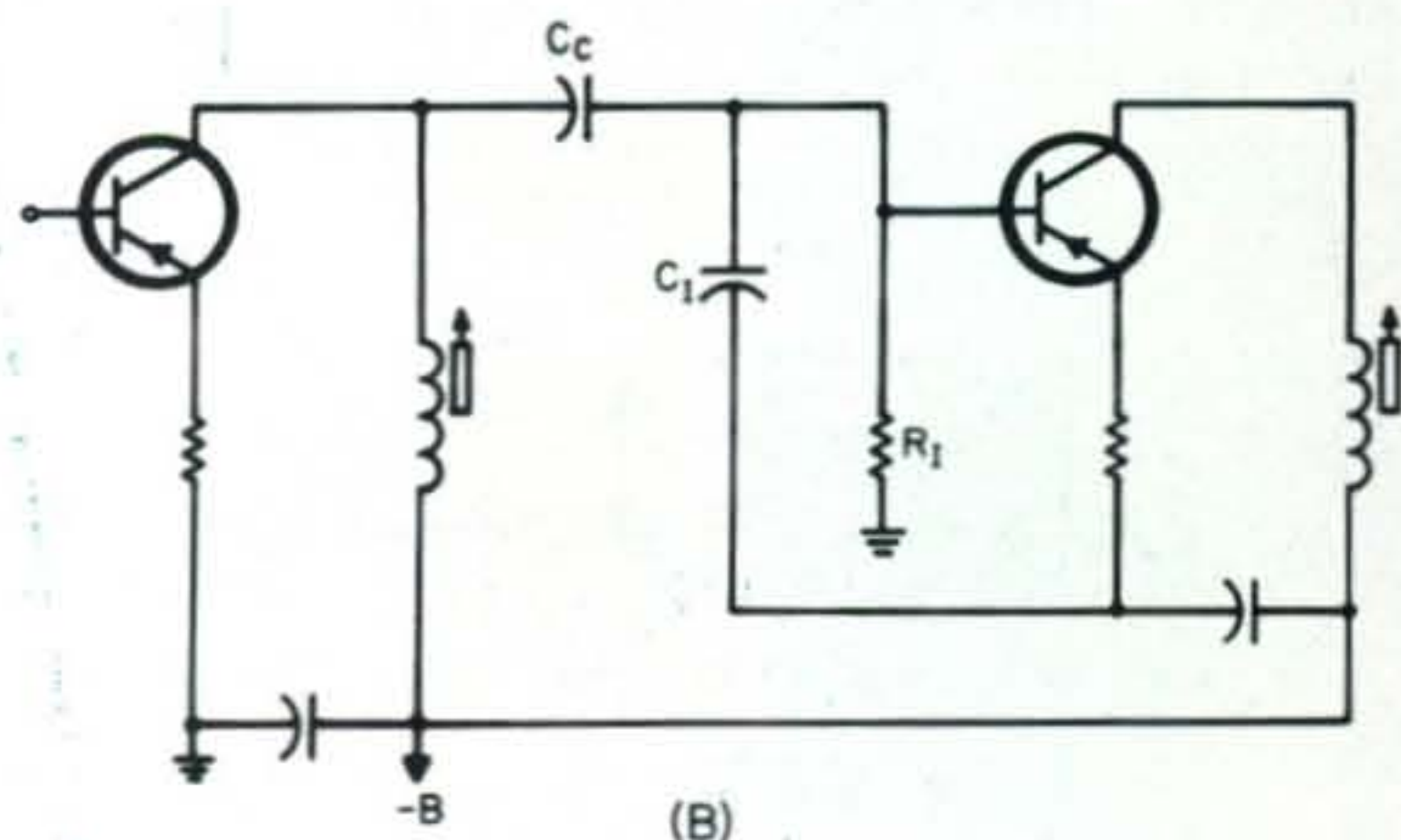
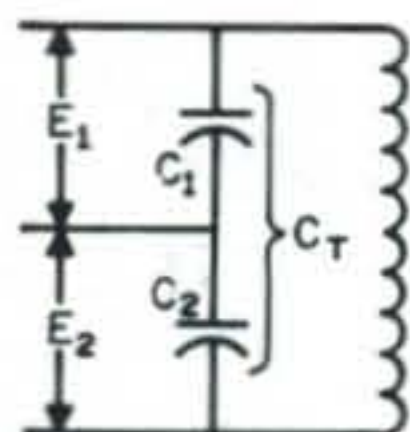
### Input Circuits

In order that the low impedance input of the transistor does not excessively load the tuned circuits thereby reducing the gain, some means of impedance matching must be resorted to.

$$E = E_1 + E_2$$



(A)



(B)

Fig. 5—(A) Impedance matching by means of a capacitive divider. (B) Typical circuit uses the coupling capacitor,  $C_c$  and the input capacity  $C_1$  to form the impedance divider.

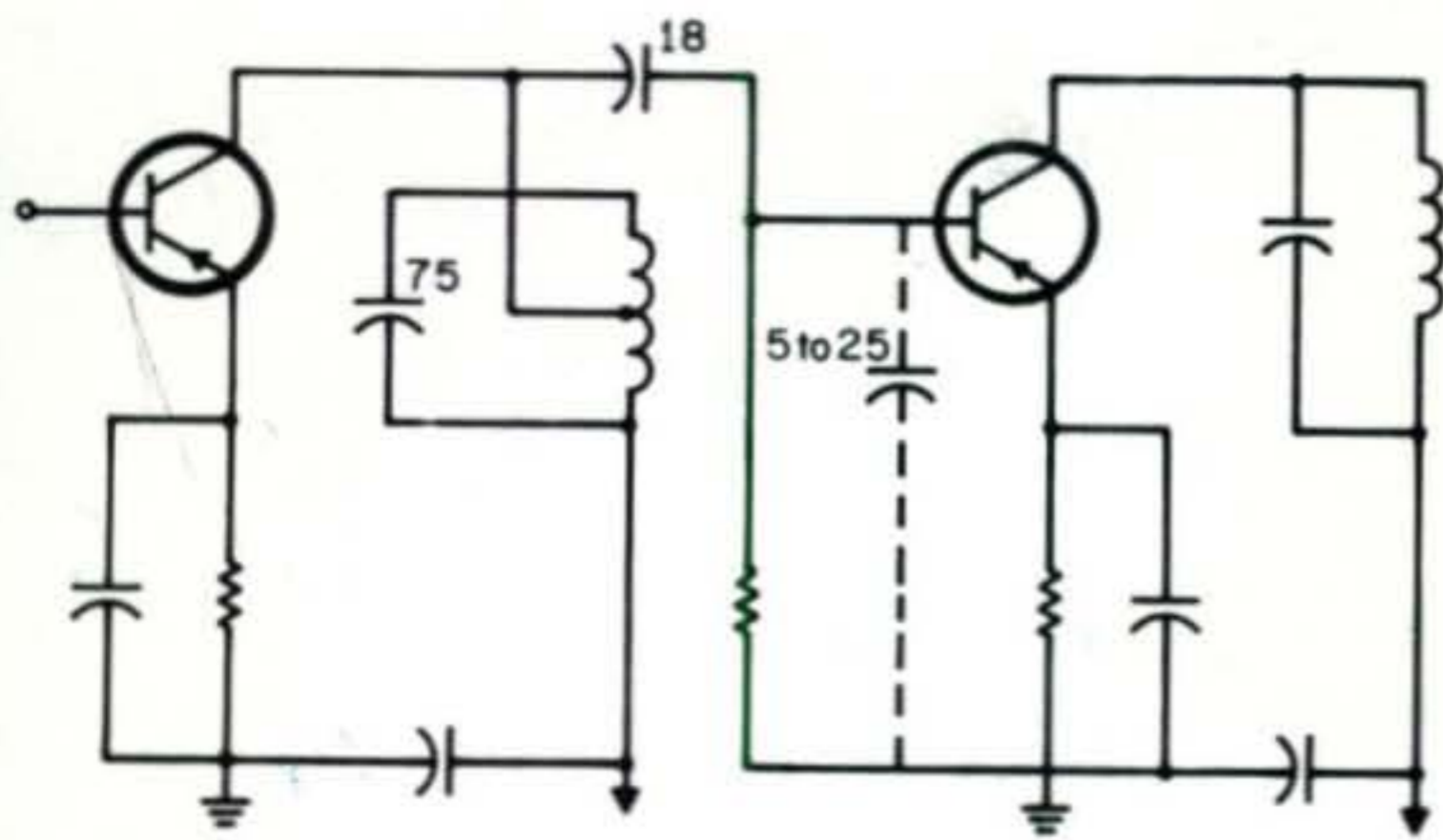


Fig. 6—Typical capacitor divider circuit and values.

There are three ways in which the proper match may be achieved. To better understand these methods, consider the various relations of the parallel tuned resonant circuit shown in fig. 3.

At resonance, the inductive and capacitive reactances are equal and the resonant impedance,  $Z_r$ , is the product of the coil  $Q$  (determining the bandwidth) and the reactance of *either* element since they are equal at resonance. The  $Q$  is the ratio of the tank current ( $I_L$  or  $I_C$ ) to the total current from the generator. Since the current  $I$  divides, the ratio of the currents in each branch depends upon the ratios of reactances and resistance present in the tank circuit. If the generator is considered to have a very high impedance, then the signal may be injected between the common terminal and terminal 1, 2, or 3 in fig. 4, without affecting the resonant frequency, unloaded  $Q$ , or resonant impedance of the tuned circuit, since  $Z_T = Z_1 Z_2 / Z_1 + Z_2$  as in parallel resistance.

Since the inductance of a coil varies as the square of the number of turns, the inductance, and hence the reactance and impedance at points 1, 2, and 3, will be one ninth, four ninths, and the total impedance respectively. Other arrangements are equally possible, *i.e.* a center tap gives one fourth the total impedance, *etc.*

The tuning capacity (where used) may be employed in a similar way to divide the total impedance, as shown in fig. 5(A). If the resultant capacity is the tuning capacity, the r.f. voltage across the tuned circuit is divided in the ratio of capacitive reactances, or the inverse of the capacity ratios, since:

$$IX_{c1}/IX_{c2} = E_1/E_2;$$

$$X_{c2}/X_{c1} = \frac{1}{2\pi f C_1} \bigg/ \frac{1}{2\pi f C_2} = C_2/C_1.$$

Stagger tuned i.f.'s, as found in TV circuits use the tube capacity (plus strays) as the only resonating capacity. In transistor circuits the

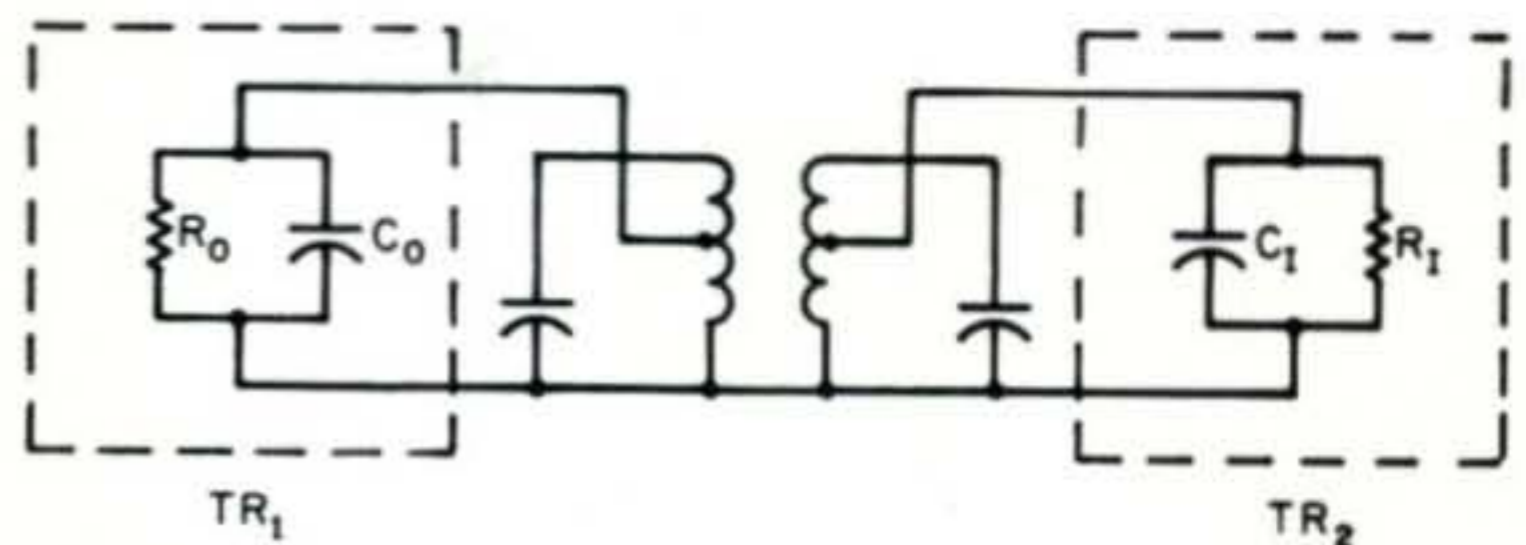


Fig. 7—Equivalent circuit of input and output matching with a tuned pair. The coupling between the two coils is discussed in the text.

input capacity is often much higher, but as seen in fig. 5(B), this capacity may be used as part of the impedance divider. If this capacity is too small, additional capacity may be used across the input, or the coupling capacitor that forms the other part of the divider may be made sufficiently small to give the proper division. When the tuning capacity consists mostly of a large fixed capacitor across the coil, this divider has little effect on the tuning if a small coupling value is used. See fig. 6 for typical values.

### Double-Tuned Circuits

Basically, the tuning and coupling of tuned pairs are accomplished the same way as for tube circuits. The only difference in their application to transistor circuitry is in the means of loading.

Fig. 7 shows the way in which a transistor with output impedance  $R_0$  and capacitance  $C_0$  is connected by means of a tap to the primary. The secondary is connected to another transistor stage with equivalent parallel input resistance  $R_1$  and capacitance  $C_1$ . The fairly high value of  $R_0$ . The secondary primary tap is usually at or near the top, due tap will normally be placed well below the middle of the coil to provide the desired amount of loading, since  $R_1$  is low, compared to  $R_0$ . The coupling may consist of either capacity or mutual inductance.

### Single-Tuned Transformer Coupling

An alternate method of matching a single tuned circuit to the input impedance of an-

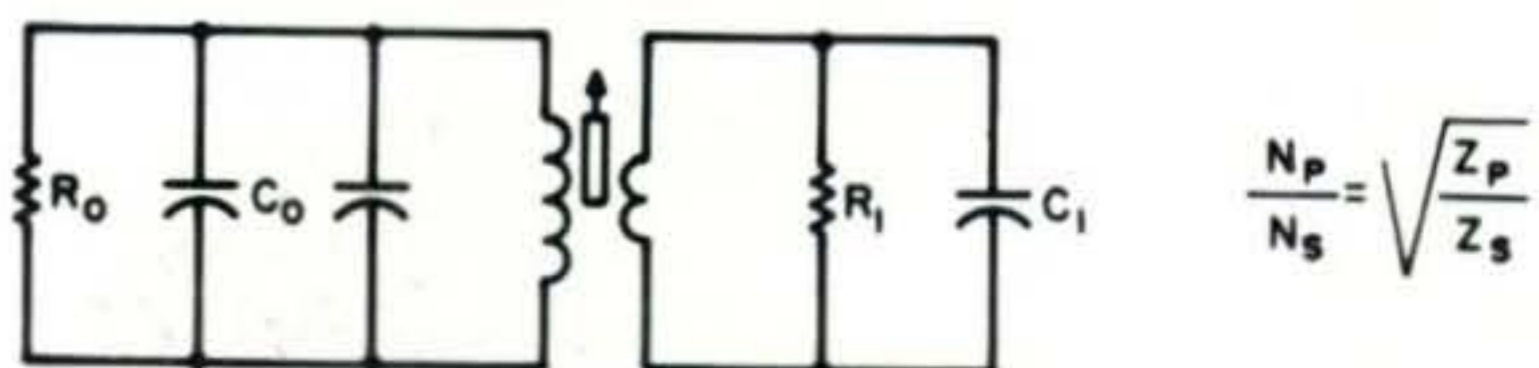
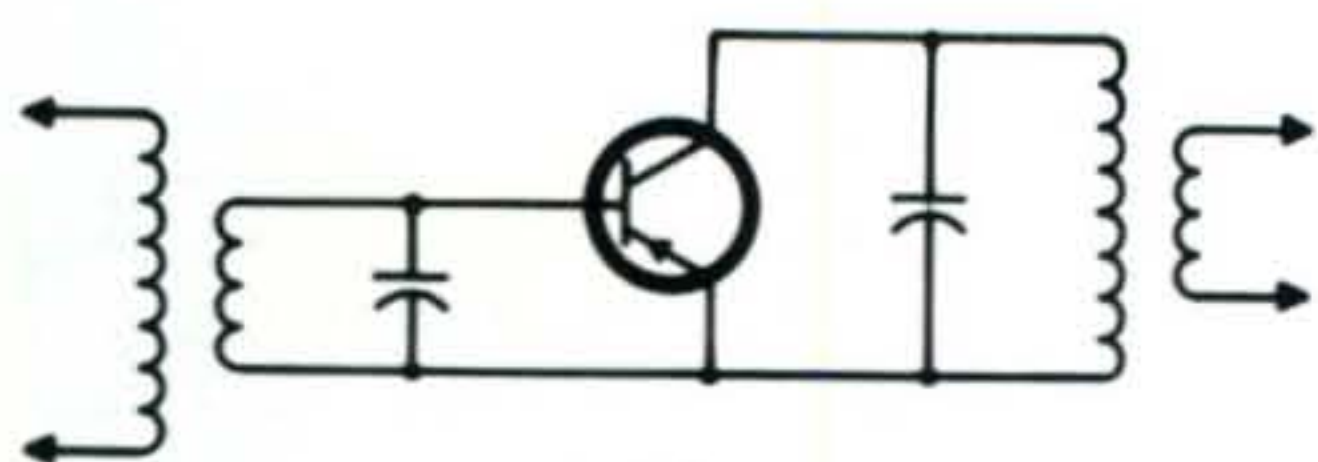
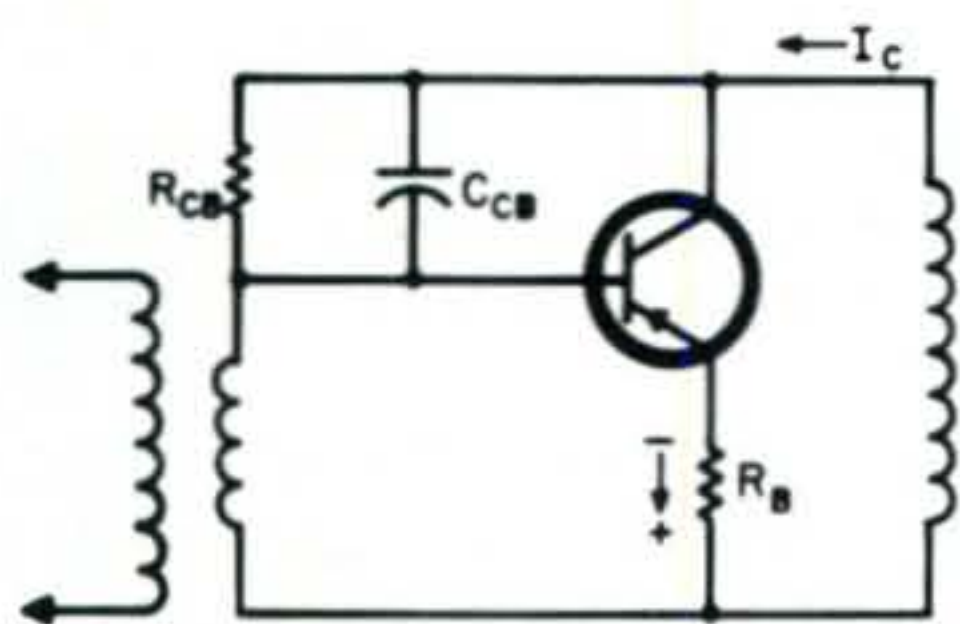


Fig. 8—Transformers with untuned secondaries are often used for impedance matching. The formula governing the relationship between the primary and secondary impedances is shown above.



(A)



(B)

Fig. 9(A)—Simplified common emitter amplifier. (B) Common emitter equivalent high frequency circuit showing the elements that produce feedback.

other transistor is by means of transformer coupling where the secondary and primary are tightly coupled but has a step down ratio. The step down ratio of the transformer should be equal to the square root of the ratio of output to input impedance of the transistors. This, in turn, gives the number of turns for the secondary, if the number of primary turns is already known. In this case the secondary is untuned, as shown in fig. 8.

### Neutralization or Unilateralization

Unlike the vacuum tube, the transistor is not a unilateral device, *i.e.* current can flow in both directions, even though small. Because it can do this, the output voltage variations cause variations at the input of the same transistor. The result is a feedback voltage that is, unfortunately, in phase and therefore *regenerative*. If this feedback voltage is large enough, the amplifier goes into oscillation. Just as in tube amplifiers, the feedback is large at higher frequencies, and if the frequency is low enough, the feedback voltage

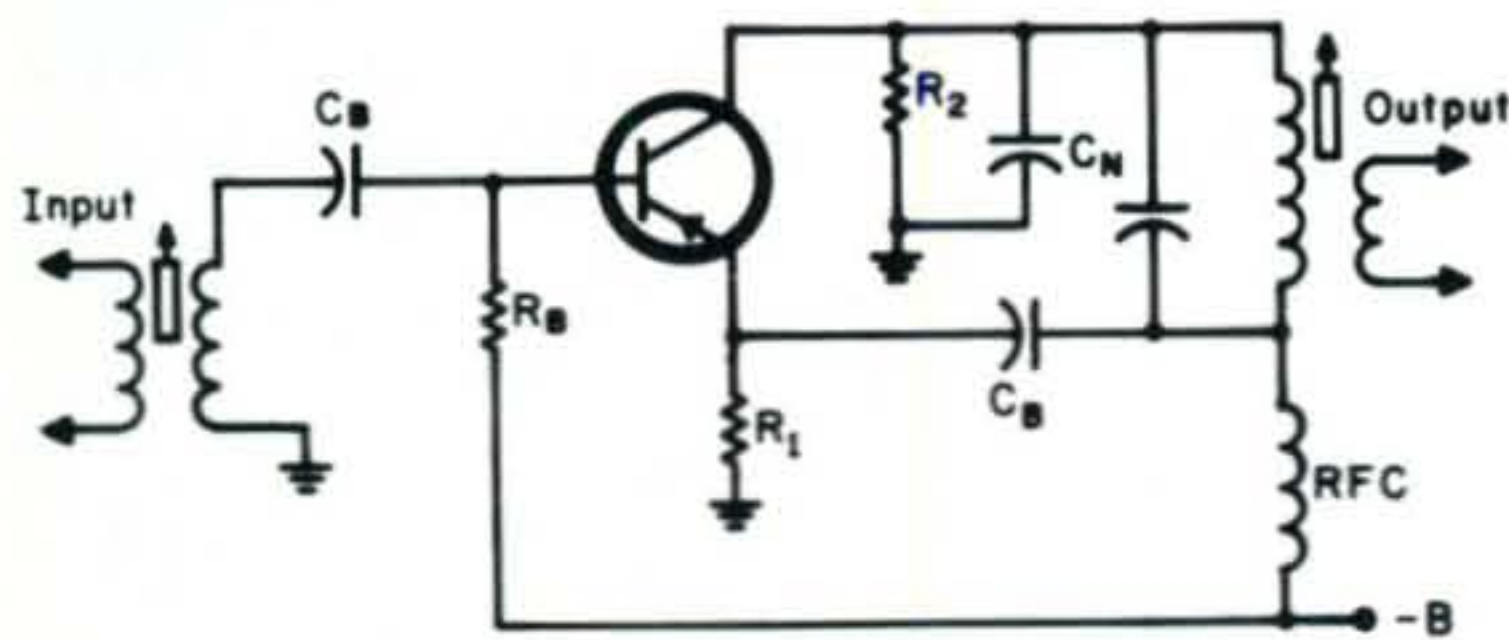
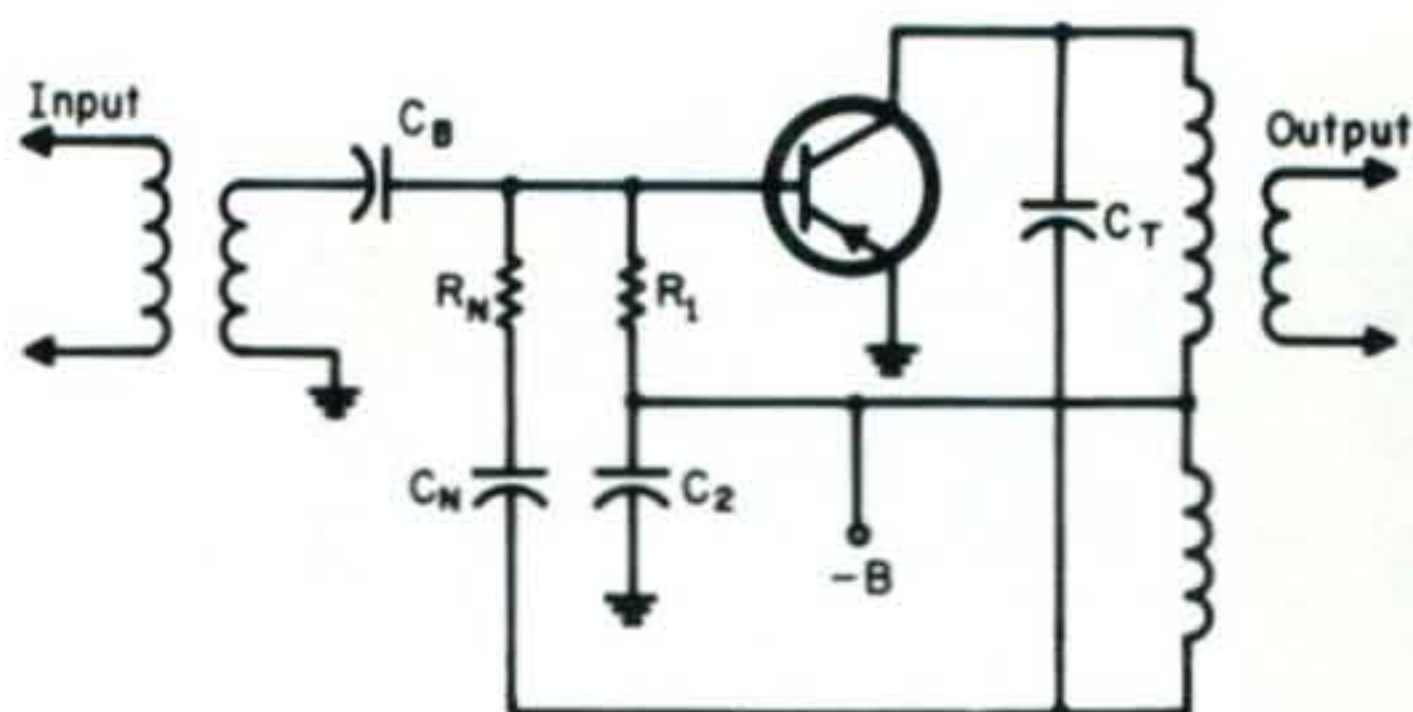
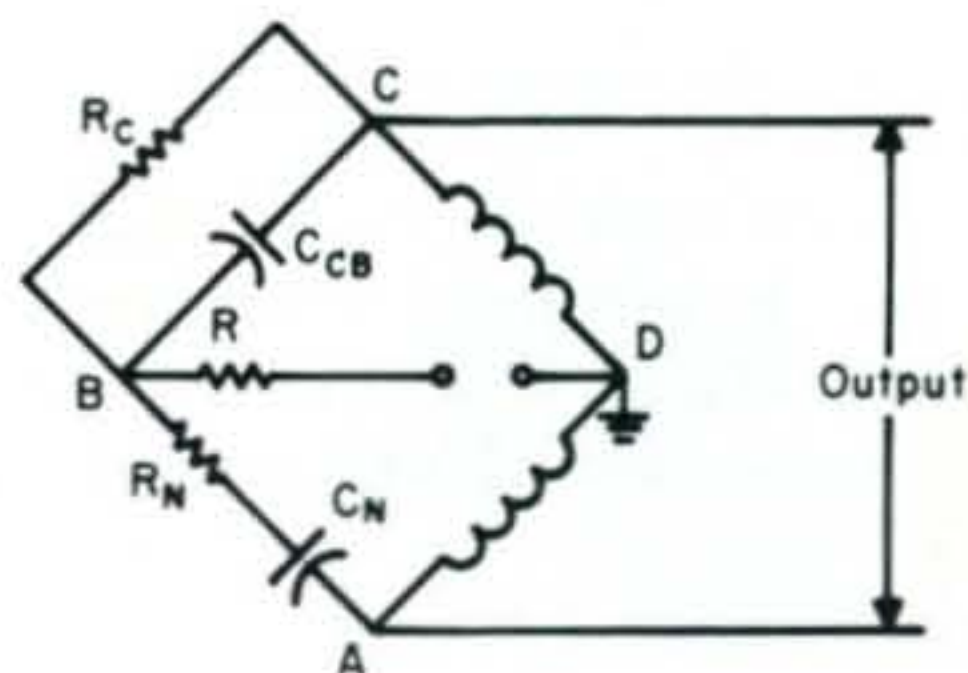


Fig. 10—Typical i.f. amplifier stage unilateralized by partial emitter degeneration. Components  $R_1$ ,  $R_2$  and  $C_N$  form the unilateralizing network.



(A)



(B)

Fig. 11—(A) Bridge unilateralization and its equivalent circuit shown in (B).

is too small to be of consequence. The equivalent feedback circuit of the common emitter circuit of fig. 9(A) is shown in fig. 9(B).

The capacity of the base-collector junction,  $C_{BC}$ , is small and of little consequence at low frequencies. The resistor it shunts,  $R_{CB}$ , is very high and is of little consequence under normal operation when reverse bias is applied to the base-collector junction. As the frequency increases, the capacitive reactance decreases, until such a frequency is reached where the impedance becomes lower than the value of  $R_{CB}$  and feedback occurs. The base spreading resistance  $R_B$ , produces a positive feedback voltage due to the collector current passing through  $C_{BC}$ .

Since we are interested in the use of these circuits at reasonably high frequencies some means must be used to prevent the occurrence of regeneration and oscillation. This method is known as *unilateralization* when *all* the input changes due to feedback, *both resistive and reactive* are cancelled. If only the reactive changes are cancelled, they are said to be *neutralized*.

To those readers who are familiar with transmitter circuitry, the methods used for unilateralization and neutralization will be familiar. For reasons previously given, the common-emitter amplifier only will be discussed, although the following methods will apply equally to the common-base amplifier.

[Continued on page 104]



# FSK WITH VOLTAGE VARIABLE CAPACITORS

BY GEORGE R. ALLEN, \*K1EUJ

**A** VARIABLE frequency oscillator can be adapted to frequency shift keying by mounting a small high speed relay in the v.f.o. circuit or by using one of the popular forms of the diode keyer. These circuits work well and are frequently used; however, in most cases shift adjustment must be accomplished by adjusting a small capacitor soldered directly into the v.f.o. circuit. This means that to adjust the shift of the radioteletype signal, this capacitor must be physically accessible. This presents little problem unless the capacitor is located in an awkward spot or unless you must put the transmitter back in its case. In these situations, shift adjustment can be a nuisance.

This article describes a frequency shift keying technique using a voltage-variable-capacitance diode. With this technique, shift adjustment is made by varying the voltage applied to the diode. Thus, shift adjustments need not be made at the transmitter and can be made at any position remote from the transmitter by varying a small potentiometer in a biasing circuit.

As an example of the use of this type of frequency shift keyer, this article describes the conversion of the HX-50 and the TCS transmitters to frequency shift keying by using a small variable-capacitance diode.

## The Voltage-Variable-Capacitance Diode

The diode used in the circuits described in this article is a TRW IN4792A which has a nominal capacitance of 22 mmf at a reverse bias of 4 volts. It can be obtained from most large parts distributors. If TRW diodes are not available, Motorola variable-capacitance diodes may be used.

\* 74 Wells Street, Westerly, Rhode Island.

From an operational standpoint, the voltage-variable-capacitance diode is similar to the usual solid state diodes used as rectifiers and as detectors. If it is forward biased (anode positive, cathode negative) it will exhibit properties similar to a standard diode and could be used as a detector or rectifier. Upon reversing the bias, this diode will not conduct and will look like a regular diode; however, upon varying this reverse bias the special properties of this diode become apparent. With this diode, the capacitance across the diode decreases in a controlled manner as the reverse bias is increased, while with a regular diode the capacitance decreases very rapidly for a small voltage change and the capacitance change is not easy to control.

## A Simple Variable Capacitance Diode Keyer

Figure 1 shows a circuit of the simplest variable-capacitance diode keyer. As the voltage  $V$  is varied, the capacitance of the diode will vary altering the resonant frequency of the v.f.o. tank. If, with some voltage  $V$  applied, a varying alternating voltage such as the output from an audio amplifier were connected to point  $A$  in the circuit, the v.f.o. could be frequency modulated.

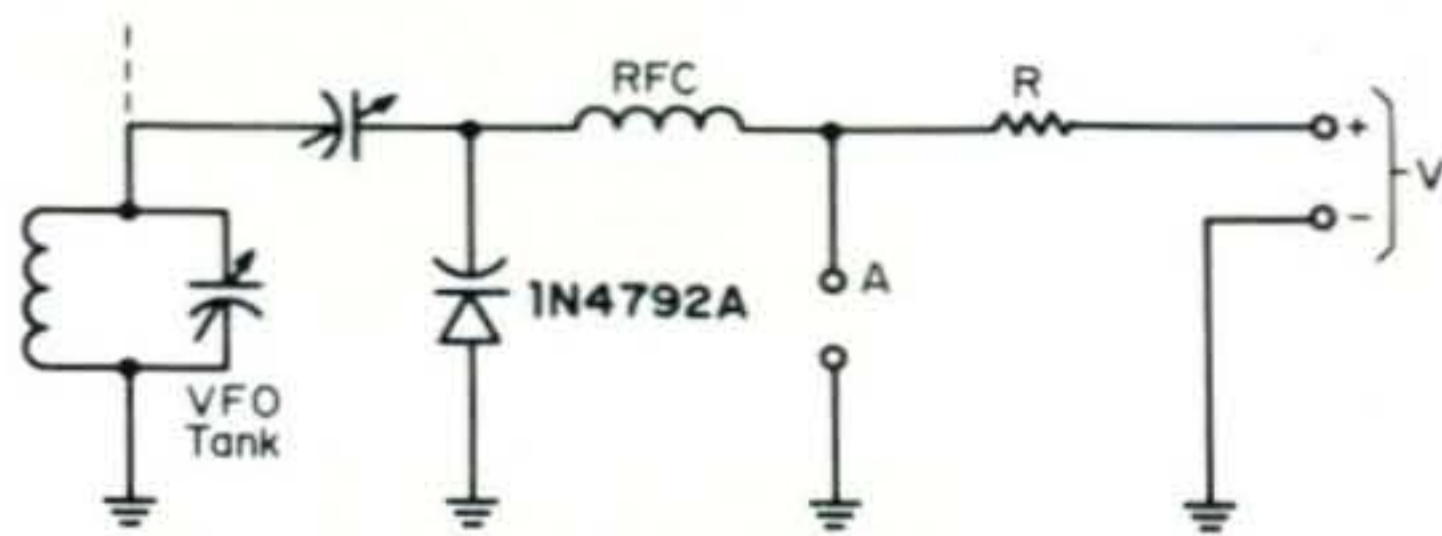


Fig. 1—Basic circuit of a v.f.o. using a voltage variable capacitance diode for frequency control.

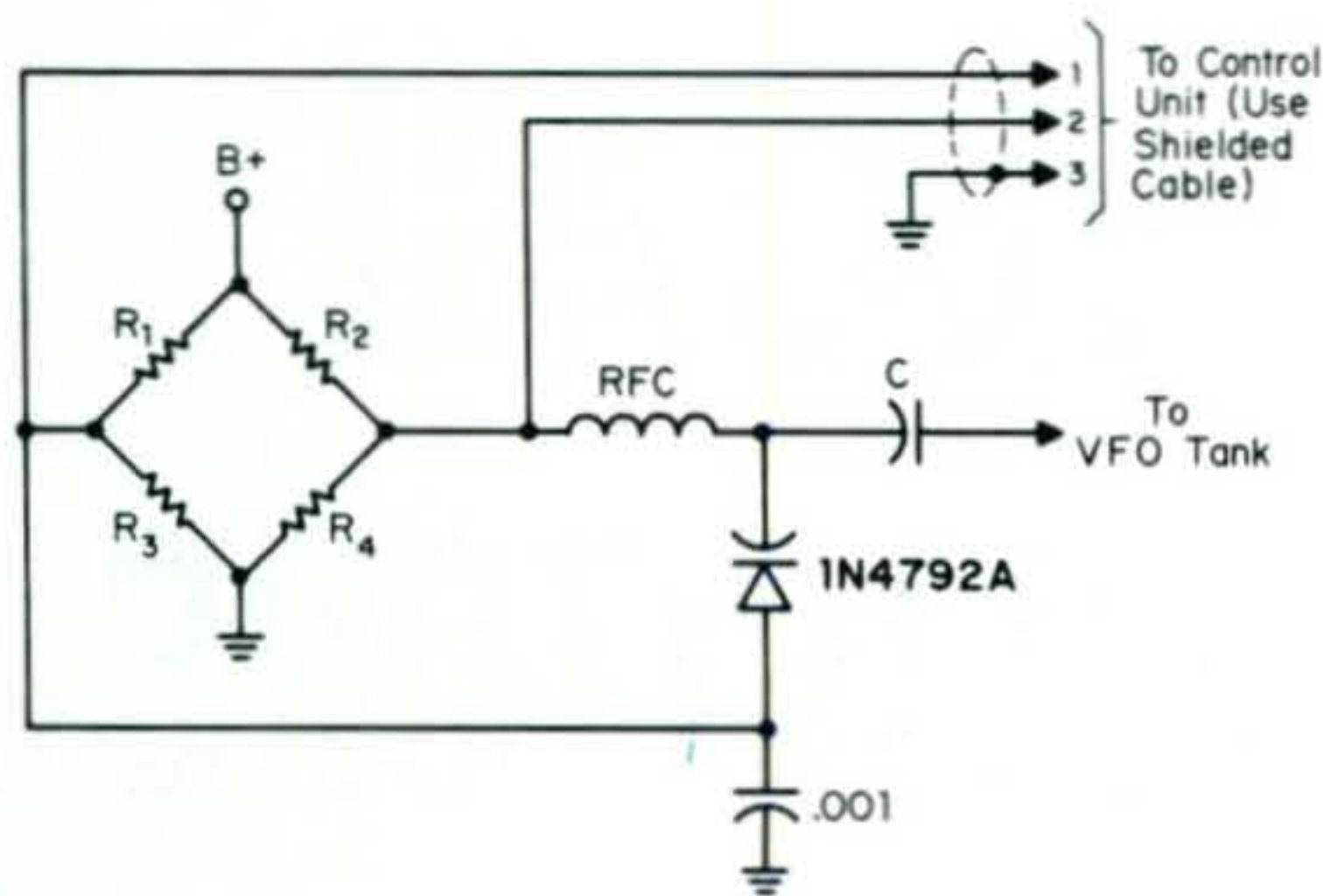


Fig. 2—Circuit of a practical keyer that can be used to frequency shift a v.f.o. With a proper control unit the keying can be reversed and the shift adjusted to any desired value. Typical component values are discussed in the text.

For frequency shift keying, a teleprinter keyboard or a polar relay could be connected to point "A". Since the teleprinter in its inactive state (a key is not depressed) shorts the circuit, the capacitance of the diode will be some value,  $C_0$ , with zero bias. When the keyboard is active (a key has been depressed) the capacitance will decrease to some value designated by  $C_v$ , where  $v$  is the voltage applied to the circuit. This net decrease in capacitance will cause an increase in frequency. Thus we have developed a simple frequency shift keyer.

Unfortunately the keyer in fig. 1 has a few disadvantages, since the way it is set up, it has no provisions for varying the shift and in addition the space is higher in frequency producing upside down keying.

### A Versatile Variable Capacitance Diode F.S. Keyer

Figure 2 shows a universal variable-capacitance diode frequency shift keyer. In this case the diode is biased by a bridge circuit permitting either normal or reversed keying. Figure 3 shows the control unit for use with this keyer. This control unit may be mounted at some convenient location at the operating position and need not be mounted on or near the transmitter. The only precaution is to use shielded coaxial cable for connecting the units together and for connecting the teleprinter to the control unit.

To determine the values of resistors  $R_1$  through  $R_4$ , the reverse voltage rating of the diode used must first be ascertained from the manufacturer's literature. The diode used in this circuit, the TRW 1N4792A, has a maximum inverse voltage of 20 volts. The values

of these resistors will depend on the B+ voltage and may either be calculated by ohms law or determined by trial and error. If you are not much for math and have 200 to 300 volts available then the proper resistors may be chosen by trial and error as follows. Starting with  $R_1$ , select a resistor of between 400K and 500K ohms; for  $R_3$  start with a value of about 20K ohms. Measure the voltage at the junction of  $R_1$ - $R_3$  with a v.t.v.m. or high impedance voltmeter with the B+ voltage connected. If the voltage is too low, increase  $R_3$  by a few thousand ohms and try again, if the voltage is too high, decrease  $R_3$ . When the proper voltage is obtained select  $R_1$ - $R_2$  and  $R_3$ - $R_4$ . Now solder the diode into the circuit and recheck the voltages again. The voltages at the anode and the cathode of the diode should be approximately equal or the voltage at the junction of  $R_2$ - $R_4$  (the cathode) should be slightly higher than the voltage at  $R_1$ - $R_3$ . If the voltages are incorrect, vary  $R_3$  to obtain the proper voltage ratio. To obtain maximum capacitance variation, the voltage difference should be less than one volt. If the voltage difference is much greater than one volt, maximum capacitance variation will not be obtained, and if the cathode ( $R_2$ - $R_3$ ) voltage is less than the anode voltage then conduction will occur (current will flow through the diode) and possible overheating may occur. It should be noted that it is desirable to obtain maximum capacitance variation so that maximum shift variation may be obtained.

After the proper resistors have been selected, the keyer should be connected into the v.f.o. circuit. The diode should be mounted as close as possible to the v.f.o. circuit. Capacitor  $C$  should be chosen so that when the junction of  $R_1$ - $R_3$  is shorted to ground the frequency shift is between a kc to 1.5 kc. For a starting value for  $C$  use a small ceramic capacitor of about 20 mmf. If the shift is too large, decrease  $C$ ; if it is too small, increase  $C$ . The capacitor,  $C$  must be chosen by trial and error for all practical purposes. The r.f. choke, RFC, may be a miniature 2.5 mh type; this choke is not critical at all.

Once  $C$  and all resistors have been selected and the circuit tested, the control unit may be connected to the keyer. This control unit has a switch and three sets of pots to provide adjustments for three different shifts. If three shifts are not needed, then one pot only may be used. In addition, a separate pot is included for adjustment of the shift used for identification keying. To adjust the shift,

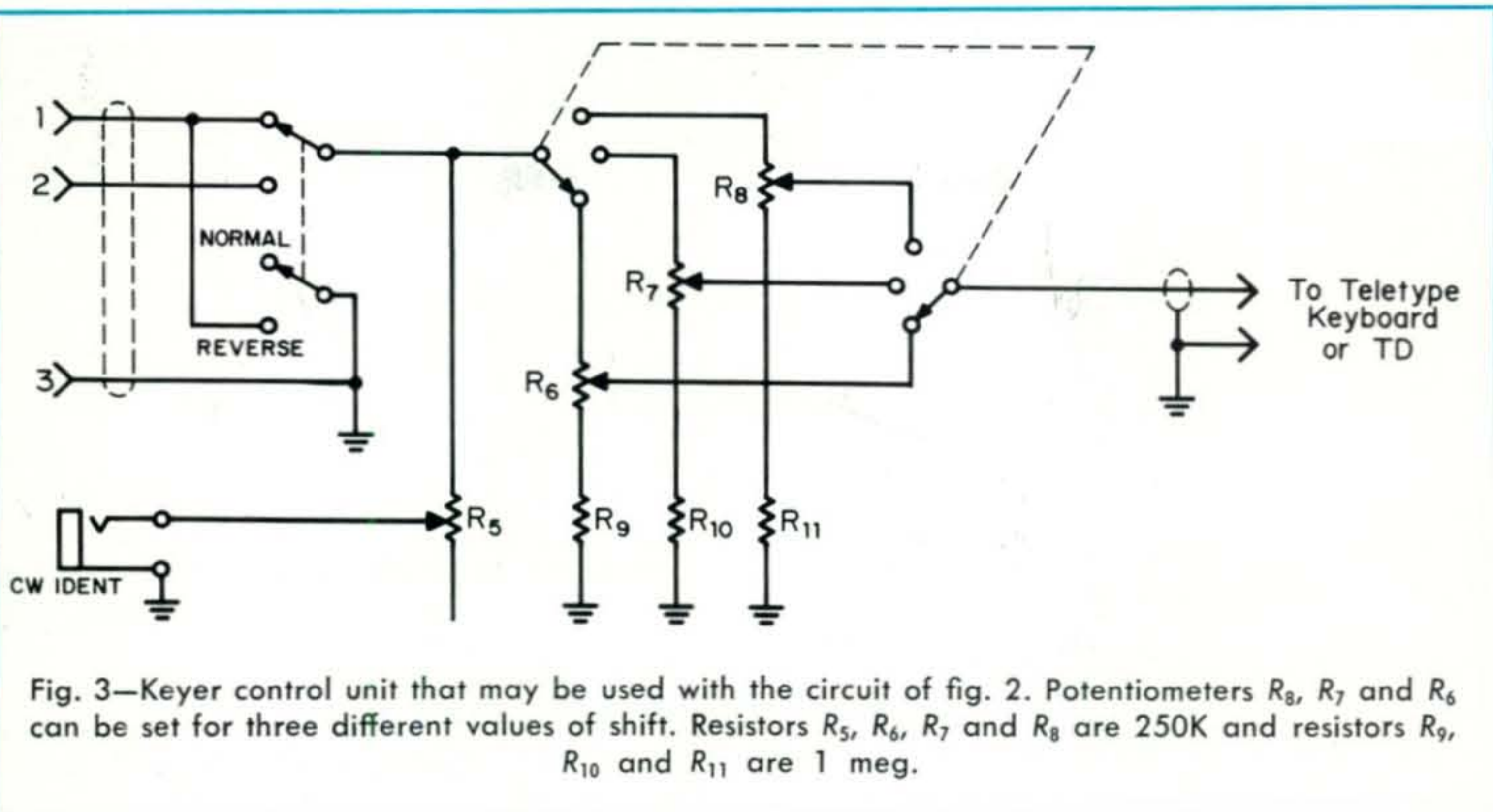


Fig. 3—Keyer control unit that may be used with the circuit of fig. 2. Potentiometers  $R_6$ ,  $R_7$  and  $R_8$  can be set for three different values of shift. Resistors  $R_5$ ,  $R_6$ ,  $R_7$  and  $R_8$  are 250K and resistors  $R_9$ ,  $R_{10}$  and  $R_{11}$  are 1 meg.

merely vary the potentiometers while operating the teleprinter until the desired shift is obtained.

Be certain to use shielded cable to connect the control unit to the keyer on the transmitter and to connect the teleprinter keyboard to the control unit. If shielded cable is not used 60 cycle voltages will be picked up on the connecting cables which will frequency modulate the carrier. If hum does occur with the shielded cable, try reversing the power line plugs on the transmitter and the teleprinter, try reversing the cable connections at the teleprinter. Also be certain that the cable is grounded to a common ground at only one end to prevent a hum loop.

### Converting the HX-50

The HX-50 is one of the easiest transmitters to modify for f.s.k. since it already contains a variable-capacitance diode as an integral part of its v.f.o. circuit. This diode is used to adjust the v.f.o. frequency on upper sideband so the u.s.b. and l.s.b. frequencies are the same. Only a one wire modification and a connection jack on the back panel are needed. The way the circuit is set up the transmitter will f.s. key normally on all bands, but cannot be simply modified for reverse keying. To modify it for reverse frequency shift keying, the circuit described in fig. 2 should be used.

Figure 4 shows the modification for the HX-50. A single wire is connected to the hot end of the oscillator adjusting pot,  $R_{138}$ . This wire is connected to a new jack which must

be added to the rear panel. By shorting this wire to ground through a potentiometer the output frequency is raised.

Figure 5 shows the control unit used with the HX-50. This control unit is a simplified version of that described in fig. 3. An ON-OFF switch has been included to disable the frequency shift keying provision to use the transmitter for s.s.b. If this switch is left in the ON position for s.s.b., the u.s.b. and l.s.b. frequencies won't agree. Again the shift is adjusted by varying  $R_{12}$ .

### Converting the TCS

The surplus TCS transmitter is very simple to modify for frequency shift keying although it does not already have a built in variable-capacitance diode. The circuit described in fig. 2 is used with the connection to the v.f.o.

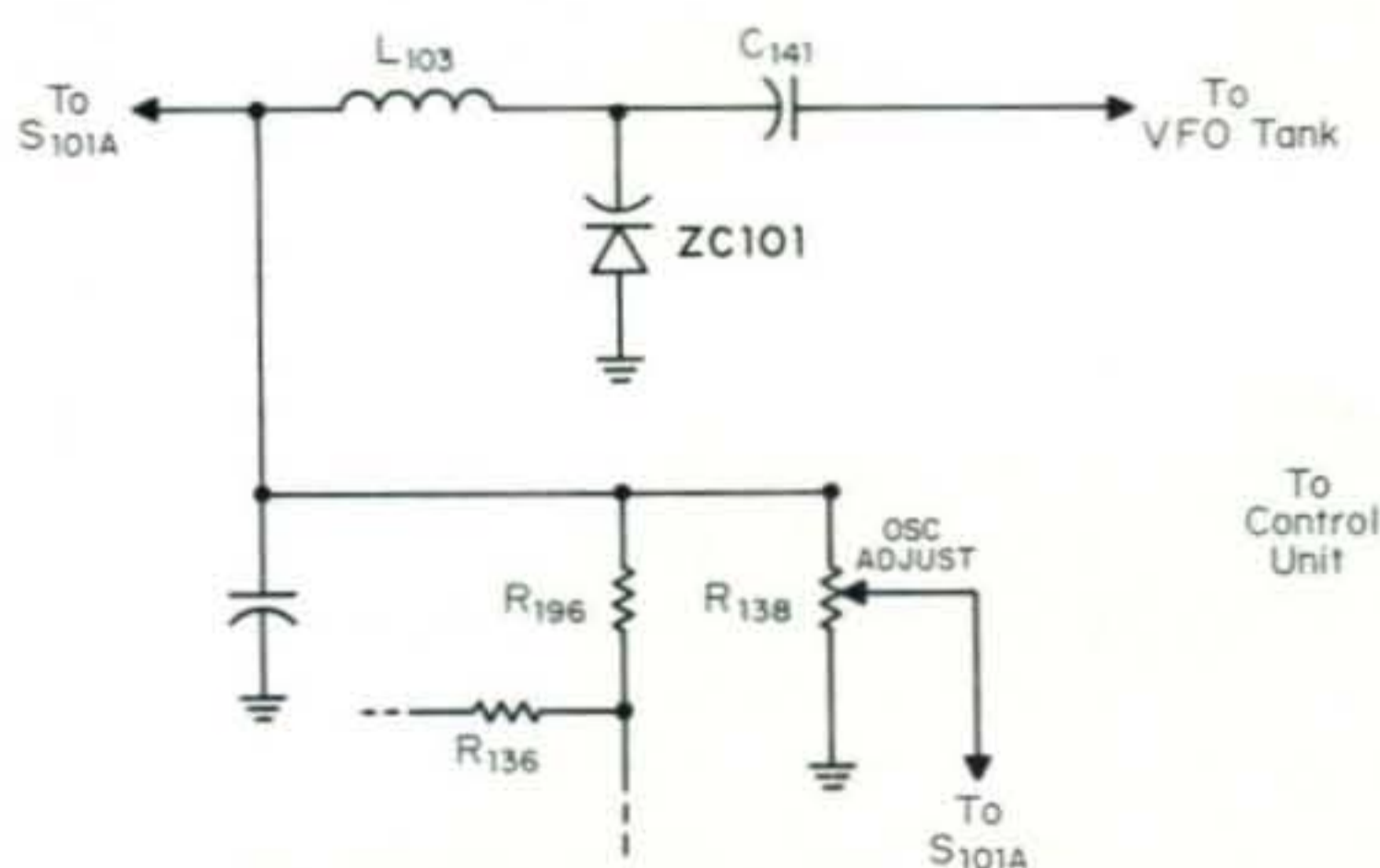


Fig. 4—Simple modification for f.s.k. operation with the HX-50. The wiring shown in color is added and the jack,  $J_1$ , is mounted on the back panel.

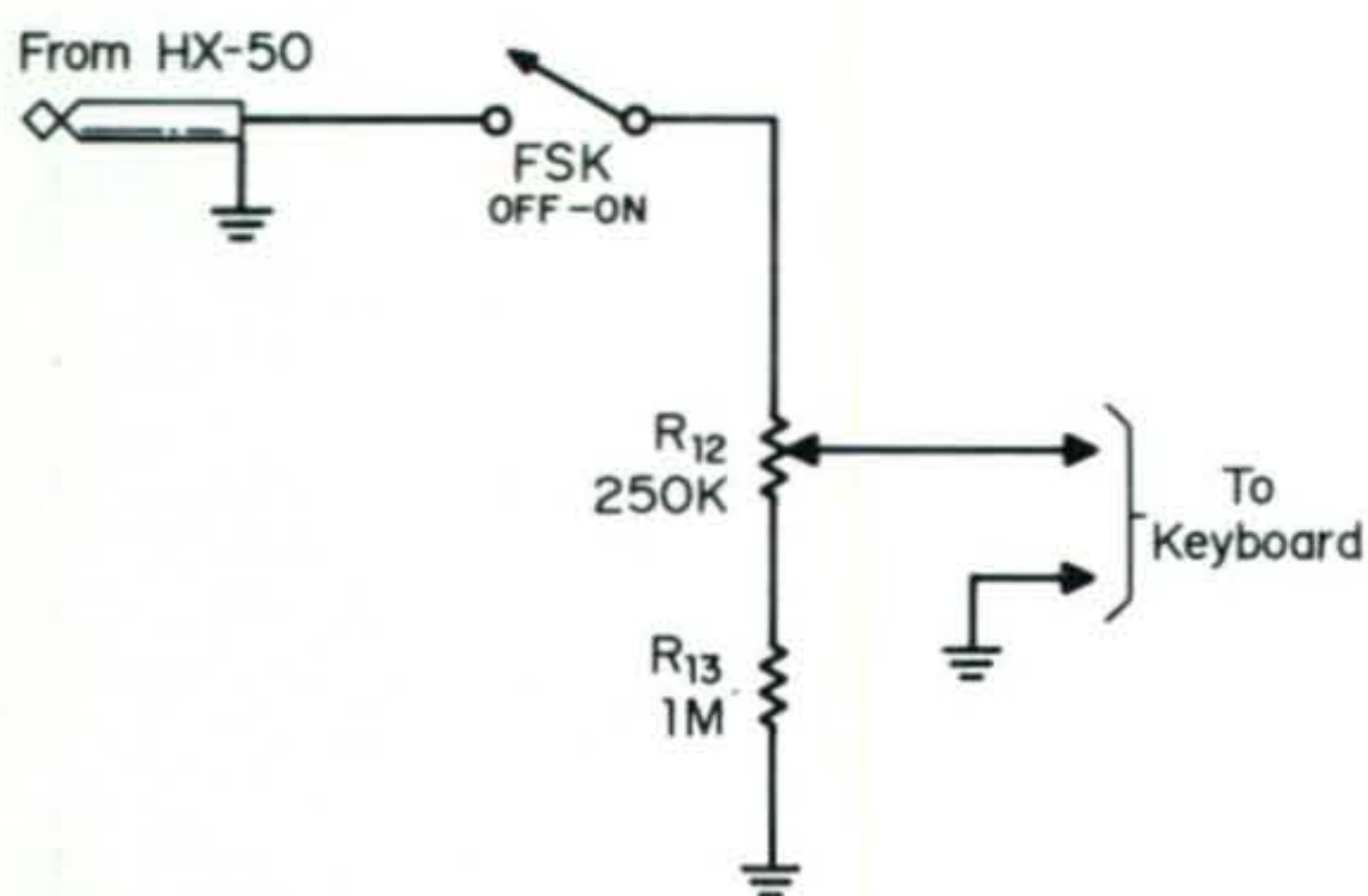


Fig. 5—Control circuit for the f.s. keyer in the HX-50 shown in fig. 4. Control  $R_{12}$  sets the shift.

made to the cathode pin of the oscillator. The cathode of the oscillator is pin 8 of the 12A6 closest to the side of the transmitter. The value of  $C$  which should be used is about 100 mmf. For a  $B+$  voltage of 200 volts  $R_1$  and  $R_2$  should be 470K;  $R_3$  and  $R_4$  should be 47K. The value of  $R_3$  may have to be adjusted either up or down so that the voltages on the anode and cathode are approximately the same when the control unit is not connected.

### Vernier Frequency Control

One problem that is very evident with some surplus v.f.o. controlled transmitters is that it is sometimes difficult to accurately zero beat a station. This presents no problems for c.w. or a.m. but for radioteletype or s.s.b it may be next to impossible to zero beat a station to within 50 cycles or so. This problem can be cured by using a variable-capacitance diode vernier frequency control. This circuit is shown in fig. 6. In this circuit, an additional diode is placed in the v.f.o. circuit.

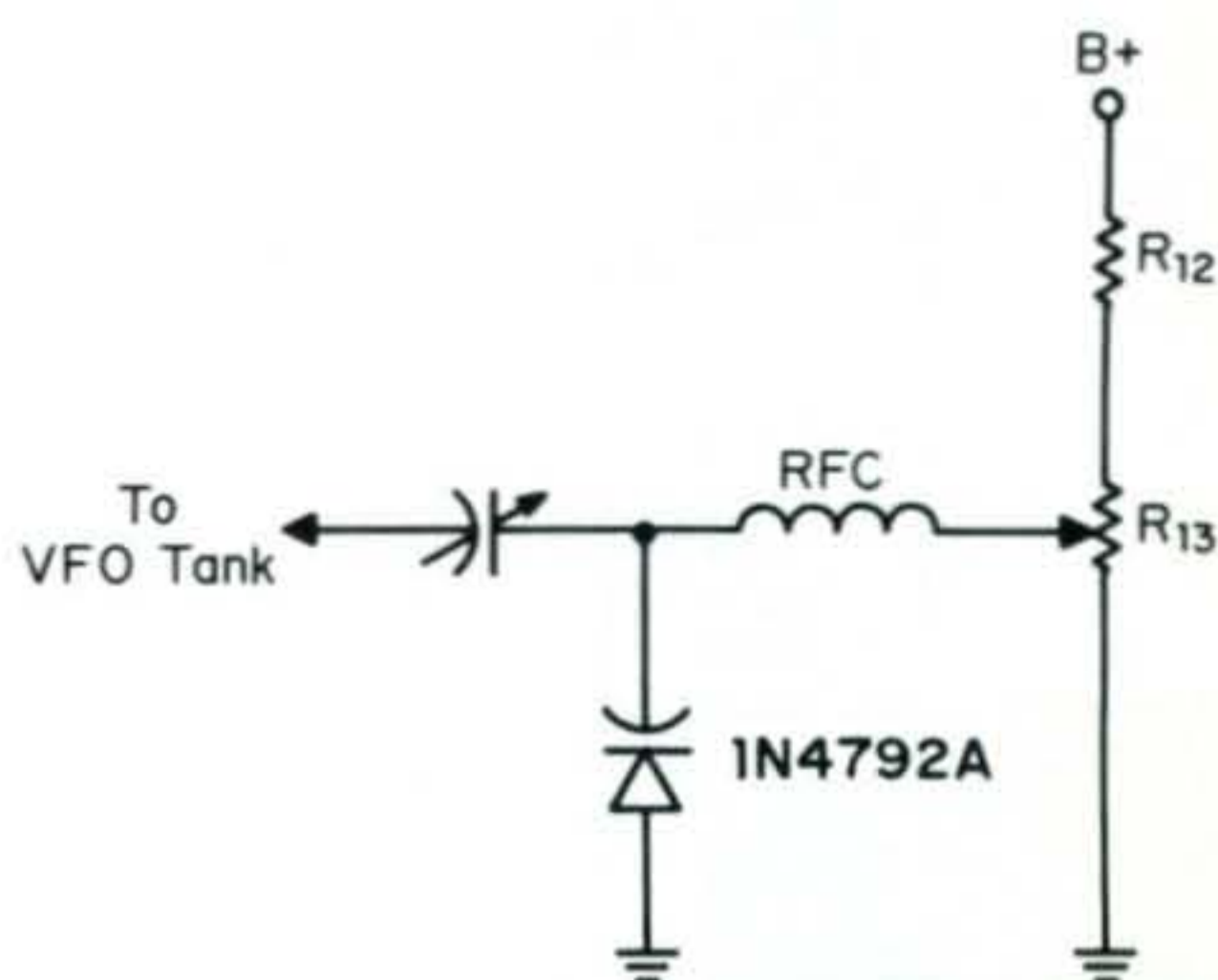


Fig. 6—Simple circuit shown above is suitable for vernier frequency control of a v.f.o. as explained in the text.

For zero beating,  $R_{13}$  is placed at mid range, the main v.f.o. is varied to place the carrier as close as possible to the desired frequency and  $R_{13}$  is varied to provide fine tuning over a kc range. Resistors  $R_{12}$  and  $R_{13}$  are chosen so that the voltage at the junction of  $R_{12}$ - $R_{13}$  does not exceed the maximum voltage of the diode used. The capacitor  $C$  is adjusted so that a maximum frequency of about kc is obtained if  $R_{13}$  is shorted out.

With the information presented in this article almost any transmitter with a v.f.o. may be simply modified for f.s.k., with the shift adjustment located at any remote operating point from the transmitter.

Although this article dealt mostly with the frequency shift keying applications of the variable-capacitance diode, this diode can be used for other related applications as well. Some of these applications might be remote tuning of a receiver, crystal oscillator, wavemeter, or similar device. ■

## 1968 YL-OM CONTEST RESULTS

BY LOUISA B. SANDO,\* W5RZJ

**C**ONGRATULATIONS to all the top scorers in YLRL's 19th YL-OM Contest, held Feb. 24-25 (phone) and Mar. 9-10 (c.w.), and especially to Sonia Rotenberg, PY2SO, who won in both sections for the YLs. (In '67 Sonia earned second high YL score on c.w.) Congratulations also to W5WZQ, David Blaschke, who turned in the top OM c.w.

\* 4417 Eleventh St., N.W. Albuquerque, New Mexico 87107.

score (he placed second in the '66 contest), and to K5MDX, David Thompson, who earned top OM score on phone, repeating his '65 win in this category.

YLRL V.P., Claire, W4TVT, who checked the logs, expressed her appreciation for the care taken in preparation of logs in this contest, adding that none was disqualified for illegibility. However, some logs were received

[Continued on page 100]

*A Salute to...*

## Mister One-Sixty

BY CHARLES M. O'BRIEN,\* W2EQS

**R**EMINISCENT and symbolic of the original low frequency pioneering trans-Atlantic experimental work carried on during the era of 1901 thru 1924 are such names as Marconi, Deloy, Schnell, Reinartz and Godley who have gone down in history.

Wireless was born in the late 1890s and its fascination instantly swept over men of all ages intent on learning the mysteries that became such a deep rooted question within them. They read with avid interest whatever small knowledge could be passed on. Nothing was known to the majority. They had to experiment with every move they made. And, the man of the day was Marconi.

Is it any wonder, then, that unequalled interest was shown upon the arrival of Marconi and his two assistants from Europe at St. John's, Newfoundland, on December 6, 1901? Six days later the Atlantic was bridged by wireless when the prearranged code letter "S" was heard. The European experimental station was at Cornwall in southwestern England 2,000 miles distant.

During the early years of wireless most amateur stations operated on frequencies covering 550 to 1500 kc and which are now known to be the broadcast band (eventually changed in later years to be 540 to 1600 kc). With rapid advancement of the art, modulation came into being and, as a result, considerable confusion and interference became inescapable. The situation was becoming not only uncontrolled but impossible. And so, the Radio Act of 1912 was passed in August of that year ordering amateurs to use frequencies of 200 meters and down. To commercial and government interests these frequencies were considered as being useless with the belief then being that the long waves were the most useful.

As a lad of but 8, Stew Perry first went on the air in 1912 using the self assigned call of "SS" simply because it was a simple one to send as well as for others to remember but very possibly emulating the single "S" of Marconi.

Known to countless numbers now as W1BB, Stewart S. Perry is the world's foremost amateur radio operator delving into the mysteries and the potential of our lowest band of frequencies . . . 160 meters.

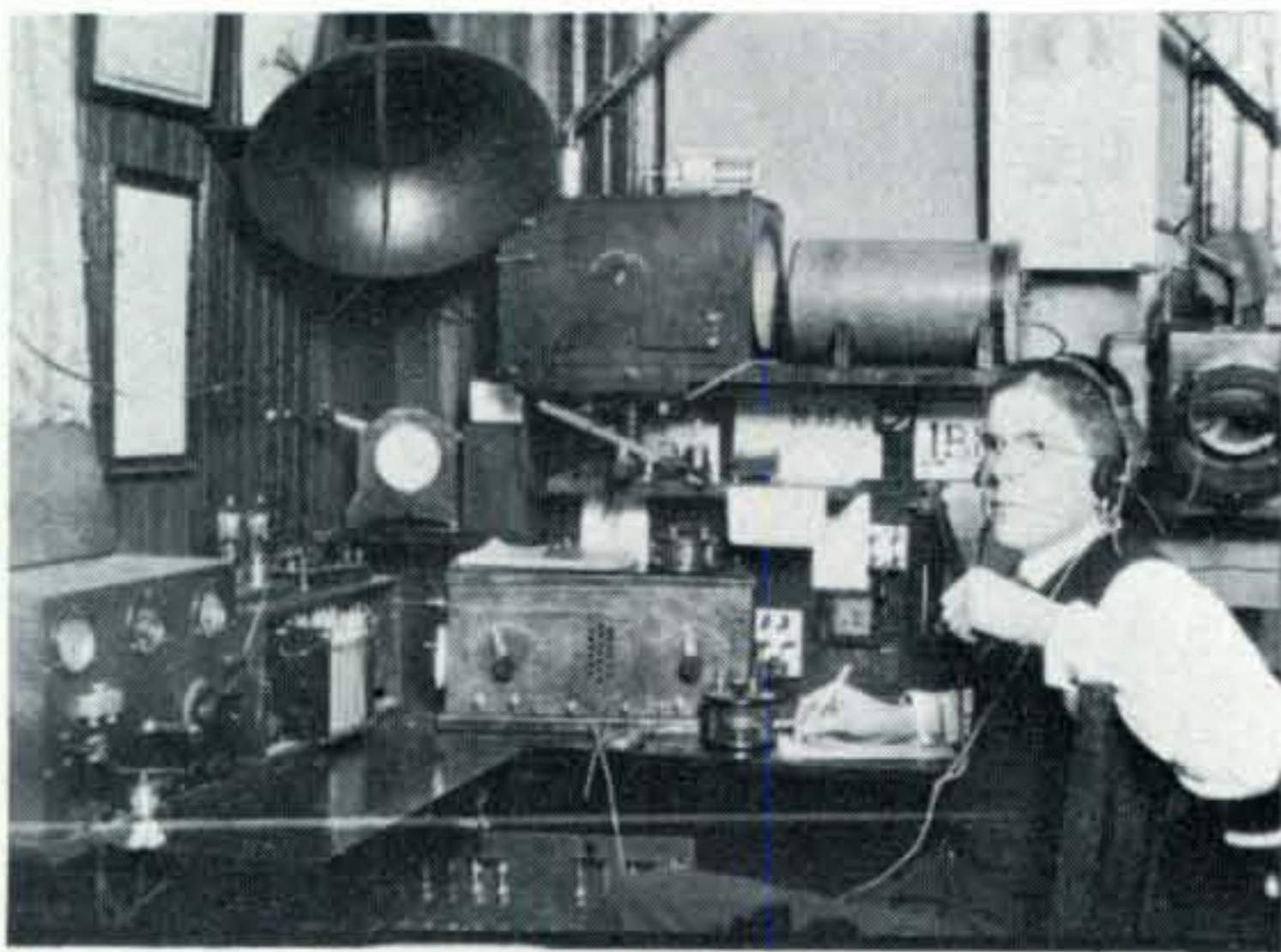
His first transmitter consisted of a single slider tuning coil with a crystal detector and 1/4" spark coil hooked to a random 40 foot piece of wire into a nearby tree. With this type of equipment one was considered fortunate to establish communication with points over 100 miles distance. One of the world's most shocking experiences at this time was the sinking of the *Titanic*. Of the many early feats accomplished by wireless, Stew recalls his copying of emergency traffic from the *Titanic* disaster as his most memorable recollection.

With the entrance of the United States into WW I, all amateur radio stations were ordered off the air as of April of 1917. Towers



The little clock reads ten to 10 in this early (1919) view of 1BB.

\* 48 Prospect Avenue, Westwood, N.J. 07675.



In 1921, Stew posed for this shot perhaps logging in some rare one. The trim efficient layout of the shack carries over his shipboard training.

and antennas were to be dismantled and all receiving and transmitting equipment sealed. Strangely enough it was at this time that he obtained his first official station and operators license and was assigned the call 1BB with which he is still active. However, with all amateur gear now being silenced he studied for his commercial radiotelegraph ship operator's license. As a boy of 16 he put to sea to earn money for college. Not only was it great fun, but it gave him great experience as he operated aboard coastal, trans-Atlantic and Great Lakes ships. The amateur bug was still in him, for at one time, when anchored in Boston Harbor, he tuned the ship's 5 kw spark transmitter to the amateur 200 meter band and let it go, causing quite some commotion to say the least. "What foolish things young squirts do but how pleasant to recall when one is older," he told me with a far off look in his eyes.

Needless to say that when amateurs were again permitted to return to the airwaves on September 26, 1919, he was one of the first to be back renewing old friendships and making new acquaintances. After his stint as shipboard radio operator he returned home with the desire to have that station of his as complete and commercial looking as his ability would warrant and pocketbook permit. His interest in ham radio has never lagged and today a young man's dream of years ago has finally been realized . . . 100 countries on 160.

Stew went on to college graduating in 1926 from the Massachusetts Institute of Technology and became a Registered Professional Engineer working on heavy industrial equipment for the Worthington Corporation. His knowledge has been put to use on Steam

Power Plant Equipment, Diesel Engines, Gas Engines, Compressors and Pumps.

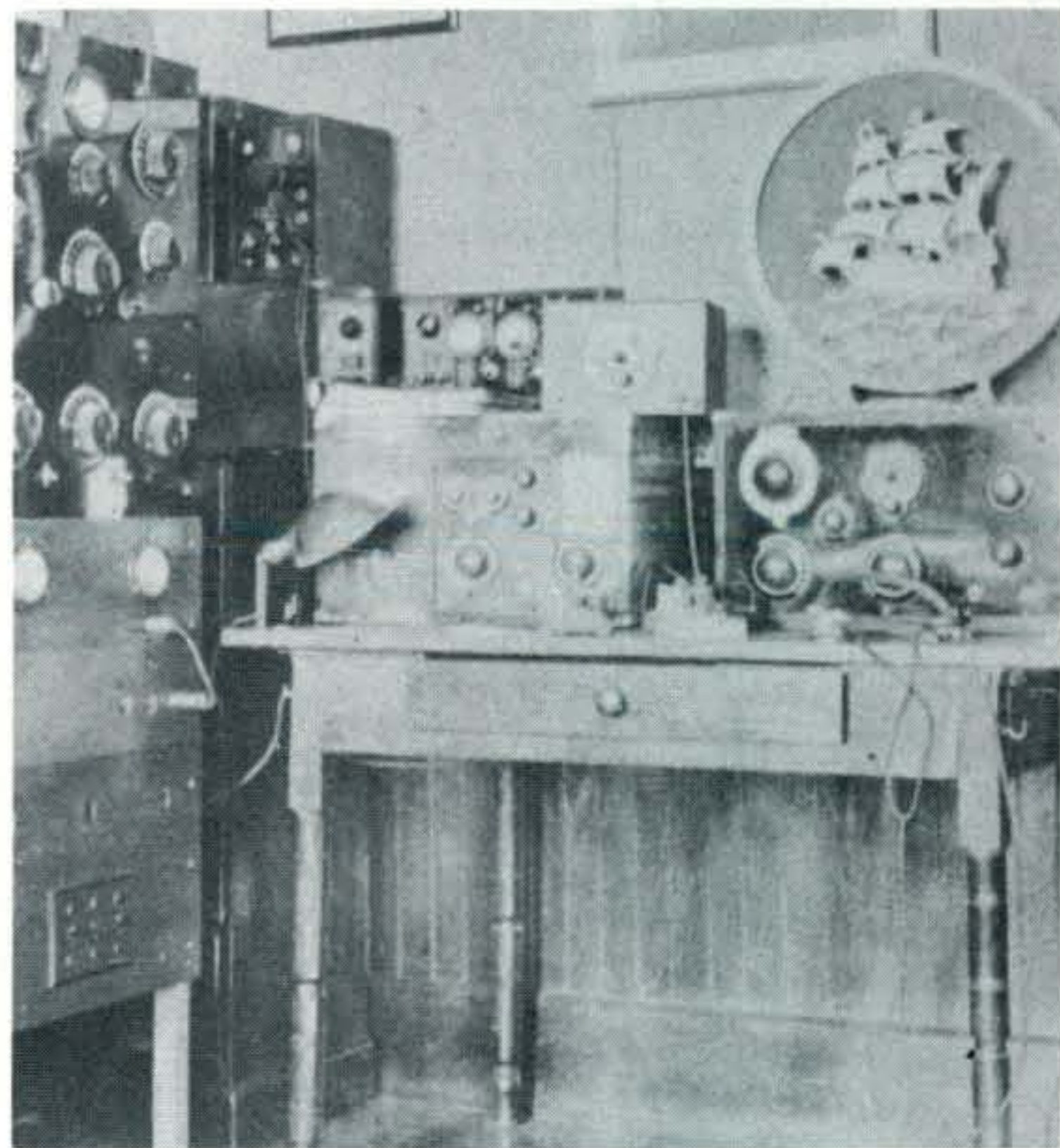
Let us return, for a moment, to those earlier days and note the changes in ham gear as more and more was learned of this mystifying hobby of amateur radio.

Going from the original spark coil, to a 1" coil, to a 3" coil, to a rotary gap and quenched gap rigs, W1BB had one of the very first c.w. transmitters as early as 1921; then, one of the first phone transmitters. In reminiscing, he told me of the first dance via radio ever had anywhere from a Victrola in the shack at his home in Winthrop fed into his mike to a party at the Wollaston Yacht Club in Quincy, Mass., a distance of 7 miles, where it was received and put out over the primitive P.A. system much to the delight of all as "three feature dances of the evening."

Throughout the years most of W1BB's equipment has been home brew although commercial receivers are used now as well as some transmitting and accessory equipment.

Stew's location for a 160 meter installation is without peer being located on a peninsula enclosing Boston Harbor and situated 6 miles northeast of the city of Boston. The antenna is an inverted Vee with its apex 265 feet above salt marshland thereby giving him the most effective type of ground for low frequency transmitting and receiving purposes.

His charming wife, Alice, is also a ham being licensed as W1DQF. "If you can't beat



This 1931 photo of W1BB shows the professional looking station which saw the start of the 160 Meter Trans-Atlantic Tests the following year.

'em, join 'em." And, this is exactly what she did. Much better to be on the inside looking out than vice versa.

When Pearl Harbor was bombed December 7, 1941, amateurs were again ordered off the air by that night. For the duration of WW II, Stew was Operations Officer in the U.S. Coast Guard Auxiliary known as the Radio Sealing Unit whose duties were to go aboard all ships in Boston Harbor checking to be sure their transmitters were properly tested and sealed and complying with all rules and regulations. His group would board ships from a Coast Guard launch, going up and over the side.

W1BB has always been active in amateur emergency work, too, having been ARRL's Emergency Coordinator for years in Winthrop and as RACES Communications Officer of the Civilian Defense Radio Network since its inception at the end of WW II.

During the war LORAN came into existence and was assigned spot frequencies within the 160 meter band of 1850, 1900 and 1950 kcs. This spelled doom for Top Band . . . temporarily. However, sharing arrangements were eventually worked out with the Coast Guard and approval was given for the resumption of amateur communications in April of 1949. Naturally one of the first signals heard was that of the old reliable W1BB, who, as always, has been a mainstay during the ensuing 19 years of 160 meter operation. His greatest love in amateur radio has been the 160 Meter trans-Atlantic DX Tests which, if memory serves correctly, he has been conducting ever since 1932. During these years he has stirred up tremendous activity in various countries throughout the world by getting them to try 160; yes, stations from every continent in the world. Many countries are active on 160 which are considered rare on any band including 10, 15 and 20 meters.

W1BB will be heard during the late evening/early morning hours particularly during the winter and, to a lesser degree, the summer, as well, looking for those evasive countries. Working them on such a low frequency band has given him some of the greatest thrills an amateur operator can experience. It instills within him that feeling of pioneering and accomplishment which is lacking in much of our other h.f. operations today. The Tests conducted by Stew have developed into a "Propagation Study of 160 Meter Signals" with amateurs cooperating from all over the

world lending to the fund of information being compiled about communications in the 2nd region. Noise level, skip paths, weather, etc. are carefully studied, charted and recorded.

Stew is also the first U.S. amateur to obtain the 160 WAC achievement accomplishing this back in 1960. To this day there are less than a handful who can make similar claim and most of these earned their WAC only after the recent trip Stew and Alice made to Japan to introduce 160 meters to many of the JA gang.

Top Band, as 160 meters is familiarly known, is essentially a night time band requiring a darkness path. Best DX is worked an hour before or after local sunrise or sunset at either or both ends. Reflection of 160 meter signals by the ionosphere are best noted during its most turbulent condition when changing its altitude from daytime to nighttime and vice versa. During this period the signal's reflection angle varies widely. It is at this time that a far away signal arises mysteriously from what would seem to be out of nowhere. On the other hand, DX will exist when ionospheric conditions are right as long as there is a darkness path. Much has been learned concerning the peaking times of the North/South and East/West paths, polar absorption and effects of the sunspot cycle.

Stew's greatest pleasures have been through his operations on 160 . . . the personal con-

*[Continued on page 99]*



Stew and Alice Perry, she's W1DQF, at the rig in 1966.

# USING THE GRID-DIP METER

## Part III

WILFRED M. SCHERER, W2AEF

Center-loaded antenna resonance may be found with g.d.o. coupled to *bottom* end of loading coil.



**T**HIS series of articles on using the grid-dip meter will be concluded with applications on transmission lines and antennas.

### Transmission Lines

The length of quarter-wave and half-wave transmissions lines may be determined as follows:

**Quarter-Wave Shorted Lines:** Use g.d.o. coupled to open wire lines as shown at fig. 2I (in Part I) and to coax lines as at fig. 2H (in Part I). When lines are trimmed for correct length, the fittings to be eventually used for connections should be installed on the end of the line. The approximate required length of the line may initially be determined by rough calculation, taking into account the propagation constant. Additional resonant

points will be found at a frequency three times that of the fundamental quarter-wave, where the line is then three-quarter waves long; or five times the frequency for a five-quarter-wave line, etc.

**Quarter-Wave Open Lines:** For open-wire lines connect a short at one end and measure as for quarter-wave shorted lines. Due to the length of the short, the actual electrical length of the line (used as an open-line) will be slightly in error depending on the line spacing. The closer the spacing, the smaller the error.

For coax lines, place short on line and measure as quarter-wave shorted line. The short should be as direct as possible from the inner conductor to the shield to avoid errors. Fittings also should be included. Shorts should be removed after measurements are completed.

**Half-Wave** For open-wire or coax lines, measure for quarter-wave shorted line at *half* the calculated or desired frequency. The resonant frequency thus found must then be multiplied by 2 for a resulting half-wave shorted line.

**Half-Wave Open Lines:** For open-wire lines couple g.d.o. at center as shown at fig. 2J (in Part I). For coax line, short one end and measure for quarter-wave shorted line at half the calculated frequency. Resonant frequency thus found must be multiplied by 2 for correct length of the line after the short is removed; provided, the short was made direct as mentioned above.

A large-size 8½" × 11" frequency vs. capacitance chart for determining capacitance using a g.d.o. and a standard inductance is available from CQ free in return for a self-addressed and stamped #10 envelope. The chart was shown in reduced size last month on page 31.



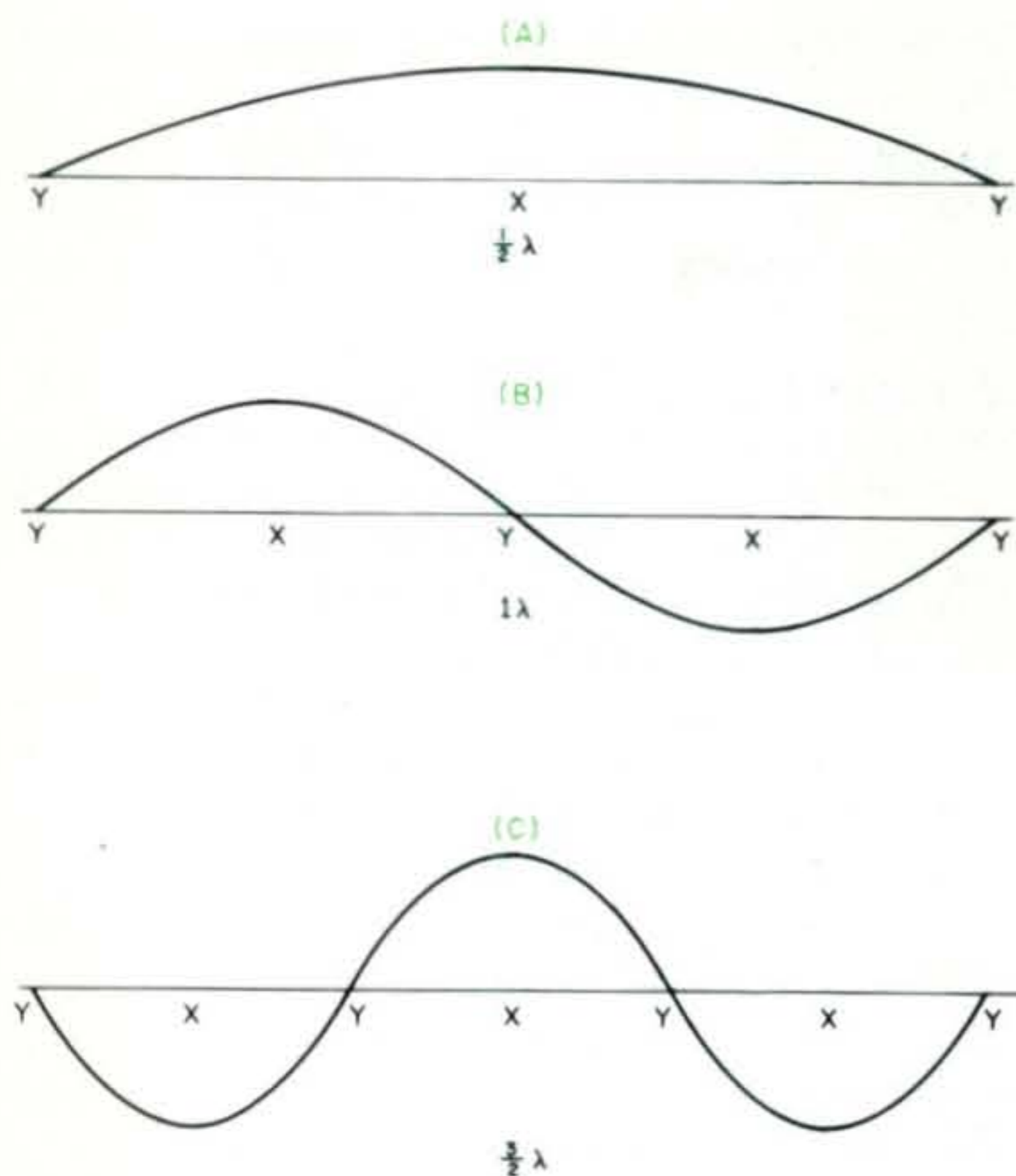


Fig. 1—Current distribution on various-length antennas. A—One-half wave. B—One full wave. C—Three half waves. The g.d.o. preferably should be inductively coupled at the low impedance points marked X. Capacitance coupling is obtained at high-impedance points Y.

**Checking Standing Waves:** Open-wire feed lines may be checked for the existence of standing waves by using the instrument as a diode detector. A flat line is indicated when the meter reading remains constant as the g.d.o. inductor is moved along the line. Care must be taken to maintain a uniform distance or coupling between the line and inductor. Since the g.d.o. inductor often is protected with an insulated sleeve, it may be held against the line for keeping the coupling constant.

This method is like that using a neon bulb or similar device, except better accuracy can be had since the variations can be more easily seen on a meter.

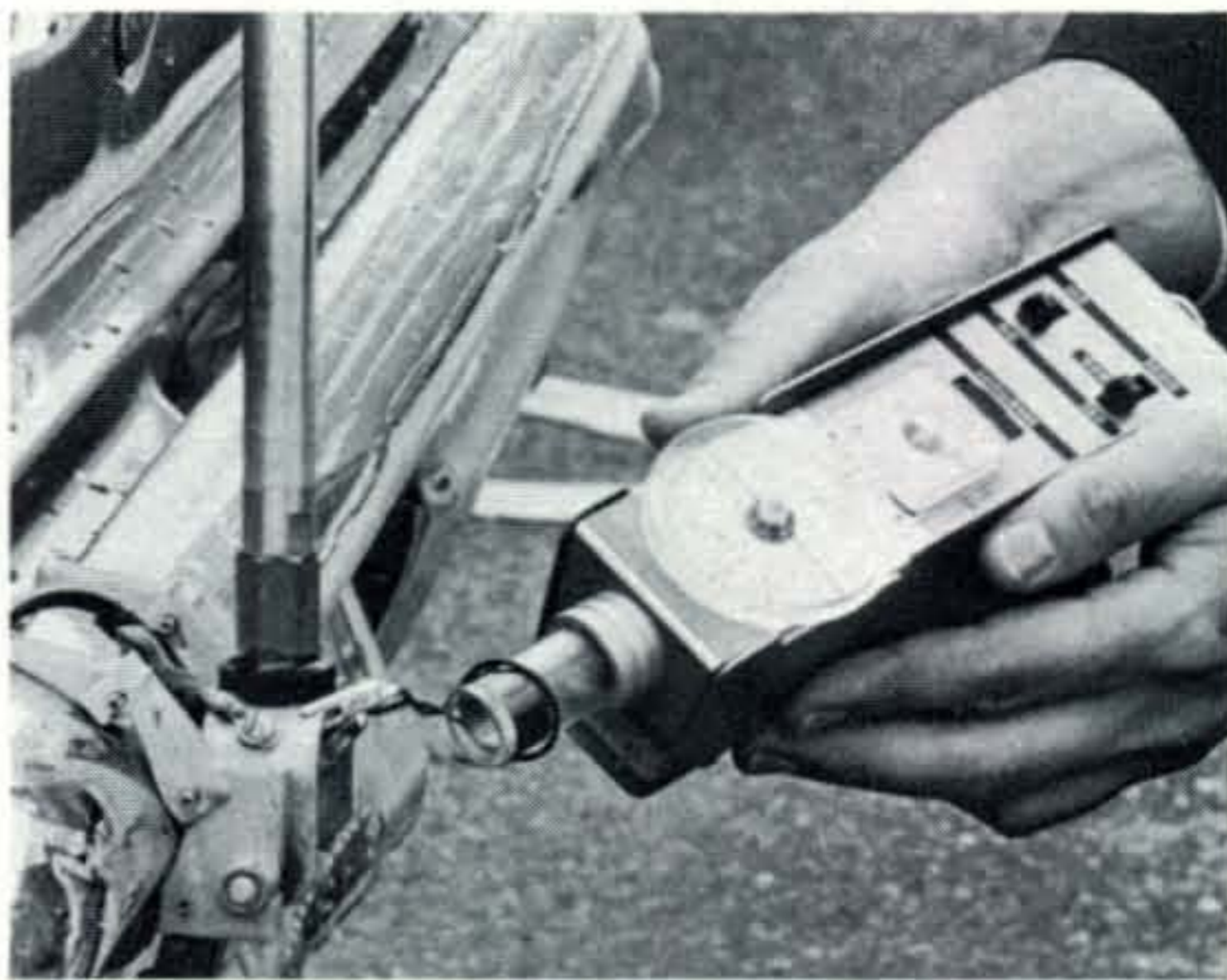
**Antennas:** Use instrument as g.d.o. Coupling should be made at a low impedance or high current point as shown in Fig. 2F (Part I). This point, for a half wave antenna or one a number of odd half-wave lengths long, is at the center. For antennas an *even* number of half-waves long, a low impedance point will be found at a quarter wave measured from either end. Also, see fig. 1. It will be observed that a full-wave antenna will not be a half-wave at exactly half its resonant frequency. This is because the end effects are

found only at the antenna ends and will be absent at other points when the antenna is a full wave or more long. Measurement should be made with the antenna placed as near as possible to its ultimate operating position. Checks on a given antenna at different heights or positions will show an amazing difference in antenna resonance.

If it is physically impossible to reach a low impedance point, a check may be made at a high-impedance or high-voltage point. See fig. 1. Capacitive coupling should be used as shown at Fig. 2G (Part I). If the high impedance point involved is one of the ends, the end effect will be altered due to the presence of the instrument and the resonant frequency of the antenna will slightly decrease. This must be taken into consideration when making measurement, *i.e.*, the reading indicated will be slightly lower than true antenna resonance (with g.d.o. away from end). This difference will be about 1 to 3% and will be encountered only when checking at the ends.

In all cases it is helpful to keep in mind the physical length in feet vs. electrical length (half-wave, full-wave, etc.) as calculated approximately by formula. Unlike lumped resonant circuits, antenna harmonics are detected when using the g.d.o. As previously mentioned, these harmonics will not occur at *exact* multiples of a half-wave.

When measurement is made, the feeders should be disconnected from the antennas. Unless the feeders happen to be perfectly matched or terminated, true antenna resonance will not be indicated because unmatched feeders or incorrectly terminated feeders will present either a positive or negative reactance and will, therefore, alter the electrical length.



Mobile antenna checked with g.d.o. coupled to small loop connected between antenna base and ground.

When the antenna element is of very large diameter, such as is often found in beams, sufficient coupling to the g.d.o. may not be obtained and some difficulty will be encountered in finding a reading. This condition may sometimes be relieved by jumping a foot or so of the antenna at the center with a small diameter wire and coupling to this wire.

If the antenna is to be normally used with its center open, close it with the shortest possible wire during measurement. This must be done also with the folded dipole. The short may later be removed, if required, when the feedline is connected.

**Quarter-Wave Vertical Antennas:** With quarter-wave vertical antennas, resonance may be found by disconnecting the transmission line, shorting the feed point to the ground system and using the g.d.o. at the base.

If adequate coupling cannot be realized for a dip indication, where possible, reverse the inductor 180° when it is plugged into the g.d.o. or otherwise orient it in relation to the antenna element as suggested in Part I. If this fails to provide the necessary coupling, then connect a small one or half-turn loop instead between the antenna base and ground using as short leads as possible (to minimize detuning of the antenna).

If the antenna has a center-loading coil, the g.d.o. may be coupled along the lower portion of the antenna element while the base is grounded. Readings also may be obtained with the g.d.o. coupled near the *bottom* of the loading coil, but care must be taken to see that body presence (particularly above the loading coil, does not detune the system. Base loading may be similarly checked while following these precautions. Unloaded antennas will exhibit a fairly broad dip and loaded an-



Method of coupling g.d.o. to shorted twin lead.

tennas will produce sharper dips due to their higher  $Q$ .

**Mobile Antennas:** Mobile antennas usually are the quarter-wave vertical type, requiring the use of the g.d.o. as described above for such antennas.

**Parasitic Beams:** Tuning a parasitic beam for maximum gain or best front-to-back ratio cannot be very well done using the grid-dip meter; however, the determination of other characteristics may be helpful and can be accomplished as follows:

Parasitic beams may initially be adjusted using the g.d.o. to check the frequency of each element. The driven element should be resonated to the operating frequency, while the directors are tuned slightly lower in frequency and the reflector slightly higher. These elements may be checked individually using the g.d.o. coupled at the center of the element. The feedline and any matching device should be disconnected and if the center of the driven element is open, temporarily place a short across this point.

Since the various elements are coupled together according to the spacing between them, several dips may be observed on any one element and may be indicative of the resonant frequency of the other elements. The most pronounced dip will be that related to the element under test. When changes are made in the length of one element, interaction may shift the resonant frequencies of the other elements. This then is a give-and-take proposition. The final result should be one that produces the most pronounced dip as possible on the driven element at the operating frequency with the least indication of dips from the other elements.

Final precise adjustment should be made, particularly if a matching system is to be employed at the antenna, by using an s.w.r. bridge or a variable-impedance bridge driven by the grid-dip meter used as a signal source with it's being coupled to the bridge through a one or two turn loop. The coupling to the instrument should be as little as possible consistent with obtaining a useable reading, otherwise the oscillator frequency may slightly shift; as a matter of fact, an occasional frequency check of the signal on a receiver will be advisable.

**Trap Antennas:** Trap antennas may be set up by first adjusting the individual traps for the proper resonance, before they are installed, as explained under parallel-tuned traps. After

[Continued on page 106]



### The DX Award's Program

**WAZ:** Worked All Zones was the most popular award this month, with 34 new certificates authorized between April 1 and April 30. There was an unusually large crop of 2-way s.s.b. applications. In fact there were as many s.s.b. WAZ's as there were c.w.-phone WAZ's, 15 each. This was exceptional as the c.w.-phone category normally has many more applicants than either 2-way s.s.b. or phone. S.s.b. has definitely come of age. The new certificate winners were the following:

**WAZ 2-Way S.S.B.:** W8GGE-524, LU2CF-525, W4FPS-526, W0SFU-527, W9DNE-528, VP7NA-529, W0PAN/KH6-530, WA0KDI-531, K8IKB-532, W8ROC-533, DL3AA-534, K3HHY-535, K0BHT-536, WB6CPE-537, WA3ATP-538.

**WAZ C.W.-Phone:** F3CT-2409, WB2GHI-2410, W3AG-2411, WA9KQS-2412, W1RLV-2413, W4KJL-2414, DL7HC-2415, DJ4XA-2416, W9UTQ-2417, W4AQW-2418, W7YEX-2419, W1AGF-2420, K4BAI-2421, W5OBS-2422, K8ANA-2423.

**WAZ Phone:** W0MGI-376, W9HPS-377, DL9RE-378, W9ZTD-379.

**WPX:** The prefix chasers were also busy this month, with 16 new certificates authorized and 24 endorsement stickers sent out. The winners were:

**WPX C.W.:** K9DWG-842, W3AIZ-843, K6SDR-844, W6QFU-845, K9QVV-846, DJ4SK-847.

**WPX S.S.B.:** YV3KX-331, W8GGE-332, OE1KW-333, W4UF-334.

**WPX Mixed:** W9GFF-165, W6LDA-166.

**WPX Phone:** W4HA-150.

**S.S.B. CONTEST WPX:** F9MS-3, SM7CSN-4, SM5AD-5.

**WPX Endorsement Stickers:** Continent-Europe: SM7CSN, K3QVV. North America: W6CHY. Africa: PA0SNG.

**Band-7 mc:** YU1AG. 3.5 mc: YU1AG.

**Mode-Mixed:** W9GFF-700, YU1AG-600, W9ZTD-550, W4HA-550. **S.S.B.:** WA5LOB-500, W6LDA-350, YV3KX-350, OE1KW-350, YV4QG-300. **C.W.:** W4NJF-700, VK3AHQ-650, YV1AG-600, UC2AR-600, W9ZTD-400, I1ZQ-400. **Phone:** PA0SNG-650, W6CHY-550, W4HA-500.

The response to our April request for suggested prefixes to include on the standard list for the WPX Honor Roll has been truly grati-

\* P.O. Box 205, Winter Haven, Florida 33880.

fying. Mike, WA8GGN, sent 5 typewritten pages (single-spaced) discussing the various possible additions and deletions, and old standbys like W9WHM, W4OPM, W6TMP, W8KPL, K4DSN, K2DDK, WA1CBP, K3HGX, *et al.*, also made helpful contributions. The remaining prefixes for this list will be published next month, and hopefully the special forms for application to the Honor Roll will be available shortly thereafter. Anyone wishing to receive a WPX Honor Roll application as soon as they are ready should send an s.a.s.e. to K4IIF. The business size envelope is preferred. The cut-off point is difficult to predict at this time, but if you have over 500 of the prefixes on the standard list confirmed in any of the 4 WPX categories you may be eligible.

**S.S.B. DX Awards:** There were only 5 new certificates authorized during April, but as we move into May the tempo of applications is picking up. Award custodian W8HDB is doing an excellent job of reorganizing the files, and plans to come out with a better application blank in the near future. The S.S.B. DX Honor Roll will be a regular feature, and will list everyone with at least 250 countries confirmed. Applications and requests for information should be directed to Louise Rippe, W8HDB, 3785 Susanna Drive, Cincinnati, Ohio 45239.

The new certificate winners were:

**100 Countries:** G3PQF-508, K8DBW-509, OK3DG-510.

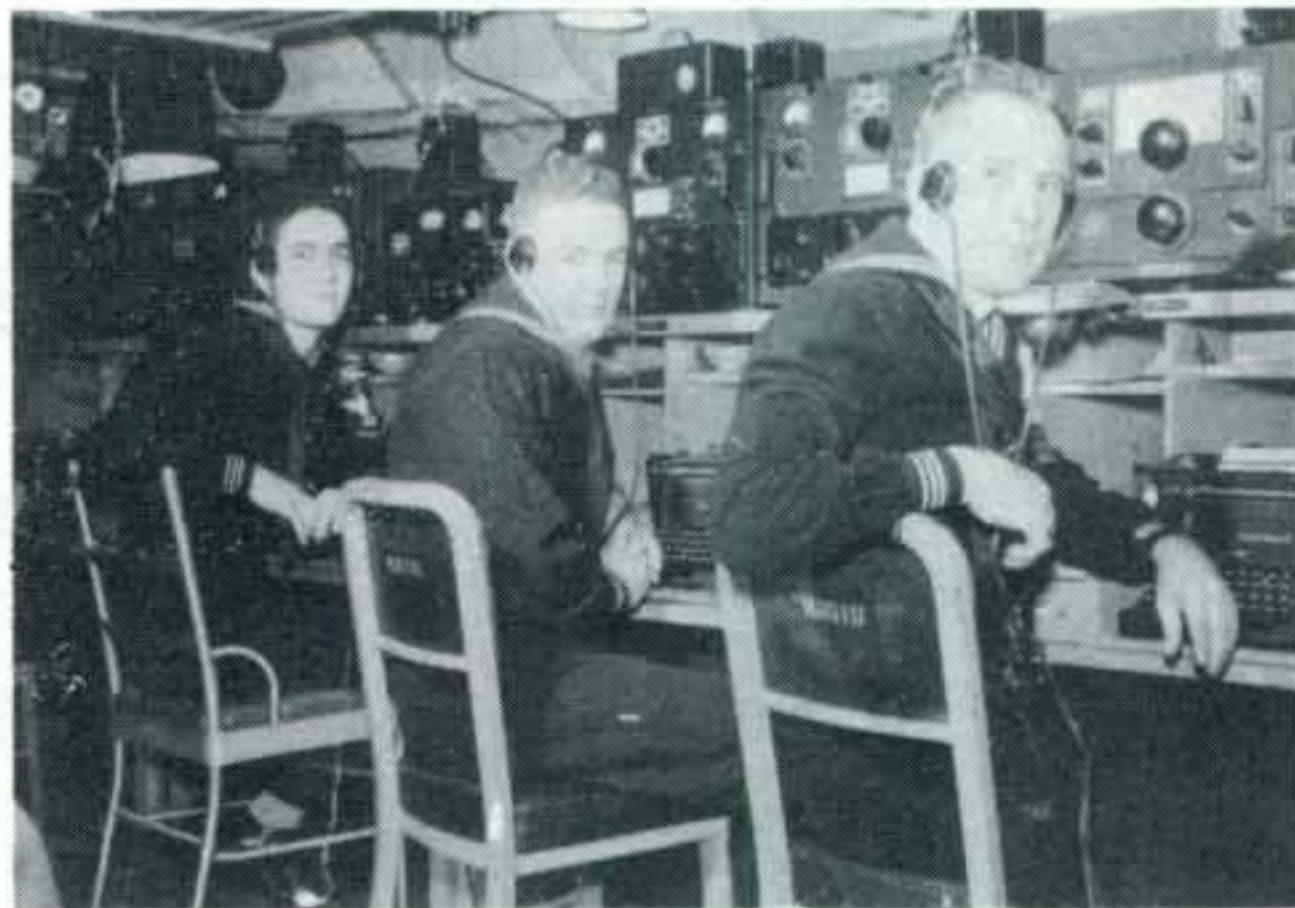
**200 Countries:** DL9CQ-152, K6CAZ-153.

### S.S.B. DX HONOR ROLL

VK3AHO ... 314	WA8AJI ... 300	WA21ZS ... 293	W2LV ... 271
WA8AJI ... 312	WA2RAU ... 300	W2VCZ ... 291	G3NUG ... 270
W2TP ... 307	W4SSU ... 300	K1IXG ... 289	K8ONV ... 270
W2ZX ... 307	K6ZYG ... 300	K8RTW ... 288	G2PL ... 266
T12HP ... 306	W4PAA ... 300	W1LLF ... 282	W6YMV ... 265
W0QVZ ... 305	I1AMU ... 300	W6UOU ... 282	G2BVN ... 264
K4TJL ... 305	W5KUC ... 300	W3KT ... 282	W3DJZ ... 263
W2BXA ... 304	KP4CL ... 300	W7DLR ... 277	G3DO ... 260
G3AWZ ... 303	G6TA ... 300	DL1IN ... 276	W6WNE ... 260
G8KS ... 303	W8EVZ ... 300	HB9TL ... 276	WA2EQQ ... 259
5Z4ERR ... 301	K2MGE ... 300	PZ1AX ... 275	PJ2AA ... 258
K6CTG ... 301	W3NKM ... 296	W6RKP ... 274	K1SHN ... 257
W8PQQ/ ... 300	W2RGV ... 296	K9EAB ... 274	K6CAZ ... 254
W8BT ... 300	W2FXN ... 294	W4SSU ... 274	K6LGF ... 251
W4OPM ... 300	W3MAC ... 293	DL3RK ... 273	W1AOL ... 250

### De Extra

**Deliberate Interference to Contest Operations:** This column has always felt that there were two sides to all questions. As a consequence it has gone to great lengths to be fair to each viewpoint. However, on this subject there is no in-between ground. The line between right and wrong is cleanly drawn with no gray area in the middle. Deliberate interference is wrong, bad wrong.



Here are "fore and after" shots of one of our real OT DXers, Ray, W2BA1, of Passaic, New Jersey. Ray was first licensed in 1928 as W2AMR and got back on the air again 3 years ago as W2BA1. He recently qualified for WAZ. On the left is Ray as he appears today, while on the right is Ray in 1943 operating in the Mediterranean Theatre as a Navy Radioman First Class.

For many years there has been a small clique of lids who have done their best to disrupt communications during DX contests, particularly on the 3.8 mc band. Phone DX-ing on this band has traditionally been confined to the frequencies between 3800 and 3805 kc. This is quite logical as 3800 is the lower limit of the U.S. phone band. Consequently, the DX stations, who frequently operate with very low power, can transmit between 3795 and 3800 and listen just above their own frequencies for W,K responses. This arrangement is generally quite effective, except for three weekends out of each year. These are the two weekends of the ARRL Phone DX Contest and the weekend of the CQ World Wide Phone DX Contest. Unfortunately, on these three weekends the loud-mouths have their field day.

In past years the stream of profanity which these characters have used in vilifying the contest entrants has been beyond belief. All one could do is shake one's head in pity that any person's mind could be that sick. Hippies to the contrary, four-letter words don't make great literature. It seemed pointless to report the matter to the FCC as it was inconceivable that anyone would say such things and then sign his own call. However, somebody must have felt differently because back about '64 or '65 an FCC monitoring station in Texas showed up for the 2nd phone weekend of the ARRL contest and things got squared away fast.

However, in this year's ARRL contest the lids were back in force, and while their language was cleaner their tactics were just as reprehensible. A difference this year from this columnist viewpoint is that he was hearing how it sounds to the stations in other coun-

tries, and it was a pretty sad thing. Yours truly was at Bahamian station VP7NA as a guest operator for about 12 hours of the contest. Shortly after midnight EST we got on 3795 kc to give the boys their 80 meter multipliers. It wasn't long before company arrived in the form of some crude, immature types who decreed that "there would be no DX contacts on 80 meter phone that night, no sir." They immediately spread out over the lower 10 kc of the band making meaningless noises in an attempt to disrupt communications. One of their favorites was the endless recitation of what they claimed were zipcode numbers. I'm sure the postoffice department didn't assign these numbers with the idea that they be used to interfere with legitimate, international communications.

After a while it became obvious that their scheme was not succeeding. Serious contesters generally have the best antennas and the loud-mouths simply couldn't cut the mustard. However, VP7NA and the other DX stations were working under different rules. In the Bahamas the power limit is 100 watts, and we were observing this limit strictly. When things began to go bad for the lids some self-appointed field general was heard to say "Go down and get that d—— VP7." Immediately two loud carriers appeared below 3800 taking out the signals from VP7NA and the other DX stations as well. VP7NA simply QSYed to 7 mc until after the children had gone to bed. However, some DX-stations threw in the towel and went QRT. One was heard to ask "Why do these crazy Americans try to break up the contest sponsored by their own national amateur radio society?" A hard question to answer isn't it!

The contest was over months ago, and this

editor has thought long and hard about the advisability of writing this editorial. It amounts to hanging our own dirty laundry out for public view. This is generally a bad policy. However, the hour may be late so desperate measures are in order. The FCC regulations refer to the "amateurs unique ability to enhance international good will." Believe me, if we keep enhancing international good will as we do on 80 meters during DX contests there soon won't be any amateur radio around to enhance any good will, international or otherwise.

### DXpedition QSLs

As of April 18, 1968, Art Altemiller, WØBN (ex-WØQKC) is the exclusive QSL Manager for all of Don Miller's operations from 1965-1968. Art's address is 8713 Charlton Lane, Affton, Mo. 63123. If s.a.s.e.'s or sufficient IRC's are sent cards will be answered by direct mail. Otherwise, they will go via the bureaus.

### Re 3W8 Contacts

The following letter pertaining to the K8NHW/3W8 operation was received by W3AES and forwarded to CQ by WA3ATP:

"In reply to your letter dated March 6, 1968, please be advised that the South Vietnam operation by amateur radio station K8NHW does not appear to have received the necessary authorization from the South Vietnam government. Accordingly, the Commission will not permit United States amateur operators to communicate with that station.

Sincerely yours,  
James E. Barr, Chief  
Safety & Special Radio Services Bureau  
FCC"

This letter was dated March 17, 1968. If anyone has any later information we will be glad to have it.

### Here and There

**CE9, South Shetland Islands:** CE9AT is quite active evenings on 20 meter s.s.b. He frequently makes skeds through an m.c. (master of ceremonies), QSL to CE3ZN. (Tnx WATTS).

**EA6ITU** was on the air from April 29 to May 10, 1968 from Palma de Mallorca. Over 1000 QSO's were made on 15 and 20 meters. QSL's are in preparation and should be out by late June or early July. QSL manager, c.w., W4BV; phone, W3MR or W3ASK.

**ET3, Ethiopia:** ET3FMA (ex-K4FMA) likes

14215 kc s.s.b. around 0230-0300 GMT. (Tnx LIDXA).

**F4, France:** It is unlikely that there will be any F4's in the near future as the French P.T.T. has begun to issue 3-letter F6 calls, i.e. F6ABH. All F7's are probably off the air as these were U.S. servicemen in France. (Tnx WA9FZQ/FØCV).

**HC8, Galapagos Islands:** Rolf, HC8RS, is active on 14 mc s.s.b. from 2200-0100 GMT using a transceiver. QSL to SM5EAC. (Tnx WATTS).

**HL9, Korea:** HL9US with operators Paul (WA3EHT), Bob (WAØFIX), and Grant (WB6POH) will be very active on 15 and 20 meter c.w. and s.s.b. They will be keeping daily skeds on 14215 kc at 1130 GMT, and will be available for QSOs when these skeds have been finished. (Tnx Tom Armstrong).

**I5, Italy:** I5IJ during the CQ WPX fone contest was operated from Rome by Tony, I1IJ, with a special prefix for the contest only. (Tnx I1IJ).

**JT1, Mongolia (Zone 23):** The following stations have been reported active: JT1AJ 14195 kc at 1445 GMT, JT2AB 14040 kc at 1221 GMT, and JT1KAA 14057 kc at 0250 GMT. QSL via Box 639, Ulan Bator, Mongolia. (Tnx LIDXA).

**JW7, Svalbard:** JW7YF was worked on 14150 kc s.s.b. (Tnx DX-MB).

**KH6, Kure Island:** KH6EDY is active on 20 meter s.s.b. from 0400 GMT. (Tnx GUS).

**KW6, Wake Island:** KW6EJ is active around 14200-210. QSL to W2CTN. (Tnx WATTS).

**LAØ, Norway:** Bob Snyder, WØGTA/LA, now is licensed at LAØAD. Bob will be remembered as WØGTA/8F4 and 9V1LP.

**PK, Indonesia:** This country is now available on s.s.b. PK1SH has been reported on 14105 kc and PK8YAK on 21310 and 14124. (Tnx VERON).

**SK6, Sweden:** SK6 is the new prefix for Swedish club stations. This is a new one for WPX.



DX Editor K4IIF with VP7NA at the QTH of VP7NS.

**ST2, Sudan:** Ibrahim, ST2SA, is still the only station making the Sudan available. He likes 14024 and 21035 kc c.w. (Tnx VERON).

**TA, Turkey:** TA1AV, TA1KT, and TA1QR are QRV on 20 meter c.w. and phone around 2100-2200 GMT. (Tnx DX-MB).

**VK2, Lord Howe Island:** VK5XK/VK2 reports that many QSLs sent were apparently destroyed in a post office fire. If yours didn't come through, send Arch another. (Tnx VERON).

**VO2, Zone 2:** VO2AC is active on 10 and 20 meter s.s.b. mostly in the Canadian band, G3UHR/VO2 is on 10 and 20 meter s.s.b., and VO2AB is on 20 meter s.s.b. between 14100 and 14200. VO2AB will be happy to go above 14200 for anyone who needs Zone 2. (Tnx VO2AB).

**VP2, St. Vincent Island:** VP2SY is on 20 meter s.s.b. between 14200 and 14220 evenings from 0040-0315 GMT. (Tnx LIDXA).

**VR6, Pitcairn Island:** VR6TC has a sked on Tuesdays at 2100 GMT on 21350 kc s.s.b. Wait until the sked is over before trying for a QSO. (Tnx GUS).

**VS9, Maldiv Islands:** VS9MB is the only station now active from the Maldives. Listen around 21050 kc c.w. and 21350 kc s.s.b. (Tnx VERON).

**XP1, Greenland:** XP1AA is frequently on the air Sundays. His favorite frequency seems to be 14290 kc s.s.b. (Tnx DX-MB).

**YA, Afghanistan:** YA1ZC has been reported around 21052 kc c.w. between 1500 and 1800 GMT. QSL to Box 639, Kabul, Afghanistan. (Tnx GUS).

**ZD7, St. Helena Island:** ZD7FF was worked on 14199 kc s.s.b. at 2319 GMT. (Tnx LIDXA).

**ZM7, Tokelaus Islands:** To be activated by VE7PY during the CQ WW Phone DX Contest in October. (Tnx GUS).

**ZS3, South West Africa:** ZS3LU is active on c.w. near 14013-015 kc. (Tnx VERON).

**3V8, Tunisia:** 3V8TA was heard on 21152 kc at 1935 GMT. (Tnx LIDXA).

**4A, Mexico:** This prefix will be used by Mexican stations during the Olympic year and will be a new one for WPX. The station working the most 4A's will receive a gold medal, the second highest number a silver medal, and the third highest a bronze medal. For further information contact 4A2YP (XE2YP). (Tnx GUS).

**5A3, Libya:** 5A3TP has been reported from Benghazi on 14051 kc c.w. (Tnx VERON).

**60, Somali Republic:** Bee Walton, ex-

606BW, is now in Alaska as KL7GFN. (Tnx GUS).

**7Z3, Saudi Arabia:** 7Z3AB is on the air daily between 1200 and 1300 GMT. Preferred frequencies are 14190 kc for s.s.b. and 14035 kc for c.w. QSL via W4YDD. (Tnx GUS).

### QSL Information

As it is almost impossible to stay up-to-date, all QSL Managers are urgently requested to notify the DX Department of all additions and deletions to their lists.

AP2MR—Via VE3ACD.

CE0AE—c/o WA5PUQ.

CE0PK—To WB6CDX.

CN8FV—Via W2GHK (D.O.T.M.), not via W2CTN.

CR5SP—c/o W2GHK.

CR6IK—To K3ZVM.

CR7IC—P.O. Box 135, Porto Amelia, Mozambique, East Africa.

CT1JJ—Via W6LDA, 6158 W. 74th St., Los Angeles, Calif. 90045.

CT2AA—Via WA0OMN, 1116 Hilliard Rd., St. Louis, Mo. 63122.

EA4CX—c/o WA0CEL.

EA0AH—To W4DQS.

FG7II/FS7—Via VE3EUV.

FG7TG—c/o W5BUK, 2609 Halsey Ave., New Orleans, La. 70114.

FO8BQ—To WA6WMG, 251 Lurelane St., Rialto, Calif.

FO8CA/p—Via F2RS.

G3XEM/HZ—P. K. Booth, c/o Airwork Services, Ltd., P.O. Box 2142, Jeddah, Saudi Arabia.

HB0LL—c/o WA4QVQ.

HL9US—QSOs since March 28, 1968 via T. R. Armstrong, 365 Whitten Hollow Rd., New Kensington, Pa. 15068.

HV3SJ—To WB2ETI.

HZ1AT—Via G3DYY.

I5IJ—c/o I1IJ, 10 Piazza Bologna 00162, Rome, Italy.

I7RUI—To I1ZIZ, Via Gustavo Modena 13, Firenze, Italy.

I8CLC—Via I1CLC, Via Del Cappuccini 12, Firenze, Italy.

IT7GAI—c/o IT1GAI.

JT1AG—To UA1CK, Vladimir Cuploon, P.O. Box 2, GPO, Leningrad, USSR.

JW2BH—Via LA5YJ.

JX7RR—c/o LA7RO.

KG6IC—USCG Loran Station, APO San Francisco, CA 96415.

LA0AD—To W2CTN.

MP4MBC—Via G3HSR, 11 The Crescent, Milton, Weston-super-Mare, Somerset, England.

OD5EP—c/o WB2ISL.

OX3WY—To OZ2BA.

OY7S—Via VE3FYR.

PJ5MJ—c/o W2BBK, 79 Glenwood Rd., Englewood, N.J.

PJ5MM—To K9GCE.

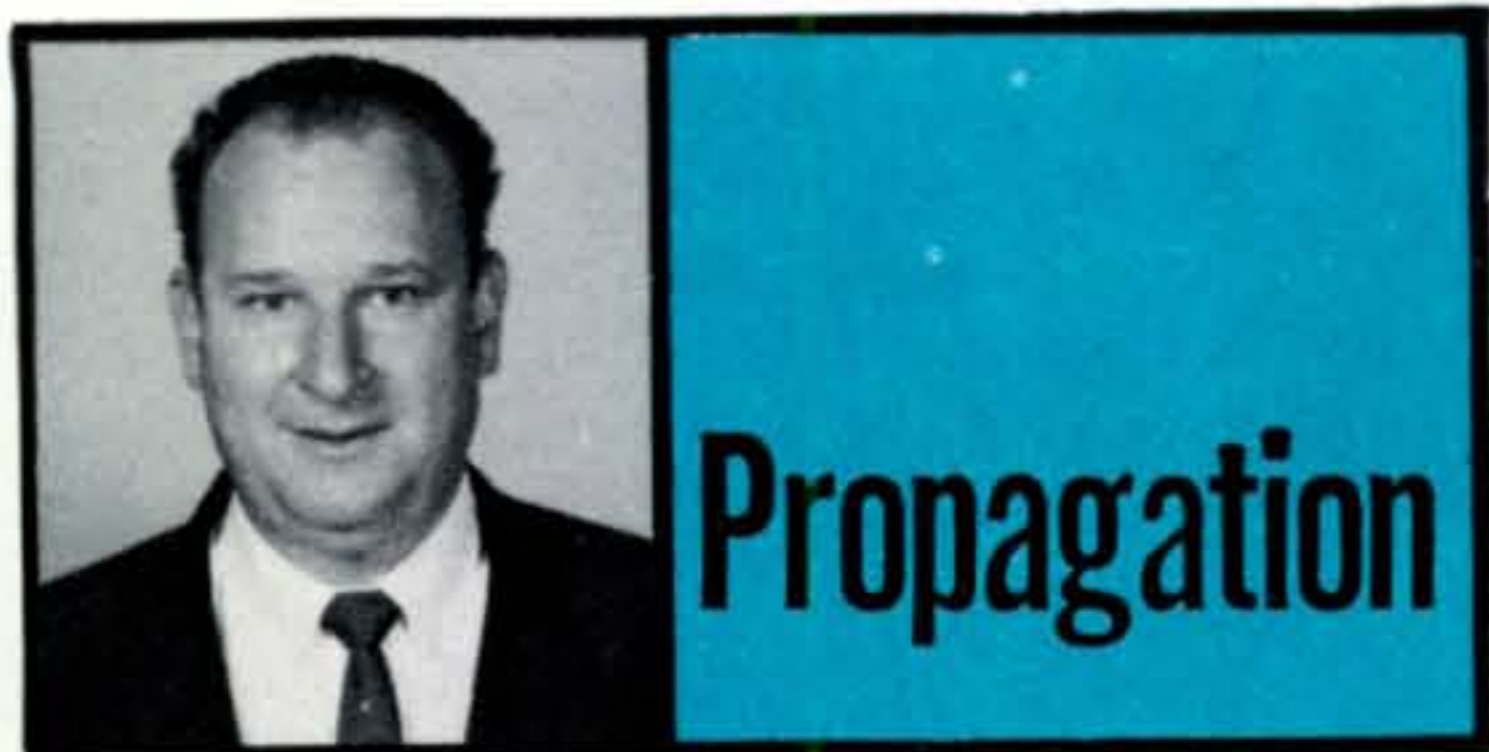
PY0BLR—Via PY4BLR.

SK3AK—c/o SM3CZS.

UA1KAC—To WB4FJO.

VK9GN—Via K7YDO. \*

[Continued on page 112]



BY GEORGE JACOBS,\* W3ASK

**P**ROFESSOR M. Waldmeier, director of the Swiss Federal Observatory has recently predicted that the peak of the present sunspot cycle will occur this month (July, 1968), with a smoothed sunspot number of 110.

This is an earlier date and a somewhat lower value of peak solar intensity than had been predicted previously by Professor Waldmeier, and by other experts. For example, the Editor of this column, in January, 1968 issue of *CQ* (page 93), predicted a cycle peak of 123 to occur during November or December of this year.

It will be several more months, perhaps as long as a year, before the exact date and level of maximum solar intensity will be known with any degree of accuracy. It is certain, however, that maximum solar intensity is near at hand, if it has not already occurred!

The Swiss Federal Observatory reports a monthly sunspot number of 81 for April, 1968. This results in a smoothed sunspot number of 95, centered on October, 1967. A smoothed sunspot number of 114 is predicted for July, 1968 by the Editor of this column.

### July Propagation

Both the 15 and 20 meter bands are expected to share honors for optimum DX propagation conditions during July.

Excellent world-wide openings are forecast for 15 meters throughout the daylight hours, and through the evening hours as well. Conditions are expected to peak on this band during the late afternoon and early evening hours, with excellent openings in almost all directions.

Twenty meters is expected to remain open to one area of the world or another, around-the-clock. Although DX openings should be possible at almost any hour, optimum world-wide conditions are forecast during the early

\* 11307 Clara Street, Silver Spring, Md. 20902.

### LAST MINUTE FORECAST

Day-to-Day Conditions and Quality for July 1 through Aug. 15, 1968

Days	Forecast Rating & Quality			
	(4)	(3)	(2)	(1)
Above Normal: 1, 8, 13, 15, 19-20, 28-29, 8, 12	A	A-B	B	B-C
Normal: 2, 5-6, 9-11, 14, 16, 18, 21-23, 25-27, 30, 3-4, 6-7, 9-11, 13, 15	A-B	B	C	D
Below Normal: 3-4, 7, 12, 17, 24, 31, 1-2, 5, 14	B-C	C-D	D	E
Disturbed: None, None	C-D	D-E	E	E

#### HOW TO USE THESE CHARTS

The following is an explanation of the symbols shown above, and instructions for the use of the *CQ* propagation predictions:

1—Enter Propagation Charts on following pages under appropriate band and distance or geographical area columns. Read predicted times of band openings at intersection of both columns.

2—Following each predicted time of band opening is a forecast rating which indicates the relative number of days the band is expected to open during each month of the forecast period. The higher the rating, the more frequent the opening, as follows: (4) band open more than 22 days each month; (3) between 14 and 22 days; (2) between 8 and 13 days; (1) less than 7 days.

On the "Short-Skip" Chart, where two numerals are shown within a single set of parenthesis, the first applies to the shorter distance for which the forecast is made, and the second to the greater distance. Note the forecast rating for later use.

3—With the forecast rating noted above, start with the numbers in parenthesis at the top of the "Last Minute Forecast" appearing above. Read down the table for a day-to-day forecast of propagation conditions in terms of Above Normal (WWV rating higher than 6); Normal (WWV rating 5-6); Below Normal (WWV rating 4); Disturbed (WWV rating less than 4). The letter symbols (A-E) describe reception conditions (signal quality, noise and fading levels) expected for each day of the month and have the following meanings: A—excellent opening with strong, steady signals; B—good opening, moderately strong signals, little fading and noise; C—fair opening, signals, fluctuating between moderately strong and weak; D—poor opening, signals generally weak and considerable fading and noise; E—poor opening, or none at all.

4—This month's Propagation Charts are based upon a transmitter power of 75 watts c.w.; 150 watts s.s.b., or 300 watts d.s.b., into a dipole antenna one quarter-wave above ground on 160, 80 and 40 meters and a half-wave above ground on 20, 15 and 10 meters. For each 10 db increase above these reference levels, reception quality shown in the "Last Minute Forecast" will improve by one level; for each 10 db loss, reception will become poorer by one level.

5—Local Standard Time for these predictions is based on the 24-hour system.

6—These Propagation Charts are valid through Sept. 15, 1968. These Charts are prepared from basic propagation, data published monthly by the Institute For Telecommunication Sciences And Aeronomy of the U.S. Dept. of Commerce, Boulder, Colorado.

evening, the hours of darkness and the sunrise period.

Some good 10 meter DX openings are expected during July, mainly on north-south paths during the afternoon hours.

During the hours of darkness, 40 meter openings are expected to many areas of the world, but seasonally high static levels may often make DX reception difficult. High static levels are also expected to result in somewhat

poorer DX conditions on 80 meters, although some openings are forecast during the hours of darkness. Not many DX openings are expected on 160 meters during July, because of seasonally high level of static and solar absorption.

Check last month's column for comprehensive band-by-band DX propagation predictions for July.

### Short-Skip

This month's column contains Short-Skip Charts for the period July 15-September 15, 1968. Optimum short-skip conditions on most bands are expected during July, mainly as a result of the seasonal peak expected in sporadic-E propagation. During the daylight hours considerable short-skip openings are forecast for 10 and 15 meters over distances ranging between approximately 500 and 1300 miles, with some double-hop openings extending out to 2300 miles. Frequent short-skip openings on 20 meters, ranging between 250 and 2300 miles, are expected almost around-the-clock, with conditions peaking during the late morning hours and again during the late afternoon and early evening hours.

Good daytime short-skip openings are predicted for 40 meters between distances of approximately 100 and 600 miles, with excellent nighttime openings between 250 and 2300 miles. Good 80 meter short-skip openings are forecast for the daylight hours up to distances of approximately 300 miles, with the range extending up to 2300 miles during the hours of darkness. While no 160 meter short-skip openings are expected during the daylight hours, some openings are forecast during the hours of darkness for distances up to 1300 miles. When static levels are low, 160 meter nighttime openings may extend out to approximately 2300 miles.

### V.H.F. Ionospheric Openings

With a peak expected in sporadic-E propagation, frequent 6 meter short-skip openings are likely to occur during July. Most of these openings will probably fall within the 900 to 1300 mile range, but some may be as great as 2300 miles. The most likely times for these openings are a few hours before noon and again during the early evening hours, although they could take place at any time of the day or night. During many of these openings, signal levels are expected to be exceptionally strong.

Be sure to check the 2 meter band during

intense 6 meter sporadic-E openings, since 2 meters may occasionally open as well. Generally, 2 meter short-skip openings take place between distances of approximately 1000 and 1300 miles.

Some v.h.f. short-skip openings resulting from auroral ionization are also expected during the month. Check the "Last Minute Forecast" appearing at the beginning of this column for periods that are predicted to be disturbed or below normal; since these are the dates that auroral v.h.f. openings are most likely to occur during July.

There is a very good possibility for some meteor-type v.h.f. ionospheric openings to take place during the last week of July, when the *Perseids* and the *Aquarids* meteor showers will take place. The *Perseids* is a major shower, and will extend into August. ■

### CQ Short-Skip Propagation Chart

JULY 15 - SEPTEMBER 15, 1968

LOCAL STANDARD TIME AT PATH MID-POINT  
(24-HOUR TIME SYSTEM)

Band (Meters)	50-250 Miles	250-750 Miles	750-1300 Miles	1300-2300 Miles
10	Nil	07-09(0-1)* 09-13(0-2)* 13-17(0-1)* 17-21(0-2)* 21-23(0-1)*	07-09(1)* 09-13(2-3)* 13-17(1-2)* 17-21(2-3)* 21-07(1)*	07-09(1-0)* 09-13(3-1)* 13-17(2-1)* 17-21(3-1)* 21-07(1-0)*
15	Nil	07-09(0-2)* 09-13(0-3)* 13-17(0-2)* 17-19(0-3)* 19-21(0-2)* 21-07(0-1)*	07-09(2)* 09-13(3)* 13-17(2)* 17-10(3)* 19-21(2)* 21-23(1-2)* 23-07(1)*	07-09(2) 09-13(3) 13-17(2-3) 17-19(3-4) 19-21(2-3) 21-23(2) 23-07(1)*
20	09-00(0-1)*	06-09(0-2)* 09-15(1-4)* 15-20(1-3)* 20-00(1-2)* 00-06(0-1)*	06-09(2-4) 09-15(4) 15-20(3-4) 20-00(2-4)* 00-02(1-3)* 02-06(1-2)*	06-09(4) 09-16(4-3) 16-00(4) 00-02(3) 02-06(2)
40	07-11(2-4) 11-20(3-4) 20-22(2-3) 22-00(1-2) 00-06(0-2)* 06-07(1-2)	07-09(2-4)* 09-11(4-3) 11-16(4-2) 16-18(4-3) 18-20(4) 20-22(3-4) 22-04(2-4) 04-07(2-3)	07-09(4-2) 09-11(3-1) 11-16(2-1) 16-17(3-1) 17-18(3-2) 18-20(4-3) 20-04(4) 04-05(3-4) 05-07(3)	07-17(1-0) 17-18(2-1) 18-20(3-2) 20-05(4) 05-06(3-2) 06-07(3-1)

† Hawaiian Standard Time is 5 hours behind EST; 4 hours behind CST; 3 hours behind MST; 2 hours behind PST and 10 hours behind GMT or Z Time. For example, when it is Noon in Honolulu, it is 17 or 5 P.M. in NYC, EST.

‡ To convert to Local Standard Time in Alaska, subtract 8 hours in the Pacific Standard Time Zone; 9 hours in the Yukon Zone and 10 hours in the Alaskan Standard Time Zone, from the GMT times shown in the Chart. GMT is 5 hours ahead of EST; 6 hours ahead of CST; 7 hours ahead of MST and 8 hours ahead of PST. For example, when it is 18 GMT it is 13 or 1 P.M. EST in NYC.

\* Predominantly Sporadic-E openings.

\*\* Indicates predicted 80 Meter openings. Openings on 160 Meters are also likely to occur during those times when 80 Meters openings are shown with a forecast rating of (2) or higher.

[Continued on page 114]



# Q AND A

BY WILFRED M. SCHERER,\*  
W2AEF

**M**ANY readers have expressed a desire to see more questions and answers published; therefore, since only a given amount of space can be allotted to the Q & A Column for each issue, we'll make this month's introduction a short one to permit room for more of the requested material.

## Full Value From Radio Magazines

Amateurs often comment that they cannot afford this-or-that magazine related to amateur radio, no less subscribing to all those available. Others feel that one or another publication does not contain enough articles in a particular classification or has too many other types not to the reader's liking. While these reasons may have some merit from an economical or interest standpoint, this need not otherwise be necessarily so; provided, every effort is made to get the most value out of each issue.

How can this be done? Simple—read every word from cover-to-cover, including the advertisements. Now hold on—why read a lot of stuff in which you're not interested? Again, the answer is simple—such a procedure will provide you with a storehouse of knowledge for present or future reference, stimulate your thinking, possibly lead you to other interesting areas not previously thought of or to enjoyable reading, provide material to help you to *intelligently* discuss a wide variety of subjects with fellow amateurs, keep you abreast of the latest technical and operating advances as well as amateur activities, learn about new gear, provide the germ for a new idea or two, furnish hints that may enable you to help yourself or others, let you see what the other fellow is doing whether it be construction, design, operating or accomplishments, stir up competitive spirit, provide thoughts on generating good fellowship and promoting amateur radio.

\* Technical Director, CQ.

Even though certain type articles or features are not of particular interest to you at the moment, some day such may be the case and when you need some information on one of the subjects covered in the past, you'll remember having seen something on it around a certain time in such-and-such a magazine, thus enabling you to know about where to go for the data.

Who knows?—you may unwittingly pick up an idea or two that will be worth a whole year's subscription—less than an amount you might spend anyway for an item towards improving your operations. Also, no matter where your amateur-radio interests lie, you may find some facet of value in the other areas that will add more pleasure to the privilege of being a ham.

Yes, even the classified ads can provide interesting reading as to what is going on in the used-gear field, particularly relating to the resale value of equipment. In addition, you may run across an unlooked-for bargain or help out a friend in search for certain gear.

So, no matter which magazines you read, why not at least try the above suggestions for several months. Doing so may possibly be of greater value than even anticipated.

## Decreasing Low A.F. Response With S.S.B. Transmitter

**QUESTION:** I use a Collins KWM-2 Transceiver, a Waters Compreamp and a Collins SM-2 dynamic microphone. My voice is quite low, so I'd like to electronically increase the h.f. response of the equipment. What circuit or component changes will do the job?

**ANSWER:** The best approach to your problem is to reduce the low-frequency response of the equipment with a roll-off below 1000 c.p.s. This is most easily accomplished by reducing the value of one or more interstage-coupling capacitors in the mic-amplifier lineup.

Approximate response curves for various values of  $C$  with a load resistor,  $R$ , of 1 megohm are shown at fig. 1. Which characteristic is suitable will require a little cut-and-try procedure, since the actual response of your voice is not known.

The easiest change will be at the *output* of the Compreamp. Open it up and insert the necessary size capacitor in series with the lead to the output connector. The input impedance of the KWM-2 is about 1 megohm, so the decrease in l.f. response should be close to the characteristics indicated by the related curve for the value of  $C$ .  $C_1$  in the KWM-2 also could be altered.

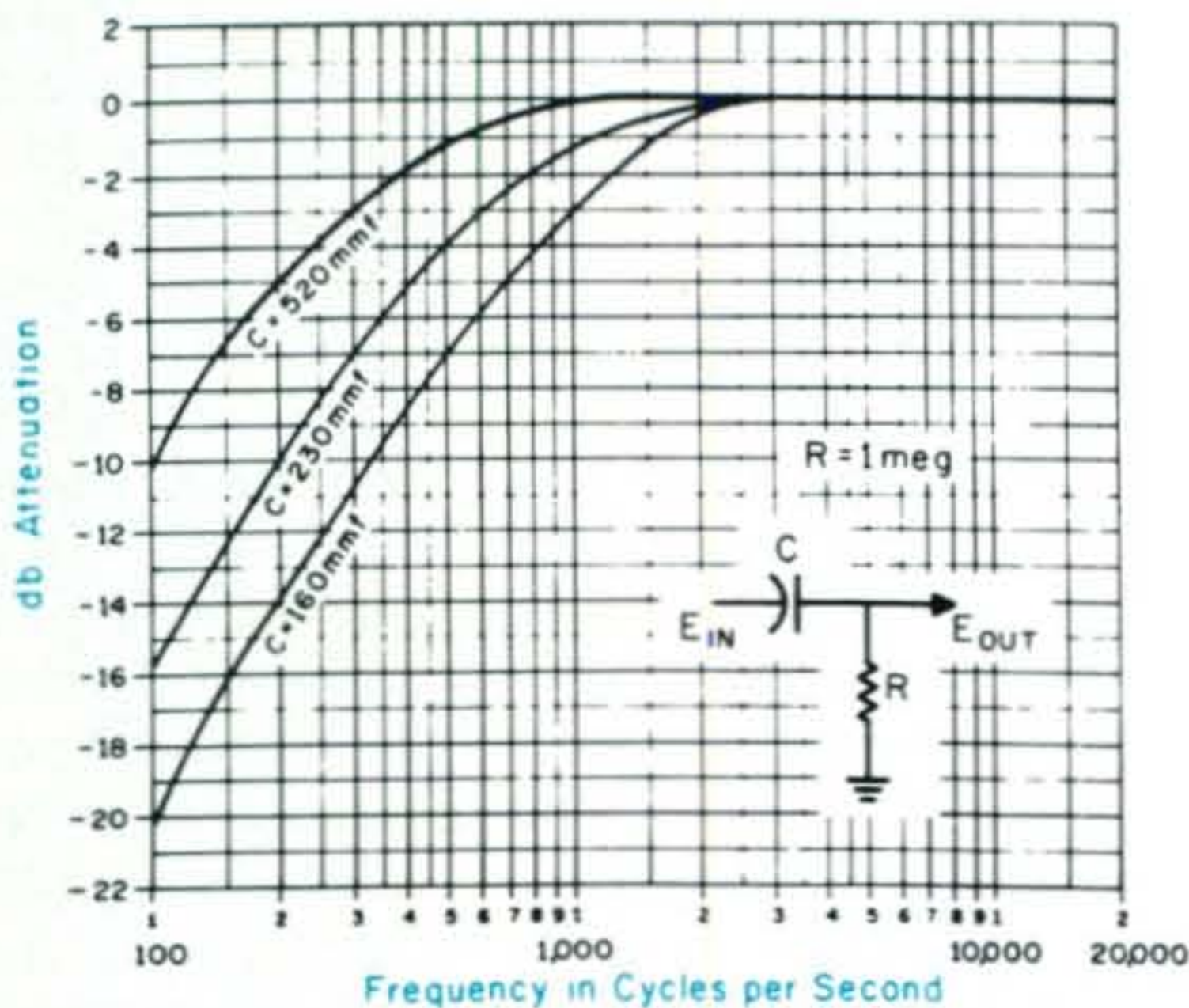


Fig. 1—Low-frequency roll-off response curves with various size a.f. interstage coupling capacitors used with 1 meg. load resistor. Other values of  $R$  and  $C$  may be substituted while maintaining indicated ratio  $R/X_c$ , where  $X_c$  is capacitive reactance @ 100 c.p.s. ( $X_c = \frac{1}{2}\pi fc$ ). A— $C = 520$  mmf,  $R/X_c = 1/3$ . B— $C = 230$  mmf,  $R/X_c = 1/6$ . C— $C = 160$  mmf,  $R/X_c = 1/10$ .

Another change might be at the input to the compreamp where the .01 mf coupling capacitor might be reduced to 500-1000 mmf. This should result in a response near that of curve A. This change will be more difficult to make, since it involves the printed-circuit board.

There are advantages and disadvantages with the changes made at different points. With the capacitor reduced at the *input* of the Compreamp, there will be less clipping of the lows (in comparison to the highs) with a given mic level and less in-band distortion; however, the output (with all frequencies clipped) may still be fairly flat.

With a small coupling capacitor at the *output* of the Compreamp, the desired roll-off will be fully maintained, but any in-band distortion due to clipping of the lower frequencies in the unit, may be accentuated. The best bet might be a compromise with a moderate roll-off at both points.

Another expedient, but more costly, would be to change the mic to an Astatic D-104. This is a crystal job which has a sharp rising characteristic that peaks near 2000 c.p.s. For this reason these mics were used considerably with a.m. transmitters where the highs usually are attenuated due to the sharp selectivity characteristics and sideband clipping of the i.f. system in the conventional communications receiver.

## Swiss Quad

Queries are occasionally received concerning the Swiss Quad. For those who in the future may desire information related thereto, we suggest reference be made to the *RSGB Bulletin* for June 1964 (published by the Radio Society of Great Britain), where the design and construction of this antenna was originally described.

## Heat Sink for Power Resistors

Here is a suggestion submitted by Richard Mollentine, WAØKKC, 19 Edgemere Court, Olathe, Kansas 66061:

Heat sinks for wire-wound vitreous-enamel or ceramic-insulated power resistors may be made using adjustable sliders as shown at fig. 2. The internal-contact "bump" should be removed, so the slider makes a good contact all around the insulation. A copper or aluminum sheet or bar, attached to the sliders, serves as the heat-dissipating element. Additional "sinking" may be obtained by fastening the bar to the chassis using silicon heat-sink compound. Thanks, Dick.

## Heathkit HO-10 Monitorscope for 50 Kc

QUESTION: How should the Heath HO-10 Monitorscope be used with the Hallicrafter SX-117 receiver which has a last i.f. of 50.75 kc?

ANSWER: Since the vertical amplifier in the Heath HO-10 Monitorscope is designed for frequencies below 500 kc. it may be used directly with the 50.75 kc of the SX-117.

To do so, connect the Vertical input of the scope with a shielded lead through a 22 mmf capacitor to pin 3 of  $V_{10B}$ . This may be picked up at the tie point to which  $C_{83}$  also is connected. If more gain is needed, increase the scope-coupling capacitor to 50 or 100 mmf.

In order to obtain the most faithful repro-  
[Continued on page 110]

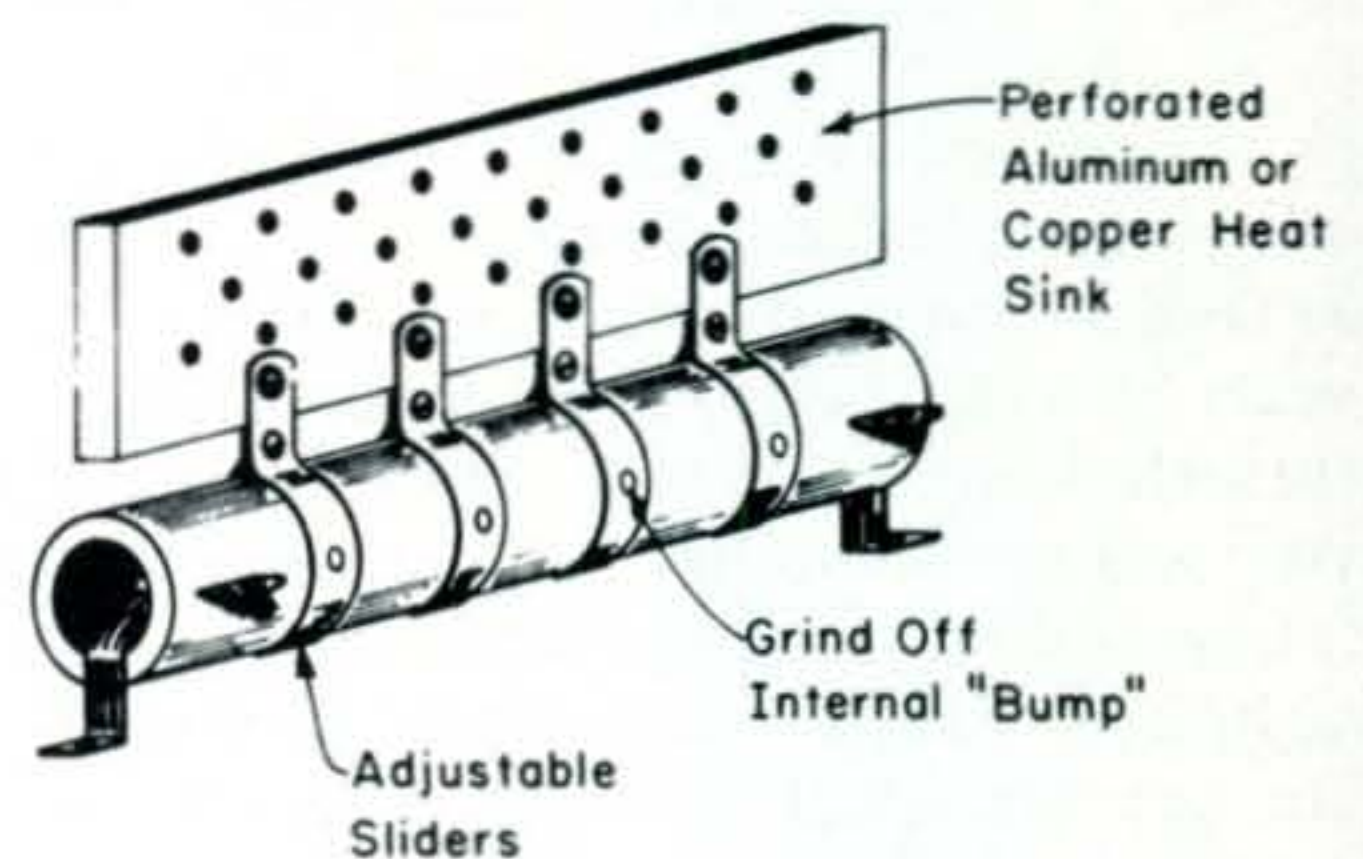


Fig. 2—Method of heat sinking large wire-wound power resistors using slider taps normally used with adjustable resistors.



# Contest Calendar

BY FRANK ANZALONE,\* W1WY

## Calendar of Events

July	3-5	KA Field Day
July	6-7	Venezuela Contest
July	20-21	Colombia Contest
July	27-28	County Hunters C.W. Party
August	3-4	Romania Contest
August	3-4	Maryland & D.C. QSO Party
August	10-11	DARC WAE C.W. Contest
August	10-11	LAMBRE C.W. Contest
August	24-25	QRP QSO Party
August	24-25	All Asian DX Contest
Aug. 31 - Sept. 1		LAMBRE Phone Contest
September	7-8	VU/4S7 C.W. Contest
September	14-15	VU/4S7 Phone Contest
September	14-15	DARC WAE Phone Contest
September	14-15	SAC C.W. Contest
September	21-22	SAC Phone Contest
October	5-6	C.A.R.T.G. (RTTY) Contest
October	5-6	WADM C.W. Contest
October	5-6	VK/ZL/Oceania Phone
October	12-13	VK/ZL/Oceania C.W.
October	12-13	RSGB 28 mc Phone Contest
October	16-17	YLRL Anniv. C.W. Party
October	19-20	Boy Scout Jamboree
October	26-27	<b>CQ WW DX Phone Contest</b>
October	26-27	RSGB 7 mc C.W. Contest
November	2-3	Okinawa (KR6) Contest
November	6-7	YLRL Anniv. Phone Party
November	9-10	OK C.W. DX Contest
November	9-10	RSGB 7 mc Phone Contest
November	9-11	ARRL SS Phone Contest
November	16-18	ARRL SS C.W. Contest
November	23-24	<b>CQ WW DX C.W. Contest</b>

## KA Field Day

Starts: 0900 GMT Wednesday, July 3

Ends: 0900 GMT Friday, July 5

Check last month's CALENDAR and W2GT's Column for details.

Your QSL's go to: Far East Auxiliary Radio League, Box C-89, APO San Francisco 96525

## Venezuela Contest

Starts: 0000 GMT Saturday, July 6

Ends: 2400 GMT Sunday, July 7

Complete details in last month's CALENDAR  
Mailing deadline Sept. 15th to: Radio Club Venezolano, Independence Contest, P.O. Box 2285, Caracas, Venezuela.

\* 14 Sherwood Road, Stamford, Conn. 06905.

## Colombia Contest

Starts: 0000 GMT Saturday, July 20

Ends: 2400 GMT Sunday, July 21

This one also covered in last month's CALENDAR.

Logs must be in hands of the committee before September 30th. They go to: The L.C.R.A. Colombia Independence Contest, Box 584, Bogota, Colombia.

## County Hunters C.W. Party

Starts: 0000 GMT Saturday, July 27

Ends: 2400 GMT Sunday, July 28

This year's party is sponsored by the South Shore A.W.A. A station may be worked once per band and may be contacted again if he moves to a different county. DX stations may be worked for QSO credit but do not count as a multiplier.

**Exchange:** RST report plus a progressive 3 digit QSO number starting with 001, county and state.

**Scoring:** Number of QSOs multiplied by number of different counties worked.

**Frequencies:** 3575, 7055, 14070, 21070.

**Awards:** Certificates to the top scorers in each state and each country, as well as the top three scorers world-wide.

**Logs:** Date/time in GMT, station worked, exchange sent/received, band and indicate each new multiplier as it is worked. Include a summary sheet with total claimed score, name and address in BLOCK LETTERS and other pertinent information. Also include a s.a.s.e. for copy of results.

Mailing deadline is Aug. 31st and logs go to: South Shore Amateur Wireless Assoc., 32 Elmwood Street, Valley Stream, N.Y. 11581

## Maryland/District of Columbia QSO Party

Starts: 2200 GMT Saturday, August 3

Ends: 2200 GMT Sunday, August 4

This is the third MD/DC QSO Party sponsored by the Maydale A.R.C. A station may be contacted once on each band and mode.



SARL Contest Committee secretary, Aila, OH2BIN, smiling after the job of checking almost 1000 SAC contest logs has been completed. Contest Chairman, OH2XK, said the stack of logs weighed 70 lbs. Wonder what Aila's expression would have been if she had to go through 250 lbs. of paper, almost 3000 logs (our total last year)?

Separate logs are requested for each mode and each band.

**Exchange:** QSO Nr., RS/RST, QTH. Counties for MD/DC stations, ARRL section or country for others. (Baltimore and Wash. D.C. count as separate counties.)

**Scoring:** Two points for each completed QSO. MD/DC multiply total QSOs by ARRL sections and countries worked. All others use Maryland counties as their multiplier. (Max. of 25)

**Frequencies:** 3575, 3850, 7075, 7275, 14075, 14275, 21075, 21325. Also 50.2 and 145.2. Novices: 3735, 7175, 21110.

**Awards:** Certificates to top scorers in each ARRL section and country. (Total from all bands and modes.) Second and third place awards will be made in sections where participation high.

**Logs:** Should show date/time in GMT, station worked, RS/RST sent and received, and QTH. A summary sheet with the scoring, name and address in BLOCK LETTERS and a signed declaration that all rules and regulations have been observed.

Logs go to: Carl E. Andersen, K3JYZ, 14601 Claude Lane, Silver Spring, Maryland 20904. Mailing deadline Sept. 1st. Include s.a.s.e. if a copy of results are desired.

### DARC WAE Contest

C.W.—August 10-11. Phone—Sept. 14-15

Starts: 0000 GMT Saturday. Ends: 2400 GMT Sunday in each instance.

This is the 14th "Worked All Europe" DX Contest sponsored by the DARC. Some minor modifications have been made to the rules of previous years, the most notable being the addition of a rest period.

All bands, 3.5 thru 28 mc, may be used, the same station may be worked once on each band for QSO and multiplier credits.

**Classifications:** Single operator and Multi-operator, both single and multi transmitter.

**Rest Period:** Only 36 hours out of the 48 hour contest period allowed for single operator stations. The 12 hours of non operation may be taken in one or two periods any time during the contest. The periods need not be equal but must total at least 12 hours and clearly shown on the log.

**Exchange:** The usual five or six digit serial numbers, RS/RST plus a progressive QSO number starting with 001. (Multi transmitter stations should use separate series of numbers for each band)

**Points:** Each QSO counts 1 point, except on 3.5 mc where it counts 2 points.

**Multiplier:** The multiplier for non-Europeans is determined by the number of European countries worked on each band. (See WAE list)

Europeans use the ARRL country list for their multiplier. In addition each call area in JA, PY, VE/VO, VK, W/K, ZL, ZS, UA9 & UA0 all are multipliers.

**Scoring:** Final score, total QSO joints plus QTC points multiplied by sum of countries from each band.

**QTC-Traffic:** Additional points may be realized by use of the QTC feature. A QTC is a report of a confirmed QSO that has taken place earlier and later sent back to a European station. It can only be sent from a non-European to a European. The general idea being that after a number of European stations have been worked, a list of these stations can be reported back during a QSO with another station. An additional 1 points credit can be claimed for each station reported.

a. A QTC contains the time, call and QSO number of the station being reported. ie: 1300/DJ3KR/134. This means that at 1300 GMT you worked DJ3KR and received number 134.

b. A QSO can be reported only once and not back to the originating station.

c. A maximum of 10 QTCs to a station per band is permitted. The same station may be worked several times to complete this quota. Only the original contact however has QSO point value.

d. Keep a uniform list of QTCs sent. QTC 3/7 indicates that this is the 3rd series of QTCs sent and that 7 QSOs are being reported.

**Awards:** There will be three power divisions for award purposes: (a) up to 200 watts input, (b) more than 200 watts, (c) newcomers licensed less than one year.

Certificates to the highest scorers in each classification in each country and country/district listed. 2nd and 3rd place awards will be given in areas of sufficient participation, and continental leaders will also be honored.

There are Trophies for both Europe and non-Europeans that are the leaders in each of the three operating categories.

A minimum of at least 4 hours of operating is required to be eligible for an award.

**WAE Endorsements:** Contest contacts can be used for WAE certificate endorsements providing the log of the requested station is also received.

**Disqualification:** Violation of the rules of the contest, or unsportsmanship conduct, or taking credit for excessive duplicate contacts will be deemed sufficient cause for disqualification.

**Logs:** It is suggested you use the log sheets of the DARC or equivalent, 40 QSOs or QTCs per sheet. Use a separate sheet for each band, and a summary sheet showing the scoring and your name and address in BLOCK LETTERS. Include a s.a.e. and IRCs with your request for official log forms.

Mailing deadline is Sept. 15th for C.W. and Oct. 15th for phone. Mail logs and requests to: Walter Skudlarek, DJ6QT, An der Klostermauer 3, D-6471, Hirzenhain, West Germany.

### WAE Country List

CT1, CT2, DL/DJ/DK/DM, EA, EA6, EI, F, FC, G, GC, GD, GI, GM, GM Shetland Is., GW, HA, HB, 4U1ITU, HB0, HV, I, IS, IT, LA, LA Bear Is., JX, JW, LX, LZ, M1/9A, OE, OH, OH0, OK, ON, OY, OZ, PA/PI, PX, SM/SL, SP, SV, SV Crete, SV Rhodes, TA Europe, TF, UA/UV/UW 1-6, UB/UT/UY, UC, UN, UO, UP, UQ, UR, UA Franz Josef Land, YO, YU, ZA, ZB2, 3A, 9H.

### QRP QSO Party

Starts: 0200 GMT Saturday, August 24

Ends: 2300 GMT Sunday, August 25

The QRP A.R.C. International, with over 3000 members, announces its 7th annual QSO Party.

Members may work anyone, non-members work members only. The same station can be worked on different bands and modes for QSO points.

**Exchange:** QSO nr., RS/RST, ARRL section or country, QRP nr. (NM for non-members)

**Scoring:** One point per contact, DX 3 points. Total QSOs multiplied by ARRL sections and countries worked. There is an additional power multiplier as follows: 21-30 watts, 1.2; 11-20 watts, 1.6; 1-10 watts, 2; less than 1 watt, 3.

**Frequencies:** c.w. — 3540, 7040, 14065, 21040, 28040. Phone: 3855, 7260, 14260, 21300, 28540.

**Awards:** Certificates to the two highest scoring stations in each ARRL section and country. A special certificate to the top station in each W/K and VE call area working the most member countries. (Min. of five countries)

Logs to go: Jim Loring Jr. WA1BEB, RFD 2, Bethel, Maine 04217. Information on membership in the QRP ARC may be obtained from K7LNS.

### Editor's Notes

The rules of the Romania and the All Asian contests should have been included in this month's CALENDAR. Neither one has been received at this writing. Also no word from the MARC VE/W contest usually held the

### 1967 SAC Results

C.W.		Phone	
WA1FHU	728	K8HZU	1834
W1AYK	240	WA8QIY	296
W1BGD/2	5040	W8DWP	44
W2MEL	4750	WA8WTT	2
WA2QHK	876	W9LKI	1540
W2NRV	510	W9HDR	740
WB2UDF	350	W9AEM	264
W2ZV	336	W9QWM	182
W2LWI	318	W9TCU	24
W2KGN	210	WA0EMS	2205
WA2OIL	54	W0BMM	1936
W3BYX	2025	WA0KDI	1800
K3NUM	1695	K0DYM	185
W3CBF	264	W0LMO	115
W3QOR	44		
W4ZXI	2288	WA2CCF	21
K4BAI	1946	W3BYX	2227
W4HOS	1176	W3CBF	32
K4ELK	21	W4HOS	350
W5KC	1620	WA5ALB	189
W5JAW	1287	WA7EVO	128
4X4UJ/K5	100	K8HZU	342
W6TZD	1404	W8DWP	253
K0GJD/6	1248	W8IBX	8
WB6KBK	272	K9ECE	1312
WA6JVD	195	W9KXK	550
WA6JDT	60	WA9UGI	330
WB6RTJ	2	WA0EMS	671
		W0LBB	533

last week-end of September. No information will be published unless an official announcement has been received. Past experience has proved that this policy must be maintained. And I must have it at least three months before the month of the activity.

73 for now, Frank, W1WY

TELL THEM YOU SAW IT IN CQ



# THE awards PROGRAM



BY ED HOPPER,\* W2GT

**T**HE July, "Story of The Month" is about John Knaak, W5OYG.

### John Knaak, W5OYG

JOHN was born October 13, 1938 in Winchester, Illinois. Shortly thereafter the family moved to Hillsboro, Kansas, where he was raised and went to school.

He is the oldest of three brothers, but the only ham in the family. A ham ticket was received in April of 1956 while he was a senior in high school, and his first call was KØEQY.

Two important events took place in July of 1960, John graduated from Kansas State Teachers College at Emporia, Kansas with a Bachelor of Science Degree in Business and one week later married "Wendy!"

For the next 6 years, the family moved seven times, moving to W5 land where John became W5OYG. In the meantime, Cheryl Ann arrived in 1962 and John Jr. in 1967. (Yes, that is John Jr. helping Dad hunt new counties).

John always had a casual interest in County Hunting, exchanging QSLs with Rag Chewing contacts, but not operating any County

Hunting Nets. In October 1965, the discovery of the then newly formed 75 meter County Hunter Net started John on the road to County Hunting with great determination.

By 1966, all states had been worked and confirmed on 75 sideband. In April 1966, USA-CA-500 Award #563, endorsed All 75 meters and All sideband, was received. In February 1967, USA-CA-1000 Award #110, also endorsed All 75 meters, All sideband, was earned. USA-CA-1500 Award #58, endorsed All sideband was received in March 1967. Then USA-CA-2000 Award #38, also endorsed All sideband, came in September 1967, and finally USA-CA-2500 Award #26 dated April 2, 1968, also endorsed All sideband, was received. As this is being written, John had confirmed 2573 counties on all bands and 1449 on 75 meters.

The present equipment includes a Galaxy V MK2 transceiver, 14AVQ Vertical and an assortment of dipoles.

John's occupation is Manager of a Variety Store for T. G. & Y. Stores Company in Duncan, Oklahoma. His other hobbies are fishing and golf—when time permits. He has met many of the County Hunters personally and he agrees that a finer bunch of hams

\* 103 Whittman St., Rochelle Park, N.J. 07662.



John, W5OYG and John, Jr.

### 2nd Annual CW County Hunter's QSO Party

Starts: 0000 GMT Saturday, July 27

Ends: 2400 GMT Sunday, July 28

Sponsor

South Shore Amateur Wireless Association

116 Locust Street,

Valley Stream, N. Y. 11581

Frequencies: 3575, 7055, 14070, 21070.

See CONTEST CALENDAR

for full details.

can not be found anywhere. John would like to publicly state that he *will* beat his good friend and County Hunting rival, Dave, W5PWG to 3000 counties.

### Letters

**Hank, WB2RMM**, writes: "Thought this would be of interest to your readers. Have had several fine QSOs with WN7IRD, Wilberta "Willie" Longwell (XYL) of Baker, Oregon. Since she received her Novice Ticket in October, 1967, she has: Had 1,004 QSOs up to March 29; received her WAS certificate; worked all continents; worked 30 different countries; confirmed 20 countries; received her 15 w.p.m. sticker in code proficiency; 259 confirmed counties and is now a confirmed county hunter. Most of her QSOs last 1/2 hour and her record QSO was 2 1/2 hours, her 1,004 QSOs do not include any contest or contest style QSOs."

**Eddie, K4LSP**, writes: "Please print in your column, where one may purchase the *USA-CA Record Books*. I have over 2,000 counties and would like to apply for your USA-CA Award.

Presently I have given out to the County Hunters over 2,400 counties in 40 different states, including the provinces of Canada. I travel for a living, therefore I am on the Net most every day from some different county in the south." (*USA-CA Record Books may be obtained direct from CQ, 14 Vanderventer Ave., Port Washington, L.I., N.Y. 11050 for \$1.25. Eddie, I'm waiting for your application, Hi.*)

**Don, W8IIT**, writes: "This will acknowledge receipt of USA-CA-500 Award. I really am proud of this certificate and am anxious to get it framed as soon as possible. Thank you for your prompt attention in this matter.

I'd like to see more County Hunter activity on fone and CW on 7 MC. Thanks again for a super certificate—now the big push for USA-CA-1000."

### Awards

**The Kickapoo Council Award:** This award is sponsored by the Vermilion County Amateur Radio Association of Danville, Illinois. The award is offered free for working five club members, and no confirmation is necessary, just send CGR list to the custodian, Mr. Francis Kirk, K9JLP, 911 N. Washington St., Danville, Illinois 61832. There is a hardy group of members who meet regularly on 3925 each Wednesday evening at 0330 GMT.



Kickapoo Council Award

**Vancouver Sea Festival Amateur Radio Award:** The 6th Annual Vancouver Sea Festival will be held July 13th to July 22nd and as the Greater Vancouver Amateur Radio Operators participate in this festival, this award is being offered in their honor. Rules are: 1. All legal Amateur Radio Operators in the world may receive this award except— (a) Countries on the Department of Transport banned country list. (b) Greater Vancouver Amateur Stations located in Vancouver City, New Westminster, Burnaby, North and West Vancouver, Surrey, Coquitlam, Richmond and Port Moody. 2. Stations in 1 (b) may qualify provided all contacts are made from a portable or mobile location not defined as Greater Vancouver. 3. The certificate is awarded on submission of the following information: (a) Date and time of contact. (b) Call sign of station worked. (c) QTH of stations worked. (d) No QSL required. 4. Ten different stations must be worked in the Greater Vancouver Area as defined in 1. (b) 5. Any legal mode of Amateur Radio Contact and any amateur Band may be used but only one contact per station. 6. There is no charge for certificate or mailing. 7. Only contacts made after Feb. 1st, 1968 will be counted. 8. Applications for this award should be sent to: Mr. Jack R. Rothwell, VE7TK, 6758 Bryant Street, Burnaby 1, Vancouver, B.C., Canada.



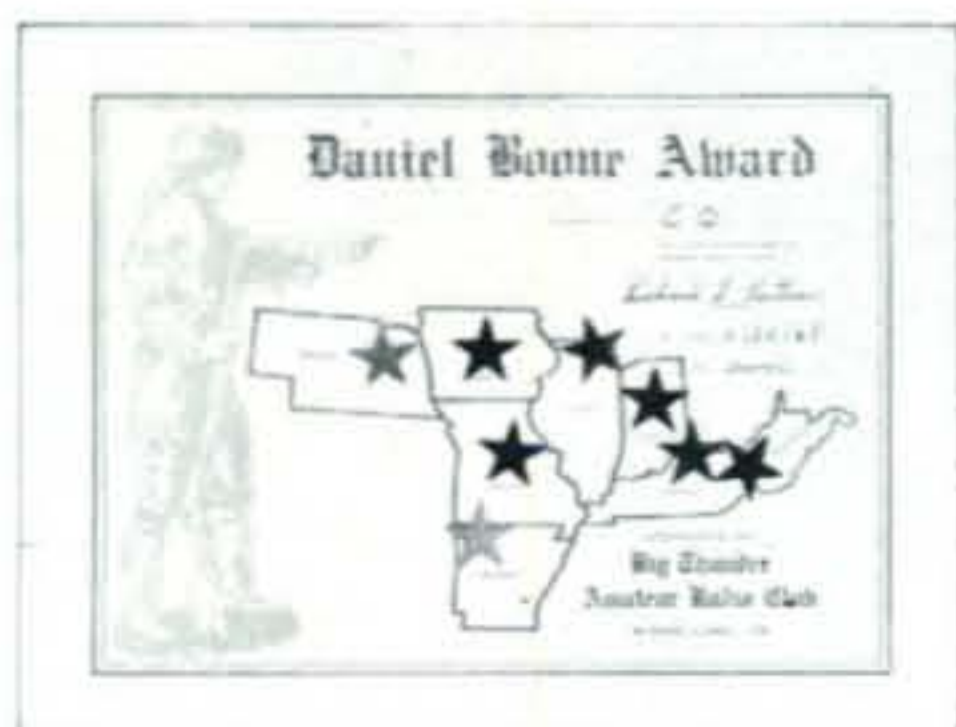
Vancouver Sea Festival Amateur Radio Award



Dixie 6 Meter Sideband Net Award

**Dixie 6 Meter Sideband Net Certificate:** This beautiful certificate is being issued to publicize the following Nets. The Dixie 6 Meter Sideband Net meets on a regular basis at 2100 EST on Wednesday and Sunday nights. Their affiliate net, the Atlanta Early-Bird Net meets every Sunday morning at 0830 EST. All Net activity is conducted on a frequency of 50.110 mc s.s.b. They also monitor 145.350 for cross band check-ins. There are as many as 30 members who check in on a regular basis. These stations are from the surrounding states including Tennessee, Alabama, North and South Carolina. The net originates from the greater metropolitan Atlanta area, so you can see this is quite a haul for 6 meter ground wave. To qualify for this award, a local station, (*i.e.*, a station in any of the aforementioned states) must answer in to any one of the three nets, three times within a 45 day period or answer in to all three nets once within a 45 days period. For DX or skip stations, the requirement is to work each net control station once on 6 meter sideband with no time stipulation. WA4JCI is NCS for the Sunday 0800 Net; W4BTW is NCS for the Sunday 2100 Net; and K4RZB is NCS for the Wednesday 2100 Net. There is no charge for the certificate or postage. Apply to Jim Broaddus, K4RZB, 408 Campbell Hill St., Marietta, Georgia 30060.

**The Daniel Boone Award:** Sponsored by the Big Thunder Amateur Radio Club of Belvi-



Daniel Boone Award

dere, Illinois. Issued for stations having had contact with a minimum of 4 Boone Counties, with seals being issued for each county after the basic 4. There are 8 Boone counties in the following states: Arkansas, Illinois, Indiana, Iowa, Kentucky, Missouri, Nebraska, and West Virginia. Charge for certificate is \$1.00, and seals for additional counties for sending QSL and S.A.S.E. No A.O.M.B. endorsements. Free to blind and handicapped. Swls can also qualify. Custodian: Dick Butram, K9LFA, Rt. 3, Box 306, Belvidere, Illinois 61008.

**Chief Big Thunder Award:** Also sponsored by the Big Thunder ARC of Belvidere, Illinois. Available to stations having confirmed contact with 3 Big Thunder ARC members after January 1, 1968. Applications have been received from 141 stations from nearly every state in the union. 4 member stations work the 75 meter county hunter nets nearly every night. Cost of award is 50¢, but free to blind and handicapped and S.w.l.s can also qualify. Information and club membership will be sent upon request, S.A.S.E. will be appreciated. Custodian: Dick Butram, K9LFA, Rt. 3, Box 306, Belvidere, Illinois 61008.

**Wonderful Wisconsin Week Award:** This certificate, sponsored by the Greater Wisconsin Foundation and signed by the Governor will be issued to help publicize the Wonderful Wisconsin Week, this year September 17-23, 1968. To qualify for the award those operators in the State of Wisconsin must make contact with at least 10 out of state amateur radio operators. Out of state operators (including all of Canada) must make contact with at least 5 Wisconsin amateur radio stations. Out of the county operators (including Alaska and Hawaii) must make contact with at least 2 Wisconsin amateur radio stations. The log information of the qualifying contacts with the names and addresses should be sent with the operations blank QSL.

[Continued on page 98]



Chief Big Thunder Award



# Why the Reginair 321 Quad is Important to You!

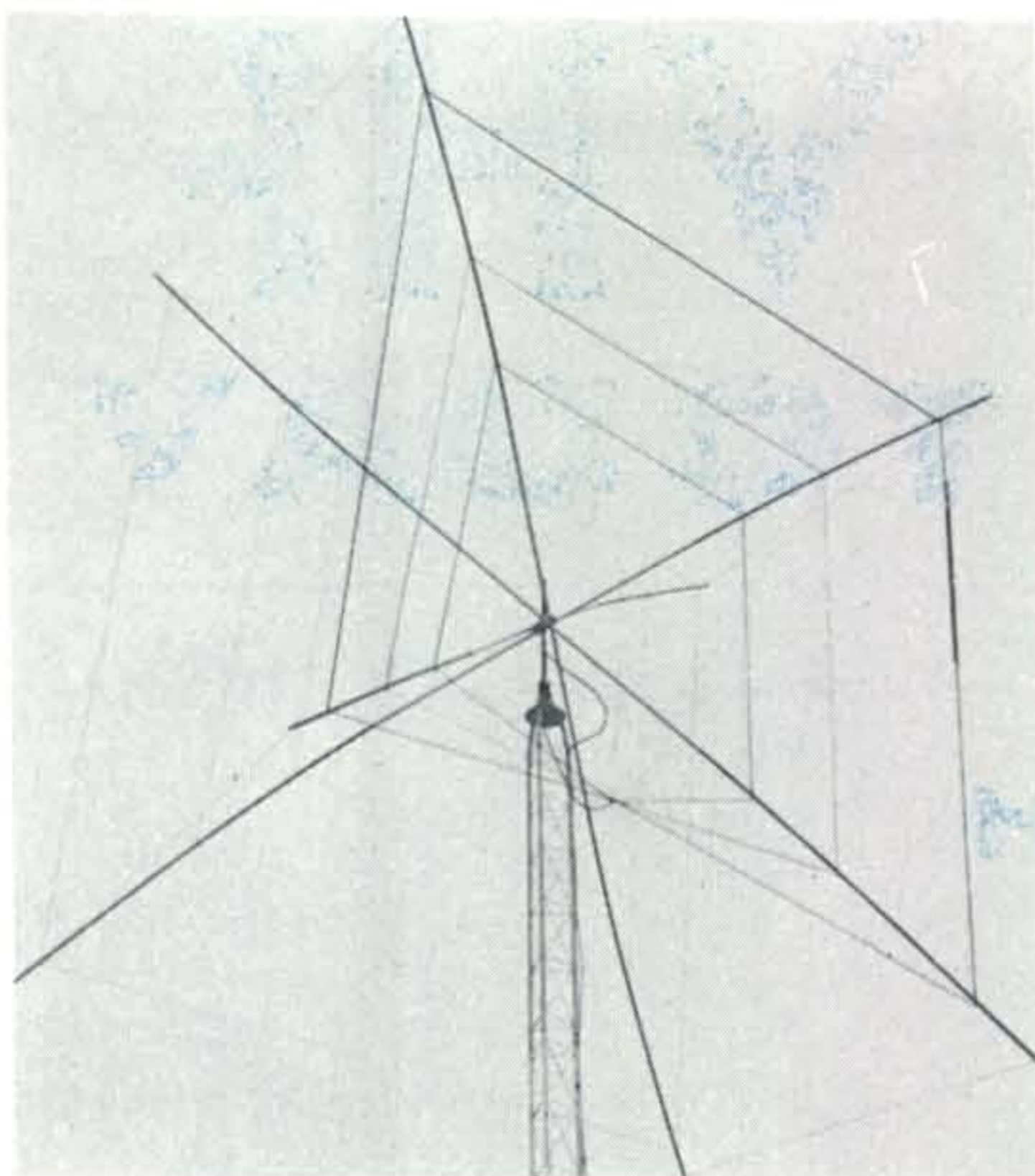
Present day transceiver and transmitter designs require an antenna match with as flat a resonant response as possible. In the olden days a typical 500 watt rig required a relay rack and 500 pounds of gear. The physical spacing and voltage parameter of the tank circuits were such that one never worried about VSWR; indeed, that term had not yet been coined! Flash over and mismatch were laughed at and tolerated.

What a difference today! In a table top box scarcely 1½ cubic feet and weighing less than 50 pounds we find a modern sideband transmitter and receiver thrown in as well. Take a good look at the components: fixed capacitors smaller than ½ postage stamp; a loading capacitor with .005 inch spacing; and transmitting tubes that are in reality TV horizontal outputs. These, then, are what you find. Do you wonder then why the manufacturer tells us we must operate into loads of 2.5 to 1 or better? Do you wonder then why the factory says to tune up in less than 30 seconds? Is it a surprise to you to find that new finals are required so quickly? Good engineering tells us that at 2.5 to 1 we have 20% of our forward power coming back to stay as circulating current and heat.

The danger comes into the picture because the average ham can't or won't confine his operation over that narrow spectrum where his antenna is in resonance and where his VSWR is less than 2.5 to 1.

Sure—new SSB designs are in the works: transceivers whose receivers will have variable selectivity; whose transmitters will use better tubes; rigs that can take more guff. But can you wait that long or afford that much money?

There is an alternative now—in fact, two choices. You can either be more mindful of the frequency tolerances of your setup, or better still, you can obtain one of our *Reginair Quads*. This is the only commercially available product that gives three band operation with one 52 ohm feed line and absolutely guaranteed low, low VSWR over the entire 10, 15, and 20 meter bands.



Our new quad is constructed of 2 different dimensioned poly vinyl chloride (PVC) tubes made into a 10 foot arm with an aluminum coupler. The PVC is especially selected for temperature and mechanical stability. Hardwood stiffeners additionally are inserted within the PVC. The hub of the quad is a virtually indestructible acrylonitrile butadiene styrene (ABC) which can withstand salt water, and the atmosphere for years and years.

The quad is furnished complete with easy to understand assembly instructions, at only \$89.95 FOB Harvard, Mass. Study the box score and see if this antenna isn't the answer to your operating and maintenance problems. You might even find that DXing can be fun now that you are hearing the rare one.

Forward gain over dipole . . . . .	5.9 db
Forward gain over isotropic dipole . . . . .	8.0 db
Front to back ration . . . . .	.25 db
VSWR over 28-29.7 MHz; not more than . . . . .	1.5:1
VSWR over 21-21.45 MHz; not more than . . . . .	1.5:1
VSWR over 14-14.35 MHz; not more than . . . . .	1.5:1
Maximum RF input . . . . .	2 kw
Maximum mast dimension . . . . .	1¾" dia.
Wind resistance . . . . .	.45 sq. ft.
Feed line . . . . .	52 ohms
Outside dimensions . . . . .	18'x18'x12'
Turning radius . . . . .	.9½'
Net weight . . . . .	35 pounds
Shipping weight . . . . .	40 pounds
Designed for 100 mph winds; ½ inch radial ice	
Frontal lobe . . . . .	.75°
Standard model price (FOB Harvard) . . . . .	\$89.95

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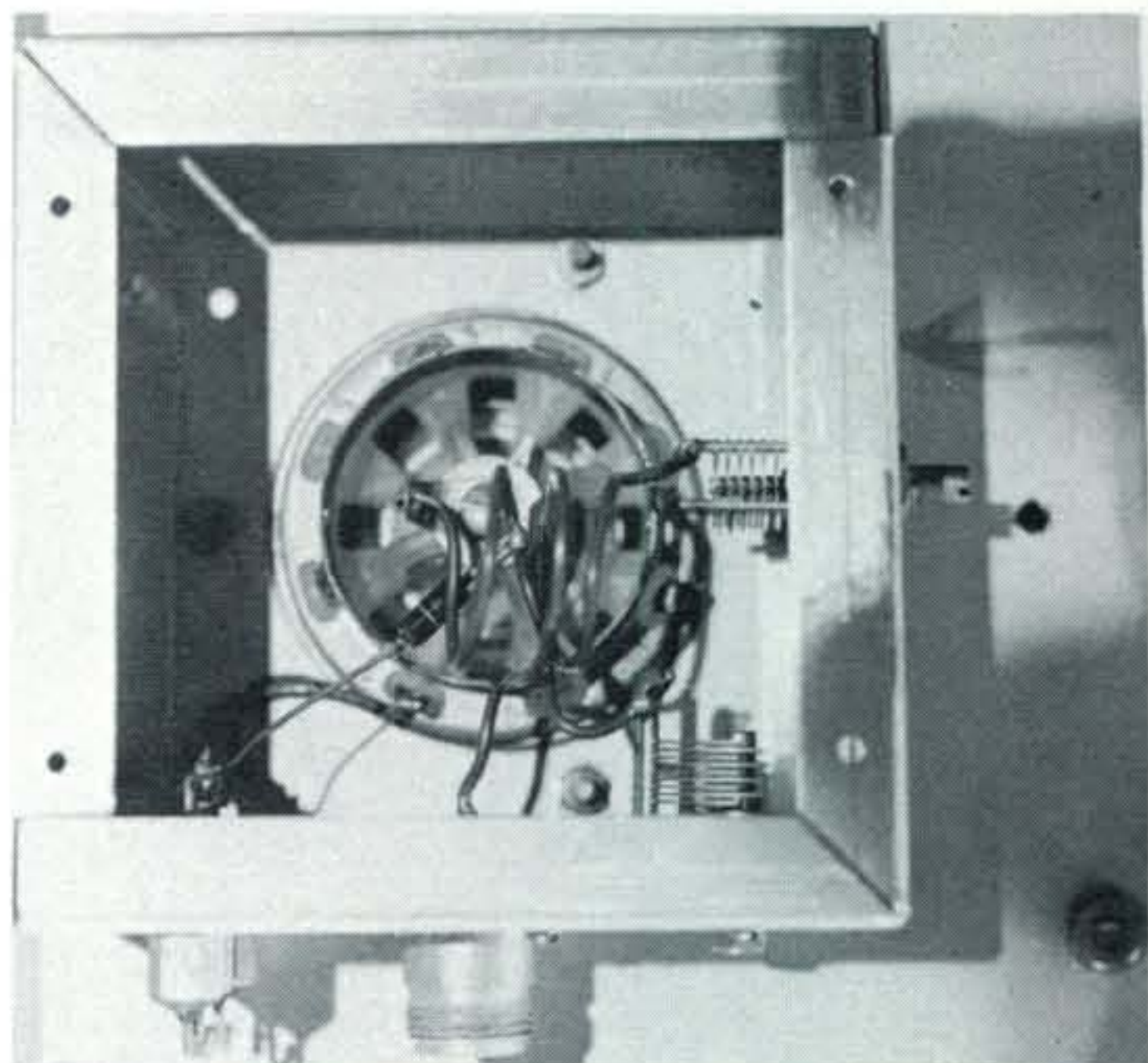
# VHF TODAY

BY ALLEN KATZ,\* K2UYH

**H**ow to get the most power out of an r.f. amplifier is an age old amateur puzzle. In general it is true that the more power into a given tube the more power out of that tube.  $R.f. \text{ Power Out} = DC \text{ Power In} - \text{Power Dissipated in Heat}$ .  $\text{Efficiency} = \text{Power In} / \text{Power Out}$ . You can usually do no better than 70% efficiency and on the v.h.f. bands you will in most cases do much worse. Thus to run 1000 watts input requires a tube with more than 300 watts of plate dissipation . . . a realistic figure is around 500 watts of plate dissipation. This is the reason at least two 4CX250's (250 watts plate dissipation each) are used in 1 kw v.h.f. amplifiers.

Suppose you have only a single 4CX250 and want to run the legal input, is there anything you can do? Back in the late 20's and 30's some amateurs ran glass bulb tubes inverted in jars of oil. The limiting condition for these tubes was envelope temperature. When plate dissipation went above a certain level, the glass envelope would become so hot that it would melt. Immersing the tube in oil allowed some of the heat at the glass envelope

\* 48 Cumberland Ave., Verona, New Jersey 07462.



Interior view of the input section showing grid connections. (photo courtesy of Mark Nadir)

to be conducted away, lowering the temperature and thereby raising the plate dissipation.

The external anode tubes of today work in a similar fashion. Most of the heat developed at the plate is carried away by forcing a continuous stream of air through the external anode. The more air moved through the anode, the more heat removed. The manufacturer's specifications set a minimum rate of air flow for which the plate dissipation rating holds. The 4CX250 requires 6.4 cubic feet per min. Some amateurs have shown that by forcing air at a rate in excess of the specifications that they are able to run these tubes at higher than rated dissipation. There are problems to this approach. The blower by necessity must be large and almost always creates a high noise level. Owners of such super-forced air cooled finals are usually forced to wear head phones.

A somewhat quieter approach is that of water cooling. Here water rather than air is passed through the anode. Because water ab-

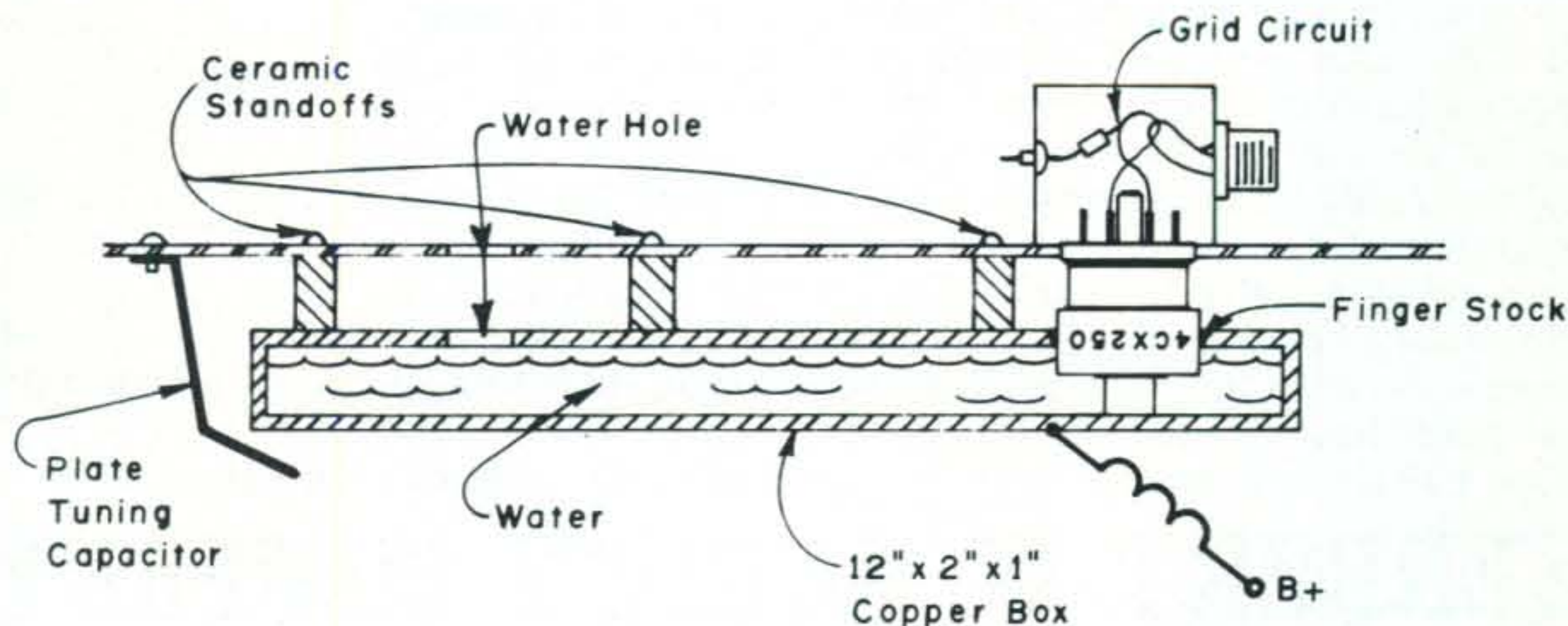


Fig. 1—Physical layout and construction details for the vapor phase amplifier operating on 220 mc.

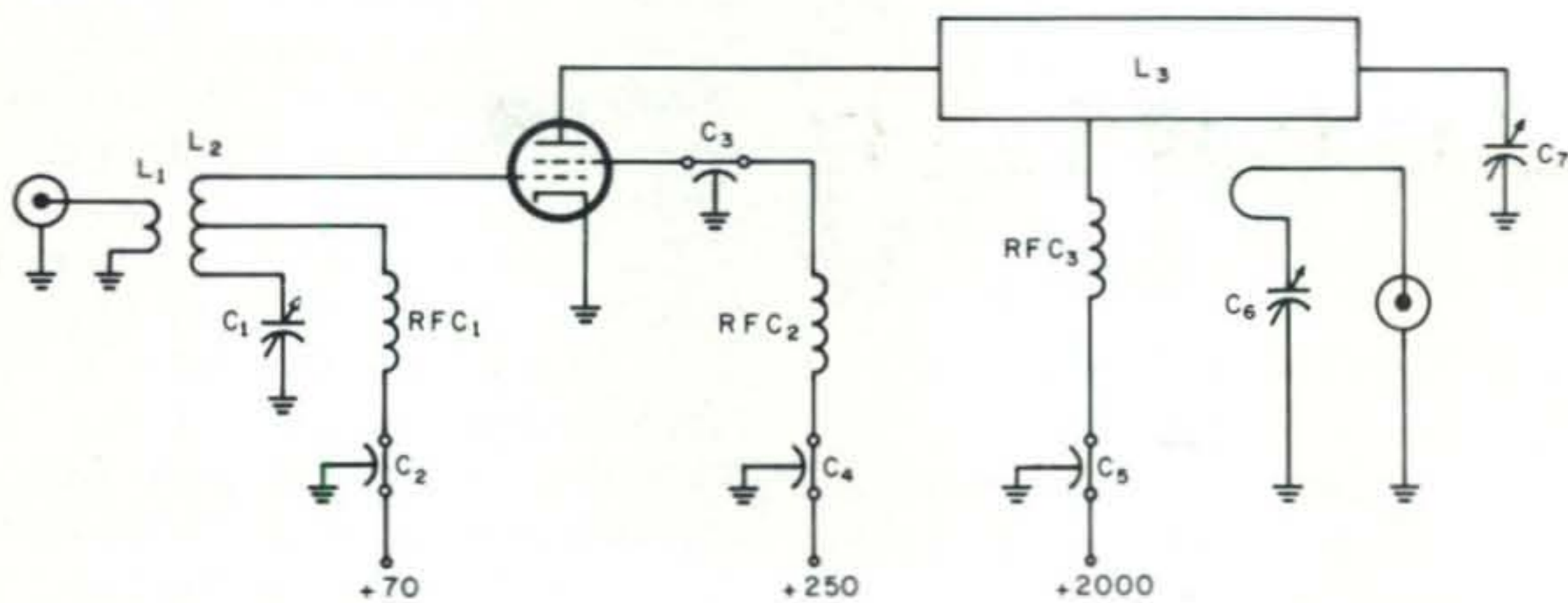


Fig. 2—The circuit diagram for the 220 mc vapor phase amplifier shown in the photographs.

C<sub>1</sub>—15 mmf variable.

C<sub>2, 4, 5</sub>—1000 mmf feed-thru.

C<sub>3</sub>—Built in screen by-pass.

C<sub>6</sub>—20 mmf variable.

C<sub>7</sub>—Plate tuning capacitor. See Fig. 1.

L<sub>1</sub>—1 t. 3/4" dia. loop.

L<sub>2</sub>—4 t. 3/4" dia.

L<sub>3</sub>—Copper box, see text and Fig. 1.

RFC<sub>1, 2, 3</sub>—Ohmite Z-220.

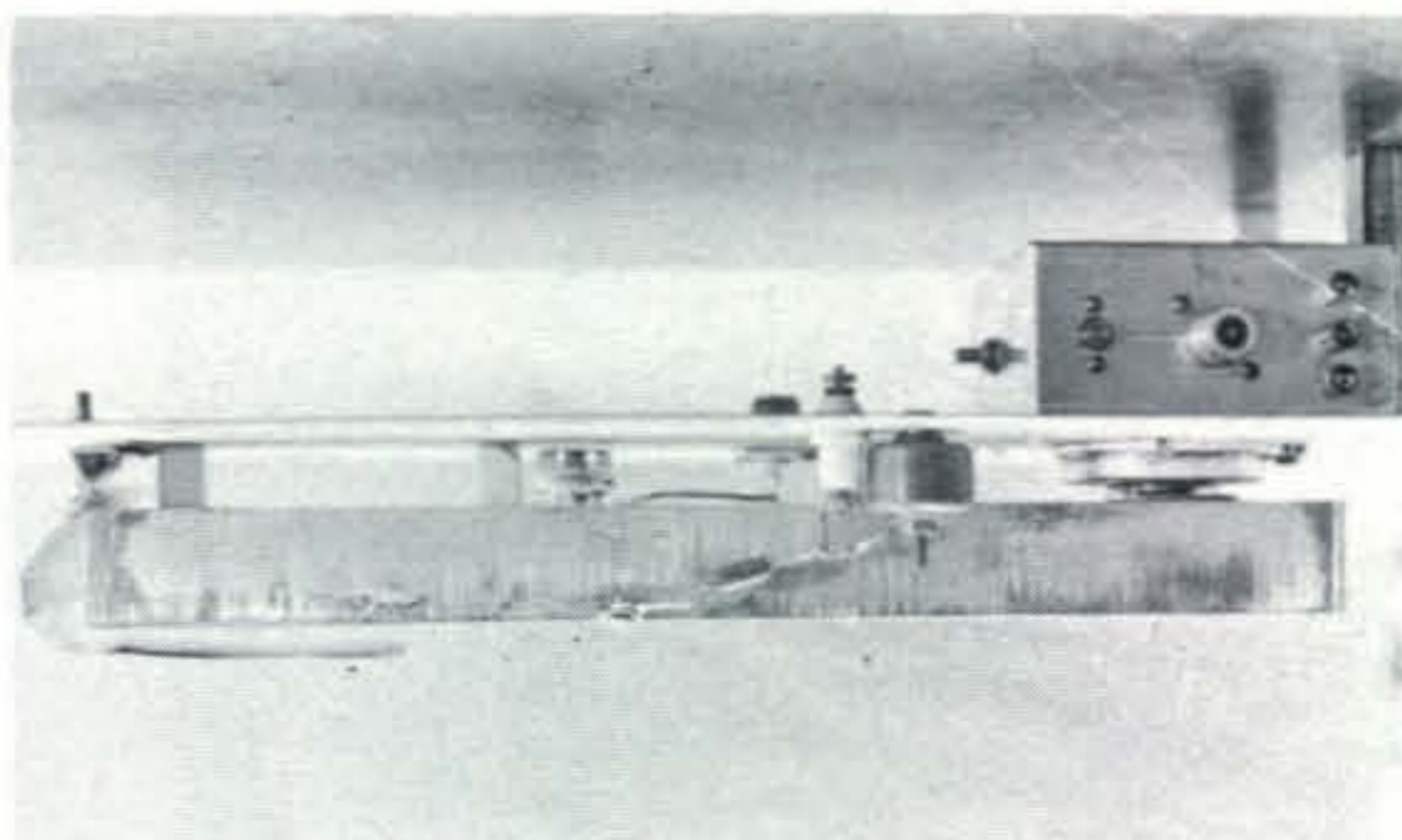
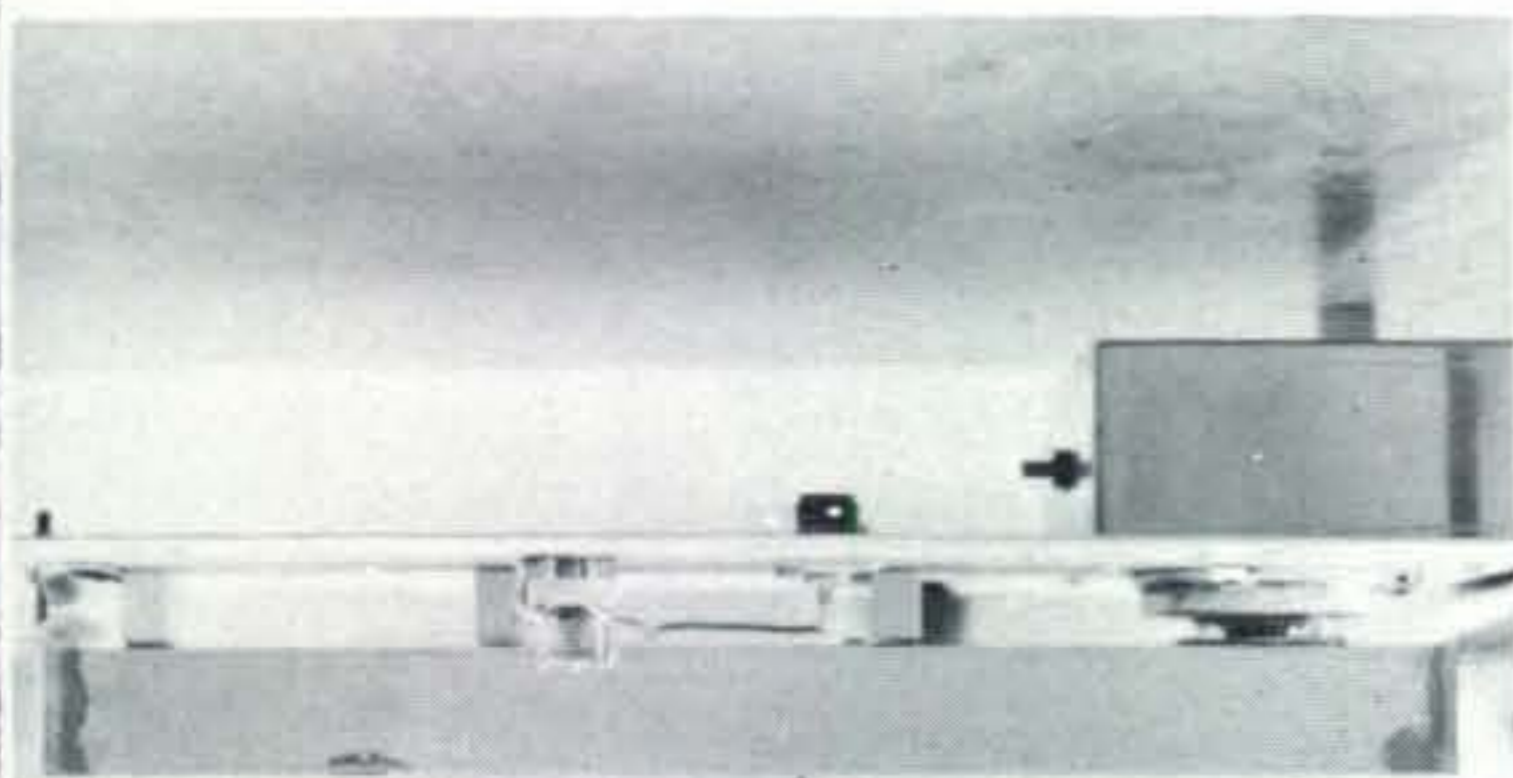
sorbs more heat per unit volume than air, a greatly reduced flow rate may be used. The big difficulty with water cooling is the associated plumbing.

Another technique is vapor phase cooling. This method has the ability to more than double the plate dissipation of a tube like the 4CX250 and is almost as easy to implement as normal forced air cooling. It does use water, but without the plumbing problems. The principle upon which vapor phase cooling is based is that water boils at 100 degrees C. The parameter limiting the dissipation of most external anode tubes is the seal temperature, which must not exceed 250°C for the ceramic versions as the 4CX250 and 150°C for the glass versions as the 4X150. When water is converted into steam an extraordinary amount of heat is consumed by the process. While the conversion is taking place,

the temperature of the water can not rise above 100°C. As long as the anode is immersed in the boiling water, it too can not rise much above 100°C and the critical seal temperature is never reached.

The concept of using vapor phase cooling was first introduced to us about two years ago by W2CLL (x-W7PUA/2). His idea was to contain the water in a tank circuit and run the tube upside down as shown in figure 1. As the tube is operated the water slowly boils away. The length of time between refills can range from several hours of continuous operation to several months, depending on how high a power level the amplifier is being operated. V.h.f. vapor cooled finals have also been constructed by W2CQH, W2CCY, and WA2-FGK. W2CCY built his amplifier with the tube positioned upright and used an O ring

[Continued on page 96]



Two sides of the amplifier. The plate tuning capacitor is shown on the left in both views. Output capacitor C<sub>5</sub> is shown in the left view and the hi-voltage feedpoint is shown in the right view. (photo courtesy of Mark Nadir)

# SURPLUS sidelights

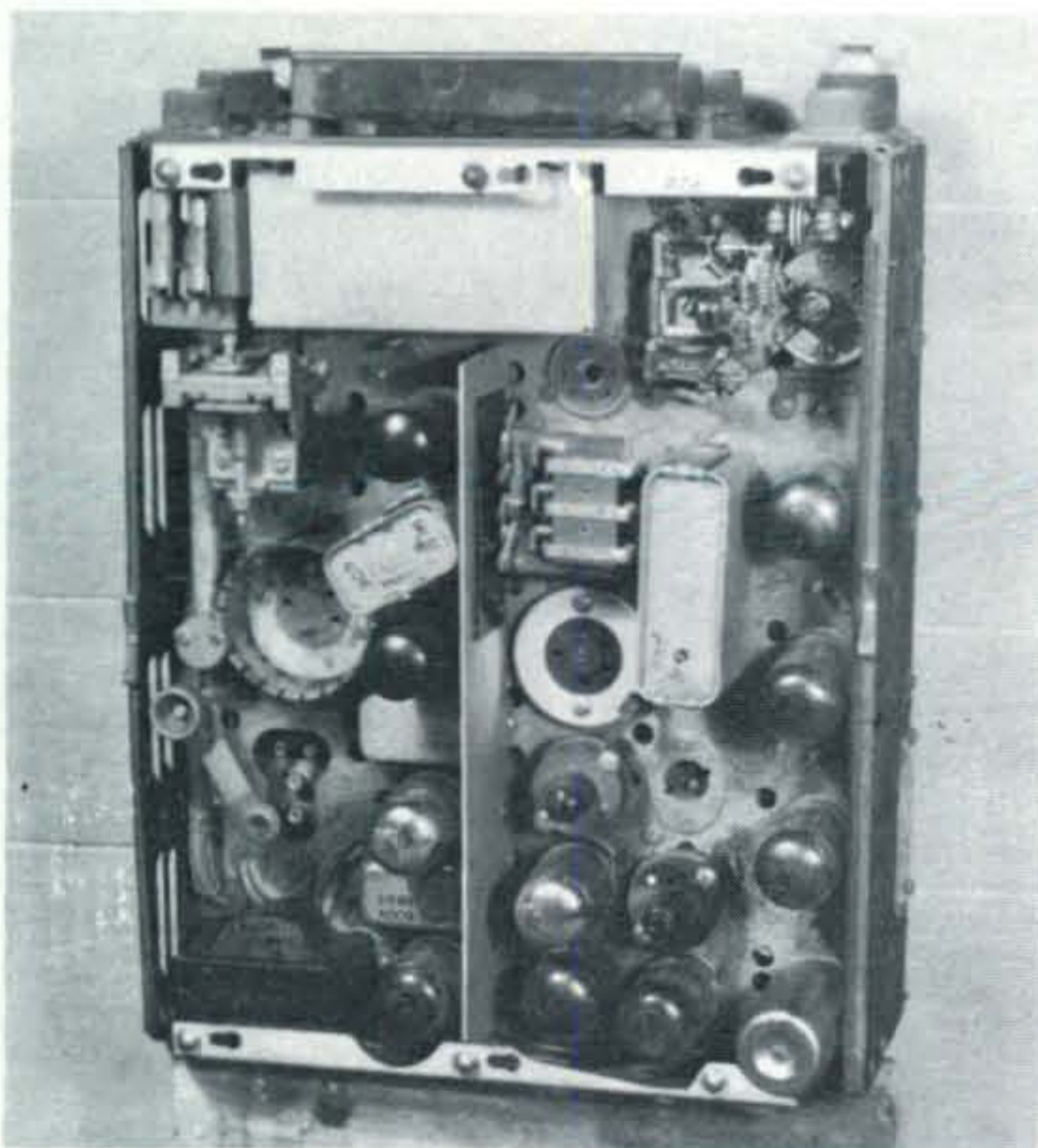
BY GORDON ELIOT WHITE\*

**S**OMEWHERE in the vast labyrinths of the military logistics system, someone has apparently found another hoard of SCR-515 radar identification sets, squirreled away in 1942. My mail indicates that these are again appearing in surplus outlets, demanding conversion information.

By way of background, the SCR-515 is the airborne portion of an Identification, Friend or Foe system, a British idea to enable ground radar operators to determine whether scope blips were German raiders or their own Spitfires—it helped antiaircraft gunners to shoot at the right planes. Later it helped ground controllers sort out the complex air battles.

In surplus, the SCR-515 has been converted to a mobile or fixed-station receiver for the 420 mc amateur band, the 450-460 mc citizens band, and the 470-500 mc experimental TV band. The units are readily available from many surplus houses, particularly G & G, in New York, Columbia Electronics,

\* 5716 N. King's Highway, Alexandria, Virginia, 22303.



The BC-645 transceiver, part of the SCR-515/ABA IFF system.

in Los Angeles, and Fair Radio, Lima, Ohio. Prices now range around \$20-\$25 for a set in excellent shape, plus a few dollars for accessories such as plugs, dynamotor, mount, antennas, etc.

The BC-645 is the chief component of the SCR-515. Under U.S. Navy nomenclature the same set was known as ABA. The unit is designed to pick up signals from a ground radar transmitter, and if the properly-coded pulse sequence is recognized, the BC-645 transmits its own pulse train on the same frequency, creating a "bloom" on the ground 'scope. Presumably an enemy aircraft would be unable to reply properly. The same principles have been updated by the military into incredibly complex IFF systems which are an integral part of "electronic warfare." Going in another direction, civil aviation uses the principle in "transponders" which can send aircraft identification and altitude information to traffic control radars.

Designed by General Electric for the Navy in the late 1930's, the SCR-515 system was an excellent one. Known at first as "RR" (radio recognition) in the U.S., it outdated the British IFF of the time (MK II) and as I have noted, its principle has been universally adopted for civil and military transponders since. The Army's Signal Corps Aircraft Radio Laboratory, at Wright-Patterson, Ohio, dropped its own RR designs when the SCR-515 was tested there. Unfortunately the British did not.

Though the U.S. and the British were cooperating in electronics as early as 1940, the SCR-515 became the victim of a short-sighted snafu between the allies. The British had built a bulky, slow, IFF known as MK II, and by 1941 had an updated version, MK III. The number MK IV was assigned to the SCR-515. Despite its clear disadvantages, the British tended to stick to their own design.

The argument was unresolved on December 7, 1941, but the rush to arm the nation after Pearl Harbor led to a decision to use the tried British unit, which American factories were already building for Lend-Lease. Philco was given a contract for an American version of the MK III, and the SCR-515 was stockpiled for use in case the MK III should be seriously compromised by falling intact into enemy hands.

Signal Corps officers still believe that if the SCR-515 had been adopted, those radar operators at Opana, on the west side of Oahu, would have been able to recognize the blips

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- BC-348 Receiver—200-500 KC and 1.5-18 MC w/Crystal Phasing BFO, and Vernier Tuning, AVC, MVC. Prices: Used, less Dynamotor: \$69.50.....Used, less Dynamotor, operation checked: \$79.50
- Power Supply for BC-348—115 VAC .....New: \$18.95

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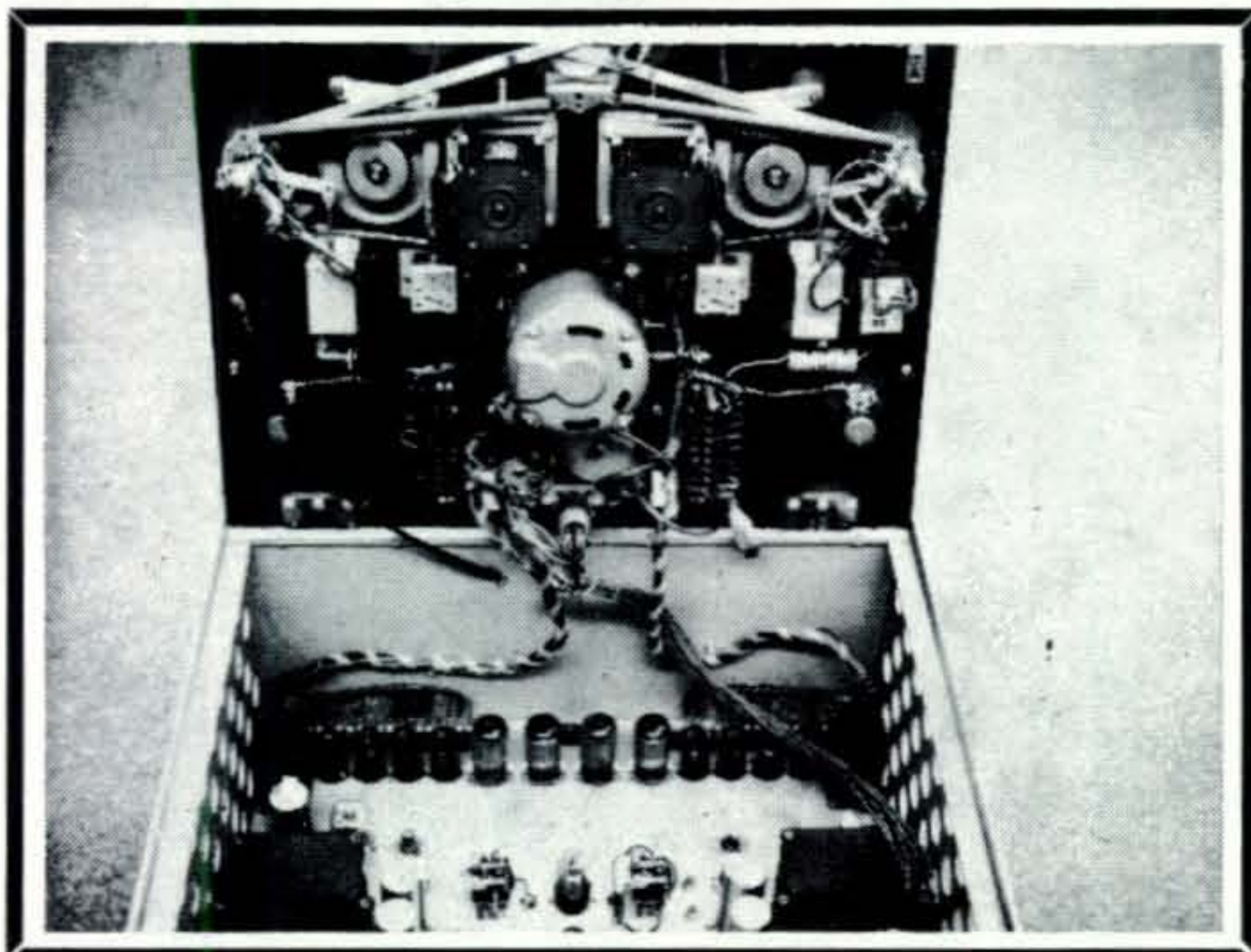
on their screen on December 7 as enemy planes, rather than as an expected flight of B-17's. The operators at their SCR-278 scopes then might have been able to prevent much of the Pearl Harbor damage, though U.S. air forces probably could not have completely protected Hawaii.

A total of 15,000 SCR-515's were bought at a price of \$2,000 apiece, plus many of SCR-532 (short range) and SCR-533 (long range) ground radar sets used in the system. The waste was nearly \$50 million, not including 64 Signal Corps technicians who had just completed SCR-515 training when the decision was made not to use it.

The set itself operates in the 470-495 mc cycle band then used widely for radar, before the advent of microwave transmitters. It had a rated range of 150 miles at 10,000 feet, probably a line of sight figure. Converted for amateur use in the 420 mc band, it would more likely be good for up to 15 miles range depending upon the antenna system. Lack of an r.f. amplifier in the receiver, and using a modulated oscillator without crystal control on transmit side puts it in what Don Storey, W6TNS, calls the "puttering around" class. But it is good fun for someone who wants to break into the ultra-high frequency area cheaply.

Among other interesting things to be noted in the SCR-515 is the self-destruct system. Antedating the sophisticated security system of the U.S.S. Pueblo by thirty years, the BC-645 contained thermite bombs which would destroy the set to prevent its capture. Though these have presumably been removed long since, check for thermite capsules in the bottom of your set, just to be sure, particularly if you get one in its original wrappings.

The receiver section of the BC-645 can be tuned as low as 450 mc by adjusting the silver plated disc between the oscillator lines. The mixer section will handle a 390 to 500 mc band, and require no changes to hit 420 mc. To alter the oscillator, extend the tuned line by about 3/8 inch, and install a front panel tuning capacitor, soldered to the extension. A small butterfly capacitor may likewise

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AN/ARM-65  
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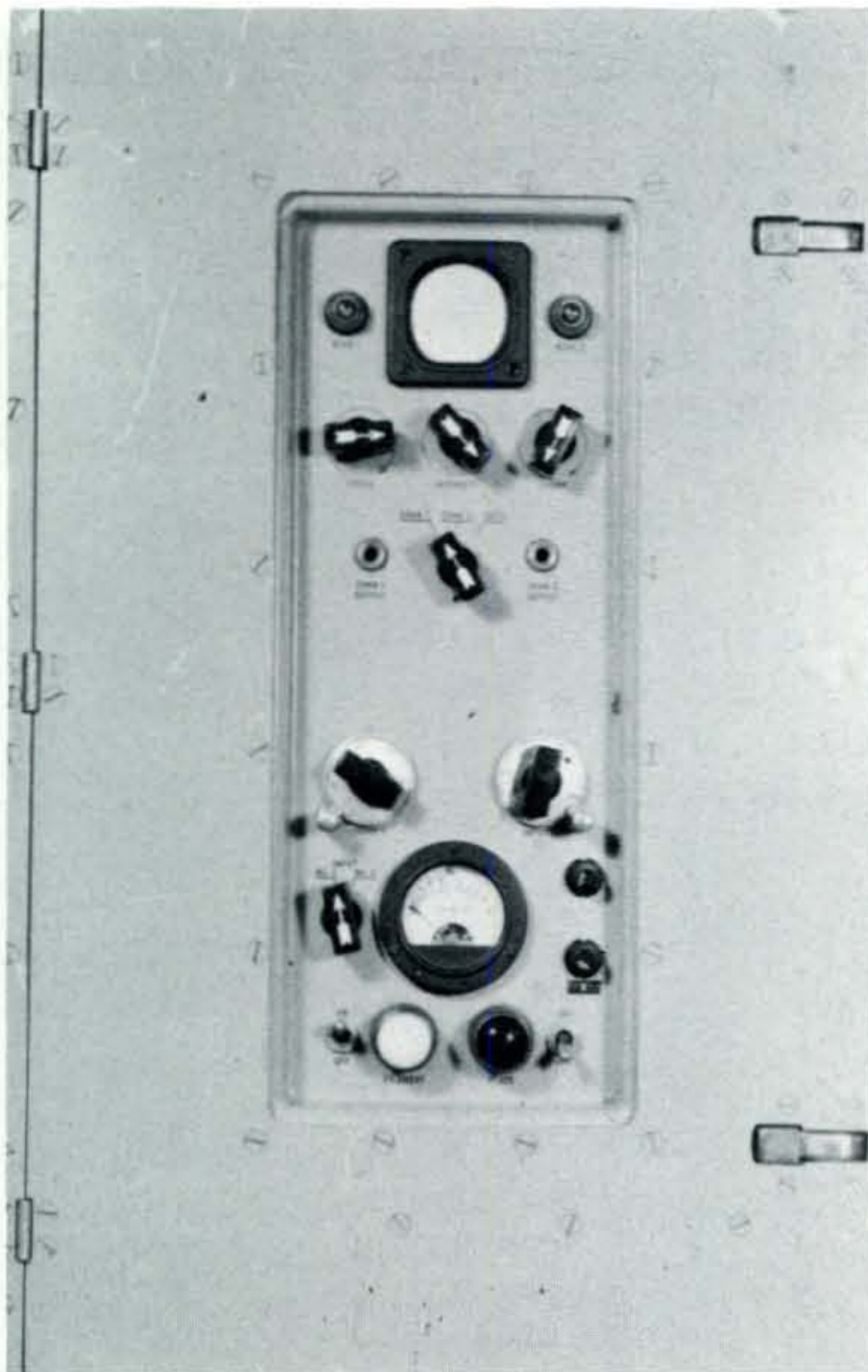
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The mystery FSK unit disposed-of by the Army Security Agency.

mounted at the ends of the transmitting oscillator lines to adjust its frequency down to the 420 mc band.

For further detailed conversion dope, look up the 1956 *CQ*'s at any well-stocked public library.

Switching from the past to the present, I note that recently the armed services have been releasing quantities of once-secret security equipment, notably that used by ASA, NSA, CIA, etc. to monitor various frequencies. Apparently the transistorized material has at last begun to push tube types out. Much of this gear is secret enough that the name plates are removed when it is junked, but not so secret as to need to be smashed. Some of this is carried under nomenclature such as "AFSAV-39C", "ASAN-53" or "ASAN-54." The latter two units are teleprinter converters, similar to the common AN/FCC-3, but I have come across an interesting piece, reported to be AFSAV-35, which is apparently an RTTY converter. This battleship-built unit has an audio input, moni-

tor scope, and audio output. It will accept AFSK RTTY signals and put out AFSK on its own tones, but obviously, from the vast amount of circuitry, it must do more than that.

I have scratched my head over this unit, but so far its secrets—and any manuals—have escaped me. If any readers have any information on it that is not still classified, I would appreciate a note from them.

The AFSAV-39C, while it seems to come from highly secret installations, is common enough to be listed in MIL Handbook 161, as ARA type gear. Identified as a "two-channel rekeyer" it is described as working with DEN-35 and the ASAN-5, whatever they may be.

I would certainly be interested in finding a source for data on this sort of gear, which apparently has real potential for amateur use, now that its secret operations are past. ■

#### VHF Today [from page 89]

to seal off the bottom of the tank and thus prevent the leakage of water. With this configuration, as the water boils away, the remaining supply stays at the base of the anode where it has the greatest effect. The photographs show a 220 mc vapor phase amplifier constructed by us. The circuit is rather conventional. The tank is made from a 12" length of S band wavegrid (although it could have been fabricated from ordinary brass stock) sealed at both ends with rectangles of copper flashing. Regular solder is used since the temperature of the tank should never go above 100°C. It is attached to an aluminum plate on which the amplifier is constructed by means of three ½" long ceramic standoffs. The above amplifier can be driven up to 1 kw input without worry. Similar results have been obtained on 432 mc and 1296 mc (300 watts input with a pair of 3CX100's).

#### Lose Ends

There was a  $4\pi$  left out of the antenna gain formula in the May column. Also we have received questions on the construction of 200 ohm transmission line for use in stacking yagis where K-200 is unavailable. A center to center spacing of three times the wire diameter to be used will produce the desired result. Approximately 3/16" for transmission line made from #12 wire. Next month we plan to get into receiver noise theory. Until then 73  
Allen Katz, K2UYH. ■

# CQ Announces PROJECT UP-STEP

**E**XACTLY ONE YEAR AGO CQ changed printers—and with that change we instituted many improvements and new features in the magazine. Included in those improvements were more pages, full color covers, color inside the magazine, perfect binding, and a general improvement in the quality of paper and printing production.

**W**E'RE NOW READY to go ahead with phase two of our long-term plans for a better CQ. This phase will directly benefit our readers with more articles, more features, and more pages. Our present plans are to enlarge CQ in number of pages as follows: August, 128 pages; September, 136 pages; October, 144 pages; November 152 pages. What happens after that will depend on how you, our readers, respond to what we're doing.

**I**T'S NO SECRET that the ham radio field is getting more competitive every month, and we intend to keep CQ on top by giving our readers more good material than the other magazines. To do this we need more subscribers, especially among those readers who are buying their copies on newsstands and jobber counters. That will free the single copies for even more new potential readers.

**S**O HOW ABOUT JUMPING on the CQ Bandwagon with your subscription. You'll be assisting us in the bigger and better CQ that we have planned for the months ahead. And get your friends and fellow club members to subscribe as well. Remember, what comes in from subscriptions will be spent to give you more great reading.

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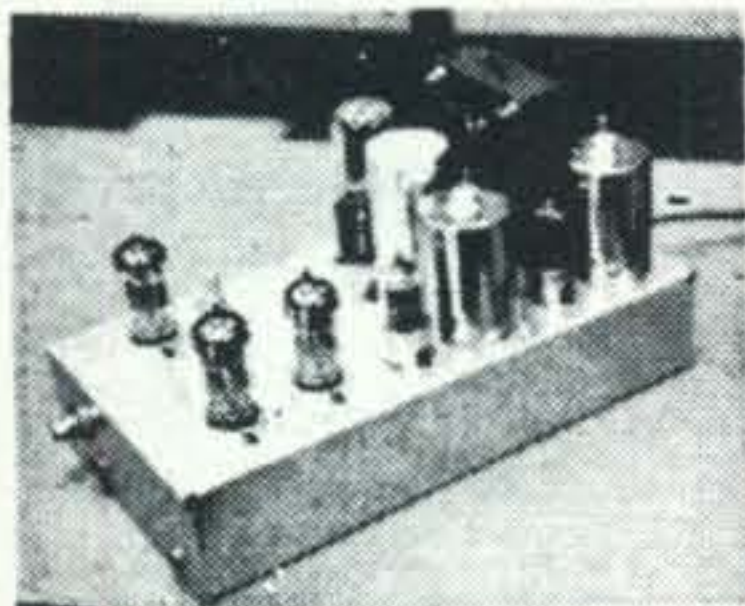
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## USA-CA [from page 86]

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### Notes

*Ordered 8/6*  
The CW County Hunter, a monthly bulletin devoted to c.w. County Hunting, is now being published by Dick Bentley, K2UFT and Rick Lobdell, K2VGR (both are members of the South Shore Amateur Wireless Association of Valley Stream, N.Y.). Their publication deadline is about the 25th of the month and the bulletin is in subscribers hands by the 1st of the following month. Subscription price is \$1.50 per year for 12 issues by first class mail, \$2.00 air mail, to the U.S., Canada and Mexico. Special rates, based upon increased mailing costs, will be available to DX stations. Please make checks or money orders payable to Thomas R. Bentley, 116 Locust Street, Valley Stream, N.Y. 11581.

As you should know, John, K3WWP who spent much time being CHN manager and also ran the 1st CW County Hunter QSO Party last year, (*swell job, John*) had to curtail such activities, so Dick, K2UFT and Rick, K2VGR have been activating the County Hunter Net on 7035 at 1600 Z on Saturdays and Sundays.

And as mentioned in April CQ, Bob Brown, WA9QQB and WA8LWK are trying to pep up things on 7035 Mondays through Fridays at 0230 GMT. By the time you read this, it is assumed the Net will move to 7055. Both groups can use your help and cooperation.

Many thanks to Craig Benjamin, WA4VAP for donating the U.S. Callbook, it is now on the way to Arif, AP2AR in East Pakistan.

Henry A. Doell, WB2RMM, 2015 Victor Holcomb Road, Victor, N.Y. 14564, having recently retired, would be happy to offer his services to overseas county hunters in helping them identify counties for their QSLs that fail to mention the county.

Those responsible for the huge success of the Garden State Amateur Radio Exposition that was held at the Garden State Plaza Shopping Center May 2 to 4th, sure deserve congratulations. In all my years in amateur radio, I have never seen so much publicity in non-ham periodicals. It seemed like all New

Jersey newspapers had front page stories and other items about it for weeks. Full cooperation was had from the Air Force, Army, Navy, FCC, all radio clubs, tremendous attendance by the general public and hams, including famous moon-bouncers like VK3-ATN, KH6UK/W2UK and others including one from PA land and one from HB9 land. Again congratulations for a job well done and such good publicity for amateur radio.

So, what is your problem? Write and let me know—How was your month? 73, Ed., W2GT.

### Mr. One Sixty [from page 69]

tacts with other hams and s.w.l.s, DXing, building, emergency work, making first QSOs with new hams on the air for the first time, visiting other ham stations and photographing them, trying to lend a helping hand where possible within the limits of his time and pocketbook to those needing it, and the operation and maintenance of W1BB and hosting visitors from all over the States, Canada and the world who come to pay a personal visit.

Just recently Stew retired but he continues to be as active as ever not only with his hobby but church work, Civil Defense, professional organizations, Boy Scouts, Masons, Yacht Club, as well as many and varied social activities. Stew and Alice have two sons . . . Skip and Jim . . . but neither took after them as far as amateur radio is concerned. However, Jim has made it possible for them now to be a grandmother and grandfather which is a new milestone in their very interesting and diversified lives.

One sixty is the "forgotten band" by most amateurs. They just don't realize the significance of our first and original portion of the radio spectrum and the satisfaction derived from solid short haul rag chews and the medium to long distance contacts. To many, however, a QSY to 160 is a revelation. The mysteries of these frequencies become a deep rooted addiction, and the thrills provide an awakening to new and more interesting fields to explore. There always seems to be something to look forward to on 160 which continually brings new excitement. One-sixty is a retreat from the maddening scramble of the other bands, its a band where working a G gives you a great feeling of satisfaction and accomplishment whereas working the same G on 20 meters is nothing more than working another G . . . it means practically nothing.

See page 118 for New Reader Service

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## NEW RTY-3 RECEIVING CONVERTER

We had intended to run a picture of our new RTY-3 Teletype receiving converter in this space. The photographer did not deliver the picture on time, so we will tell you about it instead.

Our RTY-2 Teletype converter has been so successful that we have designed a "next generation" unit. It will have a heavier, better designed case, improved circuitry, and will still feature a 100 volt selector magnet supply.

The new unit will be available at the same price, \$139.95, in mid-February.

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Our new literature is still in preparation, and will be available shortly.

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### YL-OM Contest Results [from page 66]

late, or the rules were not followed completely. Recommendations accompanying the

logs will be carefully considered for future contests. And you can mark your calendars right now for the 20th YL-OM Contest: Feb. 22-23, 1969—phone; Mar. 8-9—c.w.

Top three scores in each category, and the high scores for each district or country follow:

#### YL PHONE

PY2SO	90,216
K8ONV	44,712
K9LUI	36,450

#### OM PHONE

K5MDX*	7,619
K2EIU/5*	4,444
K4MYC/4*	4,180

#### YL CW

PY2SO	61,380
VE3BII*	37,661
K8ONV	22,761

#### OM CW

W5WZQ*	4,471
K2EIU/5	4,200
W1PYM*	3,150

#### Top District and Country Scores

##### YL PHONE

W2OWL	7,065
K3WAJ	19,110
WB4BOJ*	20,440
WA5OVX	22,328
W6PQI*	13,644
K7RAM	13,702
K8ONV	44,712
K9LUI	36,450
WA0PPK*	26,163
KL7FQQ	30,640
VE4ST*	20,231
I1SGZ	2,695
CE6CC	8,178
DL3LS	21,318
PY2SO	90,216
VK3KS*	8,702
ZL2JO*	21,525
ZS5FN*	9,075

VK3KS*	19,256
ZL2JO*	5,980

##### OM PHONE

WA1CJR*	3,135
WA2BXX*	1,875
W3BQN*	2,231
K4MYC/4*	4,180
K5MDX*	7,619
WA6KNE	1,204
W7EOI	1,363
WA8WZG*	630
K9UCR*	3,150
WA0GZA	1,410
JH1GMZ*	2,800
LA8PF*	5
W4HSC/VO2	1,350
VE3OL*	747
ZS5FF*	5

##### YL CW

K1NEI	17,556
WA2WHE*	16,575
K3SJS*	21,525
WA4VKG*	21,525
WA5SKI	16,905
K8ONV	22,761
WA9HLY*	7,975
WA0PPK*	11,344
VE3BII*	37,661
DJ9SB	3,248
HA5KDQ	3,104
OH5RZ	3,140
OK1AZQ*	3,570
PY2SO	61,380
SP6AZY*	7,166
UA1ZX	70

##### OM CW

W1PYM*	3,150
K2DDK*	2,814
W3BQN*	1,486
K4BAI*	2,613
W5WZQ*	4,471
WB6THT*	1,415
W7CFJ	1,875
WA8RDW*	1,105
W9LNQ*	3,910
W0LRW*	2,470
VE6UP	1,333
CR7IZ	9
DJ9OZ	124
EA2HR*	70

G3IDG*	90	OZ4H*	56
IT1AGA*	425	PZ1AH*	776
JA2EKR*	53	SP8NJ	144
LA8PF*	38	UA1ZX	70
OH3MF	263	XE1RD*	546
OK2QX*	300		

\* Denotes low-power multiplier

### F.M. Techniques [from page 58]

seem to disturb some fellows too much, as they reason that they can always think up ways to boost the transmitter power to equalize this loss. What they fail to consider, however, is that the attenuation of the feedline will eat a 4.2 db bite out of any signal being received by the antenna, before it ever gets to the receiver.

The 2.1 db difference in attenuation between the two types of coax is sufficient to make the difference between a readable and an unreadable signal, which, after all, is the ultimate test of desirability for any of the elements of the system. The lesson to be learned here is that when working at 100 mc and above, RG-58/U should never be used for runs of more than a few feet such as for a feedline in a mobile installation or to interconnect pieces of equipment.

### Preventive Maintenance

So now you finally have a unit that receives properly and you are hearing all kinds of things you never knew were there. What's needed to keep it that way? Something called "preventive maintenance".

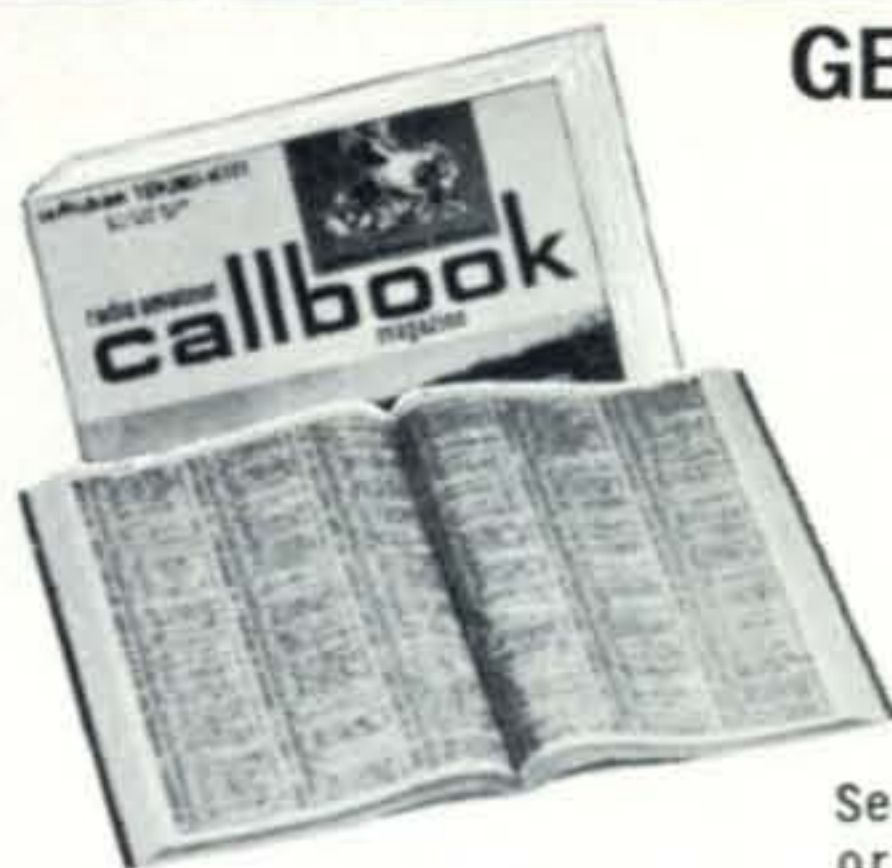
The technique of routine testing and inspection of electronic gear to prevent gradual performance fall-off (as well as to forestall disruptive failures) has been the accepted doctrine of all commercial and military communications organizations for decades. But for some reason, the ham laughs at the idea of this being applied to his equipment. For those amateurs who would rather troubleshoot than operate, this may be an understandable attitude. If you so desire, however, you can go a long way towards keeping your f.m. equipment in good condition simply by testing all tubes at least once every six months and keeping the relay contacts clean. Remember that if you replace a tube in a tuned stage in the receiver, you will have to repeak that stage.

This service routine is especially important in an area where a repeater station is used. Because of a favorable transmitter site and/or high power, the area is blanketed with the

[Continued on page 104]

See page 118 for New Reader Service

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repeater's signal and the local operators tend to get lazy about the condition of their sets. Should the repeater fail and simplex communication be attempted, the results would be disappointing, to say the least. Or, if a mobile from an area that has a repeater takes a trip through territory where stations operate simplex, he may get the mistaken impression that there is very little activity there. The personal opinion of the writer is that the case for repeater stations (in other than mountainous terrain) is often overstated. Direct mobile to mobile communications with reliability good enough for amateur radio is possible over surprising distances when all equipment is functioning properly.

Well, there you have it. With a little understanding and proper care, commercial f.m. two-way equipment will give a ham years of satisfactory performance. The terrific rate of growth of this mode of operation is a good indication of the enjoyment to be had from its use. A correctly functioning receiver is the key to that potential. ■

### Solid State Coupling [from page 62]

Figure 10 shows a typical i.f. stage using transformers with untuned secondaries for the input and output circuits. The input signal is a.c. coupled by means of the step down secondary winding, through the d.c. blocking capacitor,  $C_B$ , to the base. The transistor is forward biased by means of the resistor  $R_B$  and the supply voltage. This provides the proper bias voltage between the base and emitter. The unbypassed resistor,  $R_1$ , in the emitter provides degeneration and reduces the positive feedback produced in the base spreading resistance within the transistor structure itself. Resistor  $R_2$ , in conjunction with  $C_n$ , the neutralizing capacitor, produces an additional negative feedback due to collector current that is directed back to the emitter. The blocking capacitor  $C_B$  in the emitter circuit keeps the supply voltage off of the emitter, and the r.f. choke keeps the emitter above a.c. ground. As a result, the positive feedback is just equal to the negative feedback, and the net result is zero, or unilateralization.

### Bridge Neutralization

The use of bridge neutralization for transmitter amplifiers is well known, and has been applied without difficulty to transistor amplifiers. The equivalent resistance and capacitance of the feedback circuits have already been shown in fig. 9. If these elements are made part of a bridge circuit, and other cir-

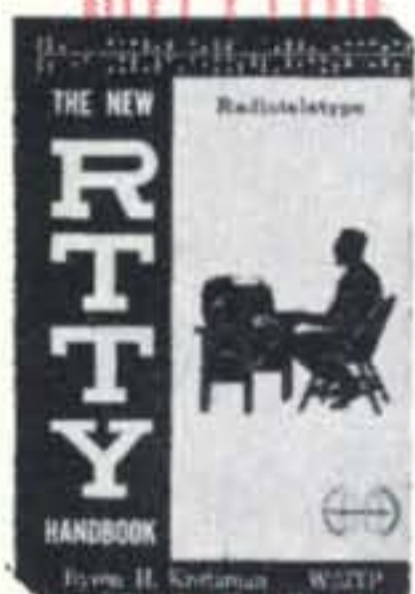
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circuit elements are used as the other arms of the bridge, the entire circuit becomes balanced (as far as the feedback voltages are concerned) and the result is unilateralization. A typical amplifier using such a bridge circuit is shown in fig. 11(A). The components that make up the bridge circuit are shown in fig. 11(B).

When the ratio of the voltages in the arms  $A-B$ ,  $B-C$  equal the ratio in arms  $C-D$ ,  $D-A$ , no output voltage appears between  $B-D$  and the bridge is balanced. Because the phase shift is also balanced, the circuit is *unilateralized*. If a capacitor alone was found to be sufficient ( $C_n$  in the bridge arm) it would be *neutralized*. ■

### Grid Dipper [from page 72]

these have been tuned and installed in the antenna, the other elements may be adjusted to length for resonance of the entire system on the related bands using the g.d.o. as explained for antenna measurements.

**Resonant Transmission Lines:** Resonant transmission lines usually are associated with end-fed Zepp antennas as well as center fed types. These generally are tuned and coupled to the transmitter through either a parallel or series tuned  $L/C$  circuit, depending on the length of the feedline and the feedpoint. The setup may be checked for resonance at the operating frequency using the g.d.o. coupled to the circuit inductor. If resonance cannot be achieved at the desired point, changes may be made in the length of the feedlines or the tuned-circuit constants.

**Un-tuned or Non-Resonant Transmission Lines:** After the antenna has been adjusted to the correct length as indicated by the g.d.o., an untuned or non-resonant transmission line may be connected to it. If the antenna impedance matches that of the surge impedance for the transmission line, the g.d.o. coupled to the line with a small loop will indicate the initial antenna frequency regardless of the line length.

If such is not the case, a matching device will be needed between the antenna and the line. A match will be indicated when the adjustments are made to meet the aforesaid conditions with the g.d.o. coupled to the line.

**Antenna Tuning via 300-ohm Twin Lead:** When the antenna is "up in the air", it may not be physically possible to reach it for a g.d.o. measurement, but the job may be done

[Continued on page 110]



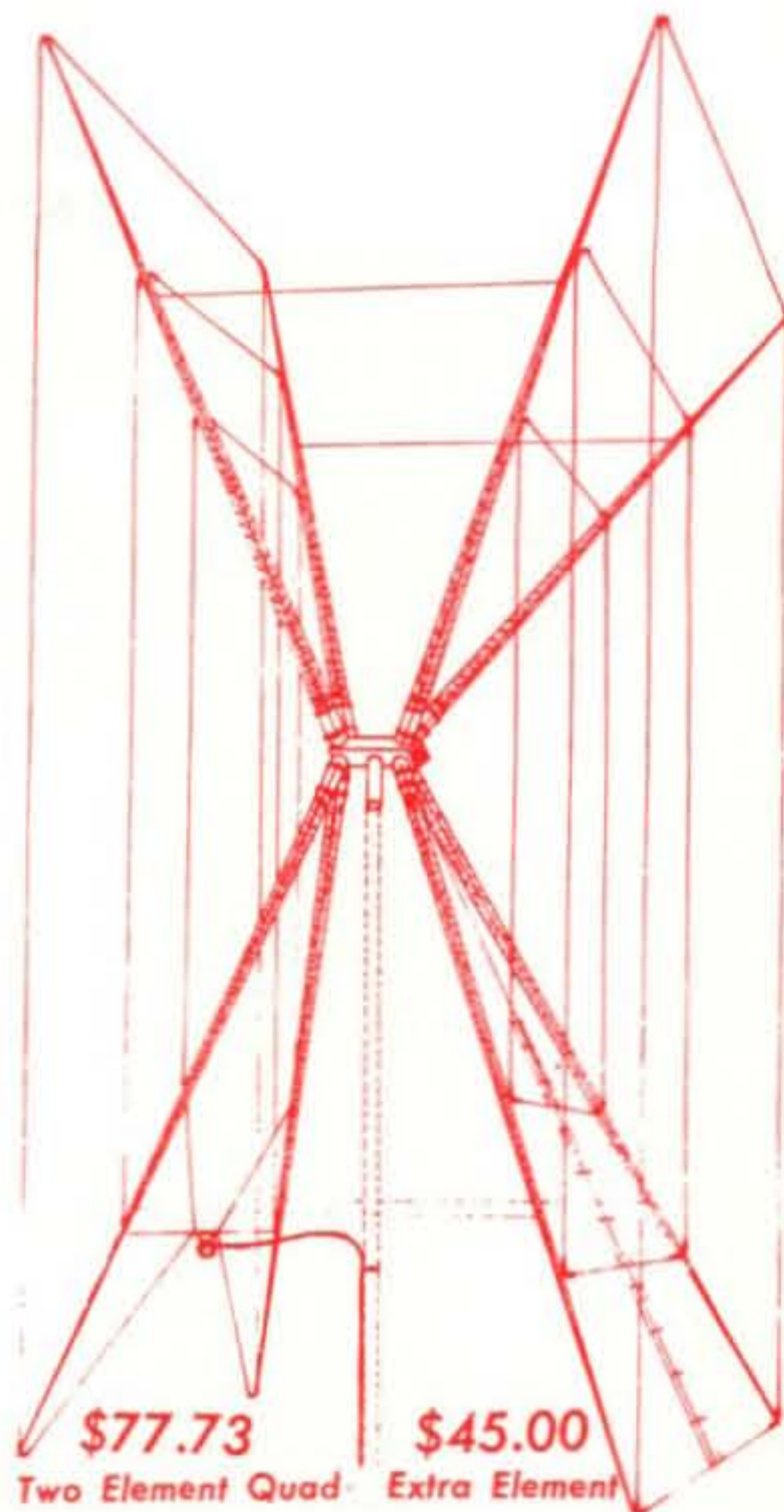
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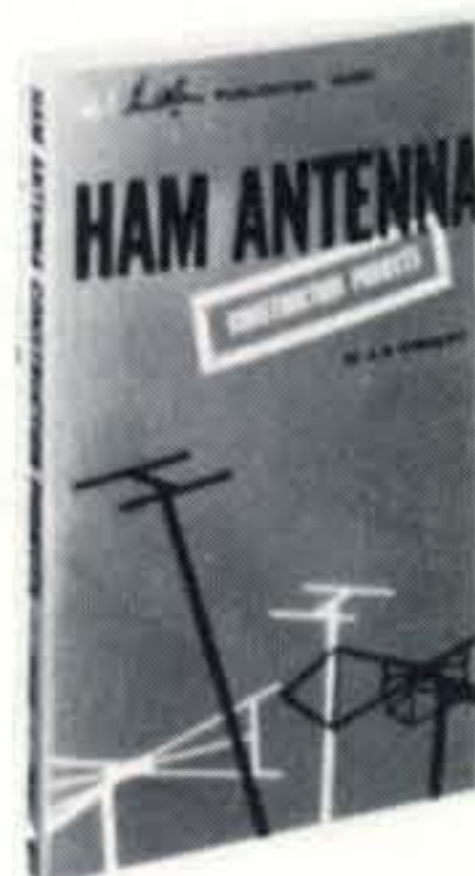


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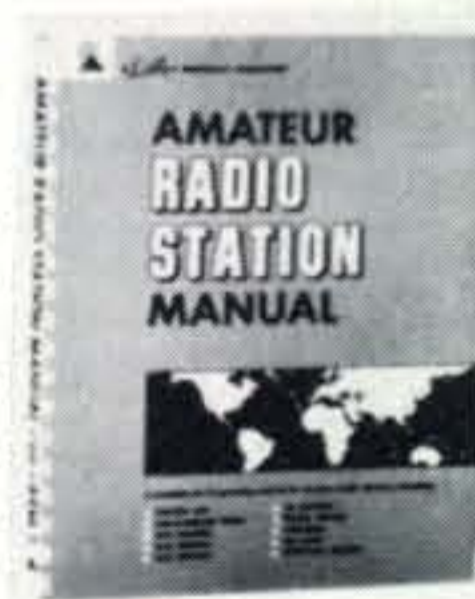


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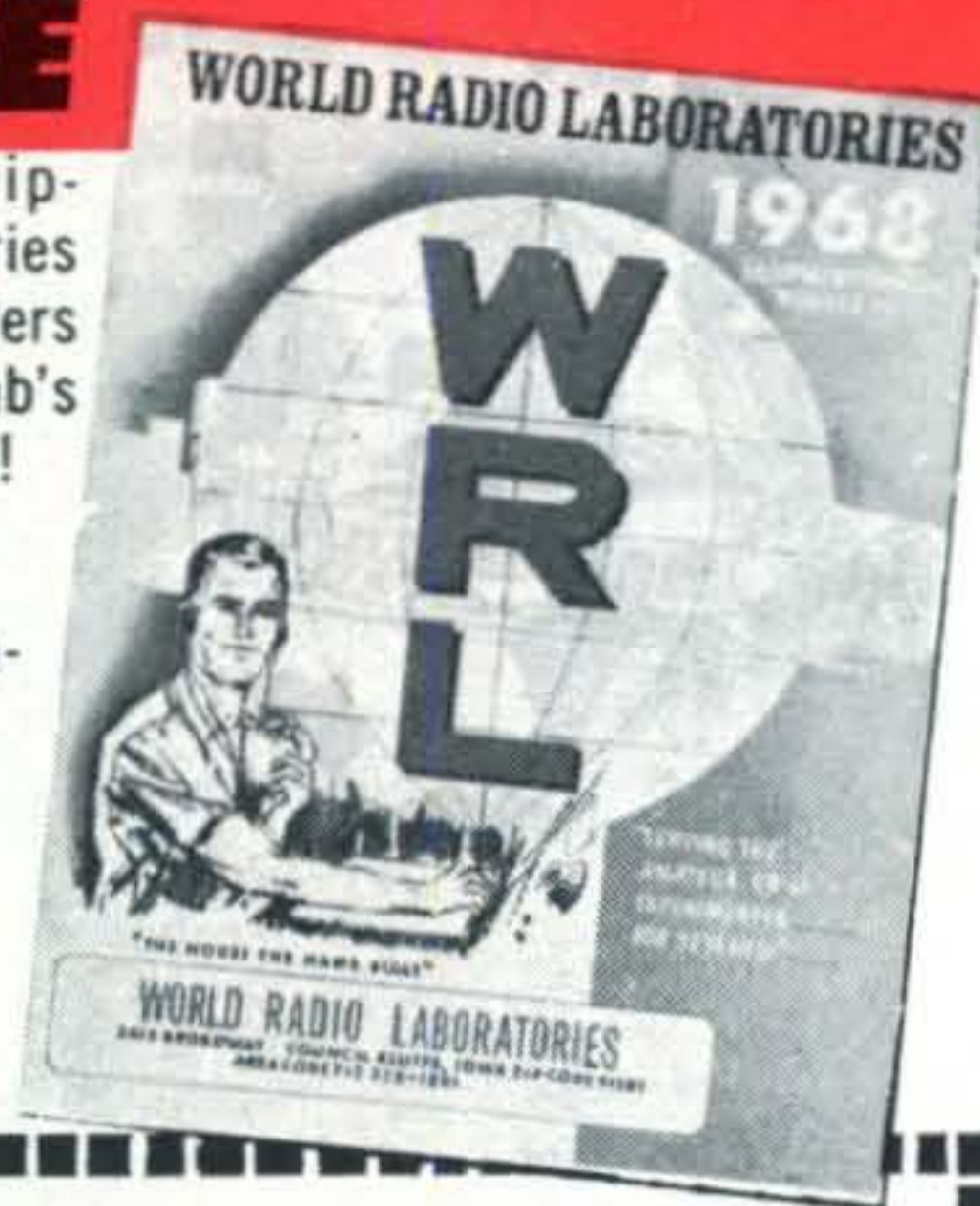
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## Grid Dipper [from page 106]

in conjunction with a half-wave length (or any multiple thereof) of 300-ohm twin lead connected to a low-impedance point at the antenna (center of a dipole).

The line itself should be cut to the proper amount by first determining its length as a multiple of a quarter wave at *half* the desired frequency as found using the g.d.o. as described for quarter-wave *shorted* lines. The short may be a small one-turn loop coupled to the g.d.o. The line will then be a multiple of a half-wave long at the desired antenna frequency and will duplicate any condition present at its far end (only at the frequency for which the line is cut).

When connected to the low-impedance point of an antenna resonant at the same frequency, the same reading therefore will be indicated by the g.d.o. If the g.d.o. dip indicates a lower frequency, the antenna is too long; if the frequency is higher, the antenna is too short. The antenna thus may be adjusted to length as needed to obtain the dip at the resonant frequency for which the twin lead was cut.

## Conclusion

We have by no means included *every* possible application for the grid-dip meter; nevertheless, the information herewith presented should be adequate for most needs and also may serve as a guide line for enabling the user to employ his own ingenuity in other situations. ■

## CQ Reviews: Drake [from page 49]

same receiver conditions.

The good bandpass characteristics of both converters are illustrated by the oscilloscope displays obtained with a sweep generator, as shown at fig. 2.

Prices for the various units are: SC-6 50 mc Converter \$64.50; SC-2 144 mc Converter \$69.00; CPS-1 Power Supply \$12.50; SCC-1 Crystal Calibrator \$24.50; CC-1 Console \$24.50. These are products of R. L. Drake Company, Miamisburg, Ohio, 45342.

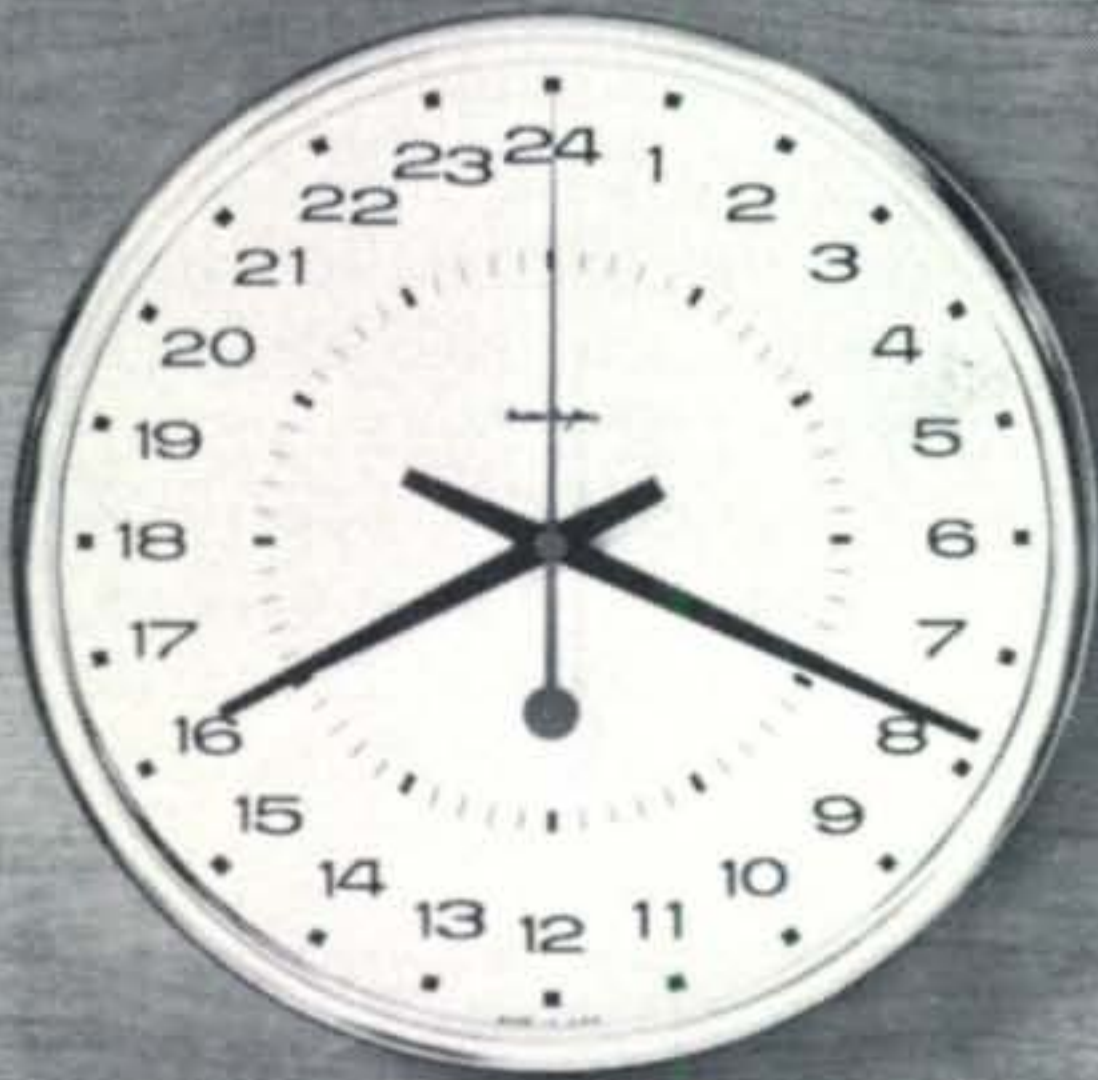
—W2AEF

## Q & A [from page 80]

duction of the modulated r.f. waveforms, use the 5 kc bandwidth position on the SX-117. Also, tune the receiver into the center of the passband. In the case of s.s.b., this will be where the peaks appear to be the broadest.

See page 118 for New Reader Service





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The s.s.b. signals will be heard slightly off frequency when this is done, but you cannot otherwise properly analyze the signal on the scope. A somewhat broader response may be obtained by connecting the scope to pin 8 of  $V_{10A}$  or pin 5 of  $V_9$ . The gain may be lower, but a better reproduction might be had.

Refer to the patterns v.s. bandwidth in the Monitorscope manual.

### MARS Reception on Heathkit SB-300

QUESTION: I have a Heathkit SB-300 receiver which I'd like to use on MARS frequencies. I have been unable to locate any material on changing the frequency coverage, but I think it can be done by changing the heterodyning crystals. Is this correct?

ANSWER: In general you should be able to satisfactorily alter the ranges to accommodate most of the MARS frequencies by changing the heterodyning crystals and retuning their related circuits. A realignment of the pre-selector circuits also may be required.

The necessary crystal frequencies will be the lowest frequency for the desired range plus 8895 kc. For example: for 3289 kc, you'd set the receiver range for 3200-3700 kc, so you can obtain a correlated frequency reading on the dial at "089." This will require a 12,095 kc crystal (3200 + 8895). The crystal-oscillator plate and the preselector circuits may have to be realigned lower in frequency which might require a little padding.

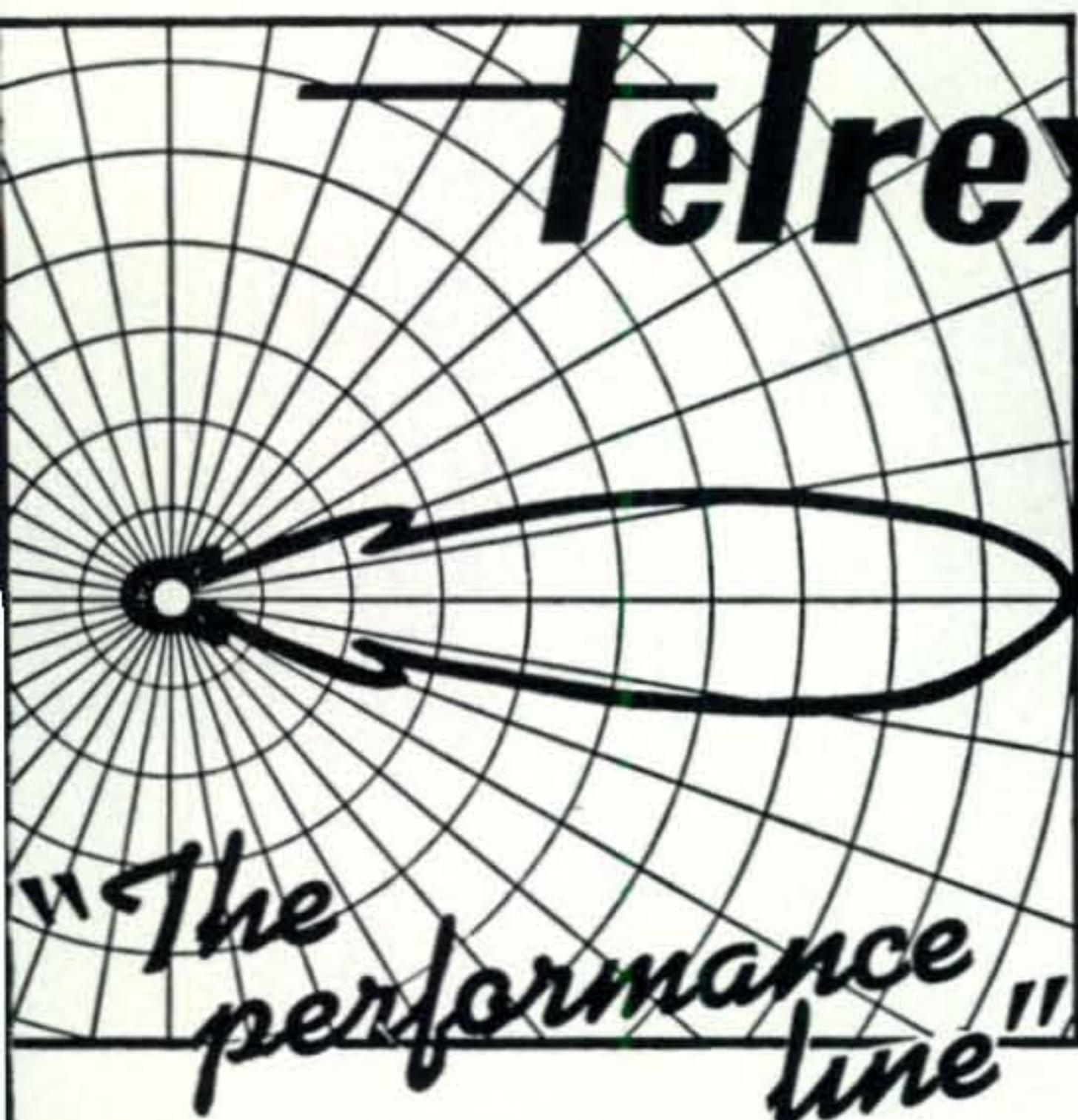
Smaller excursions out of the ham bands will require less drastic realignment.

In the event you experience undesired birdies or spurious signals on a MARS frequency, shifting the receiver range an additional 100 kc with a different crystal frequency most likely will solve the problem.

73, Bill, W2AEF

### DX [from page 76]

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- VP2MU—Via VE2YU (not VE2BRO).
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Plants in Fort Myers and Los Angeles, Calif.

**VR6TC**—Box 1, Adamsville, Pitcairn Island, South Pacific.

**W0GTA/LA**—To W2CTN.

**W6TNS/TA**—W6TNS, Box 7388, Alta Loma, Calif.

**XE0VXO**—Herb Schoenbohm; W0VXO/4, 2407 Melon Court, Orange Blossom Estates, Ft. Pierce, Fla.

**YU3TXT**—No. American contacts since Feb. 1, 1968 QSLed by WB6UJO, 9 Junipero Serra, San Rafael, Calif. 94901.

**ZA7F**—Via DJ9OR.

**ZD9BJ**—c/o GB2SM, The Science Museum, South Kensington, London SW7, England.

**ZL5AA**—To ZL2GX.

**4A1CCP**—Box 907, Mexico City, Mexico.

**4Z4AG**—Via WB4FJO.

**5L2PL**—c/o P.O. Box 1477, Monrovia, Liberia.

**5N2AAU**—To WA9UFV, 5417 W. Wrightwood Ave., Chicago, Ill. 60639.

**5W1AR**—Via W4ZXI.

**6O1GB**—c/o WIYRC.

**7P8AR**—Ulli Dehning, P.O. Box 194, Maseru, Lesotho, Southern Africa.

**7Z3AB**—To W4HEG.

**9K2BV**—Via W5GM (ex-W5EGR), 521 Monroe, N.W., Ardmore, Oklahoma 73401.

**9L2SL**—c/o K4MQG.

**9Q5SE**—To W4RNC, 8 Wilshire Drive, Asheville, N.C. 28806.

**9U5CR**—Via P.O. Box 1322, Bujumbura, Burundi.  
73, John, K4IIF

### C.W. Results [from page 35]

please pass the good word to some of the other organizations over there.

Andy, WB2CKS also reported a decided improvement in the USSR logs, so maybe we are getting thru to some isolated areas.

There was only a slight increase in the c.w. returns this year, a little under 6%, 1640 logs to be exact. But add this to the 1271 phone logs and we have a grand total of 2911 which should still qualify us as having the Top Contest in the world. There are 417 winners in 111 countries which is also an increase over last year, for the c.w. section.

And so we wrap up another one. I am referring to Andy Bodony WB2CKS, Fred Caposella W2IWC, Bob Entwistle W1MDO, Ben Lazarus W2JB, and Andy Malashuk W1GYE. We also had John Alline K1YRO for a short period before he wandered off to DU1FH. And Lorraine of the CQ office made our work much easier too.

Just mentioning names seems so inadequate when compared with the work that was involved. A few of you who have done contest work may have some idea what's involved, but believe me there's a lot more than you have ever experienced. So please forgive us if you run across an occasional error.

73 for now, Frank, W1WY

### Propagation [from page 78]

80	06-10(4) 10-18(4-3) 18-00(4) 00-06(3-4)	07-09(4-1) 09-10(4-0) 10-16(3-0) 16-18(3-1) 18-19(4-2) 19-21(4-3) 21-06(4) 06-07(4-2)	06-07(2-1) 07-09(1-0) 09-16(0) 16-18(1-0) 18-19(2-1) 19-20(3-1) 20-21(3-2) 21-04(4) 04-06(4-3)	07-18(0) 18-19(1-0) 19-20(1) 20-21(2) 21-03(4-3) 03-04(4-2) 04-05(3-2) 05-06(3-1) 06-07(1)
160	17-18(1-0) 18-19(1) 19-21(3-2) 21-23(4-3) 23-05(4) 05-07(3-2) 07-08(1) 08-09(1-0)	18-19(1-0) 19-20(2-0) 20-21(2-1) 21-23(3-2) 23-03(4-2) 03-04(4-3) 05-07(2-1) 07-08(0-1)	20-21(1) 21-00(2-1) 00-03(2) 03-05(3-2) 05-06(1) 06-07(1-0)	20-22(1-0) 22-00(1) 00-05(2-1) 05-06(1-0)

### HAWAII

#### OPENINGS GIVEN IN HAWAIIAN STANDARD TIME †

To:	10 Meters	15 Meters	20 Meters	40/80 Meters
Eastern USA	13-16(1)	06-09(1) 09-12(2) 12-16(3) 16-18(2) 18-20(1)	13-15(1) 15-17(2) 17-18(3) 18-22(4) 22-00(3) 00-02(2) 02-04(3) 04-06(2) 06-08(1)	18-20(1) 20-00(2) 00-02(1) 21-00(1)*
Central USA	12-14(1) 14-16(2) 16-17(1)	05-06(1) 06-12(2) 12-14(3) 14-16(4) 16-18(3) 18-20(2) 20-21(1)	06-08(2) 08-14(1) 14-16(2) 16-18(3) 18-00(4) 00-02(3) 02-04(4) 04-06(3)	20-21(1) 21-22(2) 22-01(3) 01-02(2) 02-03(1) 20-22(1)** 22-00(2)** 00-02(1)**
Western USA	10-12(1) 12-14(2) 14-18(3) 18-20(2) 20-21(1)	06-07(1) 07-08(2) 08-10(3) 10-18(4) 18-20(3) 20-22(2) 22-00(1)	05-08(4) 08-10(3) 10-13(2) 13-15(3) 15-22(4) 22-00(3) 00-05(2)	18-19(1) 19-20(2) 20-02(4) 02-04(3) 04-05(2) 05-06(1) 19-20(1)** 20-22(2)** 22-02(3)** 02-03(2)** 03-04(1)**

### ALASKA

#### OPENINGS GIVEN IN GMT ‡

To:	10 Meters	15 Meters	20 Meters	40/80 Meters
Eastern USA	Nil	21-00(1) 00-02(2) 02-03(1)	12-15(1) 22-00(1) 00-02(1) 02-04(3) 04-05(2) 05-06(1)	07-10(1)
Central USA	Nil	20-00(1) 00-03(2) 03-05(1)	13-16(1) 22-00(1) 00-03(2) 03-06(3) 06-07(2) 07-09(1)	08-12(1)
Western USA	01-04(1)	17-22(1) 22-00(2) 00-02(3) 02-04(4) 04-05(2) 05-06(1)	13-14(1) 14-15(2) 15-19(3) 19-01(2) 01-03(3) 03-06(4) 06-08(3) 08-09(2) 09-11(1)	07-09(1) 09-12(2) 12-13(1) 09-12(1)**

# Ham Shop

**Advertising Rates:** Non-commercial ads 10¢ per word including abbreviations and addresses. Commercial and organization ads, 35¢ per word. **Minimum Charge \$1.00.** No ad will be printed unless accompanied by full remittance. **Closing Date:** The 10th day in the second month preceding date of publication.

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Direct All Correspondence & Copy to: **CQ Ham Shop, 14 Vanderventer Ave., Port Washington, L.I., N. Y., 11050.**

**TTY gear for sale.** List issued monthly, 88 or 44 Mhy toroids, encased, five for \$1.50 postpaid. Elliott Buchanan and Associates, Inc. 1067 Mandana Blvd., Oakland, Calif. 94610.

**EARN YOUR DEGREE** in electronics engineering. Highly effective home study courses in electronics engineering technology and electronics engineering mathematics. Free Literature. Cook's Institute of Electronics Engineering, P.O. Box 36185, Houston, Texas 77036 (Established 1945).

**RUBBER ADDRESS STAMP** including call letters. Three or four lines \$1.50. Signature stamp \$3.50. Free catalog. Jackson's D. Box 443-F, Franklin Park, Illinois 60131.

**SL's 100, \$1.25 and up.** Postpaid. Samples, dime. Holland, R3, Box 649, Duluth, Minn. 55803.

**PROTECT** Radio gear with a warning sticker that reads "WARNING PROTECTED BY ELECTRONIC ALARM SYSTEM" Same as supplied to commercial burglar alarm companies. 2" x 3½", yellow/green vinyl applies instantly without water to windows in mobile unit or operating shack. Also ideal for the back door of your house or basement windows. Money back if not satisfied! 3/50¢ 6/\$1.00, prepaid. Order today from: CESR, 4 Parish Court, Tony Brook, N.Y. 11790.

**DAH-DITTER** Electronic Keyer . . . New Integrated Circuit Electronic Keyer. Fully Self Completing on both dit and dah. Built in AC supply and keying monitor. Isolated reed relay output. Completely assembled and tested, ready for operation. Price only \$34.95. Order now direct from M & M Electronics, Dept. 6835 Sunnybrook, NE, Atlanta, Georgia 30328.

**ANTED—QST's**—Last four issues needed to complete private collection 1916—FEB., MAY, JUNE, JULY. Any reasonable price paid. K2EEK, CQ Magazine, 14 Vanderventer Ave., Port Washington, L.I., New York 11050.

**SL's** by RUTGERS VARI-TYPING SERVICE, Thomas St., Milford, N.J. 08848. Free samples.

**SL's — BROWNIE-W3CJI** — 3111 Lehigh — Allenton, Pa. 18103. Samples 10¢ with catalog 25¢.

**AMFESTERS** Radio Club. Chicago, Illinois, proudly announces its 4th Annual Midwestern Hamfest, Sunday August 11th at Santa Park, 91st & Wolf Road near Chicago. The Hamfest features manufacturer and distributor exhibits, swappers row, awards and a variety of activities for all. Clowns and games for the children, activities for the XYL while you enjoy amateur radio with friends and acquaintances. The Hamfest climaxes "Illinois Amateur Radio Week August 3 thru 11th" by proclamation of Governor Otto Kerner. For information and tickets write to Charles Borkowski. WA9TWA, 1851 W. 21st Street, Chicago, Illinois 60608.

**VENTY-METER** Antenna System. Vesto HPX-100 tower, Telrex DM-546 beam and A2675RIS rotor. \$1800 FOB Alamogordo. Write for details, W50PL, 710 Arnold, Alamogordo, N. Mex. 88310.

**EW** Integrated circuit keyer. Fully self completing. Built in AC supply and keying monitor. Relay output. Ready for operation. \$4.95. 200 cycle plug in CW audio filter, 6DB gain. \$24.95. Northwest Camera Repair, 3119 Arcade Bldg., Seattle, Wn. 98101.

**S.L. Cards** \$6.95 (1,000) free samples, C.B. Wholesale Printers, P.O. Box 2231, Anderson, Ind. 64011.

**OUR CALL LETTERS**, ½" white embossed characters, black or wood grain vinyl background. On desk nameplate \$2.00. on ¾" vinyl tape \$1.10. Dobbs, Box 653, Merritt Island, Florida 32952.

**AM** Cabinet and racks, ideal for operating position or super rig. Steel desk console 57"W., 47"D., 66"H., 2 racks 21"W., 82"H., the full of plug-in units, tubes, components, other with door. Make offer. K6BCS, (213) 886-0111.

**DUISVILLE** Ham Kenvention, Executive Inn, Saturday, August 31. Featuring Fashions and Wigs for the Ladies. Manufacturer and Dealer Exhibits. DX-er's Delight—State of the Art Forums. Color TV—Semi-Conductor Seminar—Antennas, etc. Flea Market HB-W Contest. Free Coffee. \$3.00/\$2.50 Advance to 648 South St., 40202.

**FOR SALE:** HQ-100AC Mint condx. Knight T-150 Mint condition. Both for \$230. D. Frazier, 628 Kennan Rd, N.W., Huntsville, Ala. 35811

**FOR SALE:** California perforated cabinets 5½ wide, 8½ high X 11 deep suitable for ARC-5 receivers \$5. National Inst Radio course 3 bound volumes \$8. E. Mariner, 528 Colima St, La Jolla, Cal. 92037

**I'M LOOKING** For Teleplex code machine and/or Teleplex records. J. T. Lawyer, 923 W. Birch St, Deming, N. Mex. 88030

**WANTED:** Collins KWMZ 312B4-S line Etc. Also Heathkit SB101-De & AC S-plys. F. Coble, 251 Collier Ave, Nashville, Tenn. 37211

**FOR SALE:** 2 new power transistors for Heath HP13 DC Supply. Ameco PCL-P Nuistor all Band preamp 6 thru 16u built 14 power supply. Bud LF 601 A low pass filter All in Ex cond. What am I offered. M. Murrisey, 752 High St, Harrodsburg, Ky. 40330.

**WANTED:** Early 1920's Battery radio receivers and spark transmitting equipment. Need not be in working condition. State Price. D. McKenzie, 1200 W. Euclid Ave, Indianola, Iowa 50125

**JOIN SPAM**—Society for Promotion of AM. To qualify operate AM 50%. Send SASE with dope ur rig for membership free. D. Hoisington, 202 Baker Dr, Florence, Ala. 35630

**HEATH SB300** and SB400 with all filters \$475. SB200 \$200. All for \$650. Will trade for Xcvr. R. Froehling, Rte 2, Box 227, Sleepy Eye, Minn. 56085

**WANTED** Linear to work with Ht-32A. Will pay maximum cash \$200. All replies answered. A. Davis, J. M. Huber Corp., P.O. Box 831, Borger, Tx. 79007

**AUTO PILOT** for sale, type A3A. Make offer. A. C. Lewis, Box 100, Humboldt, Tenn. 38343

**"SAROC"** advance registration prize \$1,000.00 of radio equipment winner's choice from participating exhibitors at Fourth Annual "SAROC" January 8-12, 1969, Hotel Sahara's new space convention center, Las Vegas, Nevada. FM, Ladies, MARS, RTTY, QCWA, WCARS-7255, WSSB programs scheduled. Registration \$12.00 per person entitles "SAROC" participants to special room rate \$10.00 plus room tax per night single or double occupancy, admittance to cocktail parties, technical seminars, exhibit area, Hotel Sahara's late show, Sunday breakfast equal to any banquet dinner, ask any "SAROC" veteran. Brochure planned November mailing for details QSP QSL card with Zip Southern Nevada ARC, Box 73, Boulder City, Nevada 89005.

**BEAUTIFUL** Gold bordered certificate that no ham station should be without. Answers Questions that visitors may ask. Yours for a donation of Fifty cents. Rockaway Amateur Radio Club, P.O. Box 205, Rockaway Park, N.Y. 11694.

**WORK THE WORLD** by proxy, and get personal satisfaction as a bonus, by helping Handi-Hams, a non-profit organization of physically handicapped amateurs and prospective hams who are financially unable to purchase equipment. Send donations (equip. gears, parts, tubes, etc.) to: Handi-Hams, c/o Ned Carman, W4ZSW, Route 4, Rochester, Minn. All donation will be acknowledged.

**"HOSS-Trader,"** Ed Moory—Say's if you don't buy your Ham Gear from him, you paid too much. "One to a customer please": DISPLAY and DEMONSTRATOR Models with Warranty: SB-34, \$319.00; TR-4, \$479.00; T4X-B, \$379.00; R4-B, \$359.00; L4-B, \$575.00; Swan 500-C, \$459.00; Demo Ham-M Rotator and Classic 33 New Mosley Beam, \$195.00; Special ROHN 50 ft. foldover Ham Tower prepaid, \$188.00; BTI 2000 Watt Linear, \$695.00; Close-out on New Equipment Factory Warranty: Swan 500, \$395.00; New National NCX-200 and supply, regular price \$434.00. Cash Price, \$329.00; T4-X, \$299.00; R4-A, \$295.00; Galaxy 5, Mark 2, \$329.00; Used Equipment: TR-4, \$419.00; Swan 500-C, \$359.00; HT-37, \$169.00; "Ed Moory" Wholesale Radio Co., Box 506, DeWitt, Arkansas 72042. Phone—Area Code (501) 946-2820.

**MANUALS** for surplus electronics. List 15¢. W3IHD, 4905 Roanne Drive, Washington, D.C. 20021.

**MECHANICAL** Electronics Devices Catalog 10¢. Greatest Values, lowest prices. FERTIK'S, 5249B "D", Phila., Pa. 19120.

**CLEAN KWM-2:** Collins modified to meet latest specs. \$825. WA9LNS, 414 Third Ave., Rock Falls, Illinois 61071.

**WRL's** used gear has trial-terms-guarantee! Gonset GSB6-\$189.95; HW12-\$89.95; Galaxy V-\$269.95; SR46-\$99.95; AF67-49.95; Valiant-\$149.95; Viking II-\$79.95; 600 linear-\$179.95; HQ100-\$99.95; 75A1-\$169.95; RX1-\$149.95; RME 4300-\$79.95; Hundreds more—low prices. Free "Blue-Book" list. WRL, Box 919, Council Bluffs, Iowa 51501.

**RUBBER STAMPS**—four lines with call letters \$1.50 postpaid. Finest Quality, Fastest Service, Sherman's Stamp, Box 234, Natrona Hgts, Pa. 15065.

**POLICE—FIRE**—Aircraft—Marine—Amateur Calls on your Broadcast Radio with TUNAVERTER! Tunable and Crystal controlled! Guaranteed! Free Catalog. Salch Company, Woodsboro, Texas 78393.

**FOR SALE:** Surplus Motorola receiver, transmitter, power supply package. 152-174 Mc. F.M. Unmodified; in working condition. With Manual \$50. Also, Mosley CM-1 crystal controlled receiver with manual. New condition. \$125.00 plus shipping. Robert Allen, Box 342, Hurlock, Maryland 21643.

**QST AND CQ** Magazines for sale. Years '29 to present. Send SASE for list. A. Amerald, 8956 Swallow Ave, Fountain Valley, Cal, 92708

**HY-GAIN 40** meter beam mod 402-B \$50. Link 450 MC t-powered transceiver 5894 Final \$40. Trade for Colt .45 Auto. W. Davis, 4434 Josie Ave, Lakewood, Calif. 90713

**FOR SALE:** Heath SB-101 with CW filter HP-23, SB-610, SB-600 and HN-31. All are new and under warranty. Used less than a few hours. Must sell for \$600. W. Bulchis, 64 Summer St, Hawthorne, N.J. 07506

**FOR SALE:** 1 Pr. BC611 Walkie Talkies. Now on 4,080Kc. W/manual \$60. Plus transp. Waterman, 55 Lake Ave, Middletown, N.Y. 10940

**SSB-33(SF)** with Mount SBE mike and SB2-DCP Mobile PS \$235 Perf cond. Also Two er built Apr 68 \$45 with GP-11 \$55. W. Thurston, 216 Cottage Rd, So Portland, Me. 04106

**NAVY LM-14** Crystal Freq. Indicator with power supply and original calib. Book \$50. R. Cabanillas Jr, 12620 Washington Blvd, Los Angeles, Cal. 90066

**SELL:** NC-173 Receiver, Good, \$65. Knight T-150A transmitter, excellent at \$75. Or best offer. Randolph Neal, 2802 Irwin Rd, Huntsville, Ala. 35801

**1914 GERNSBACK** E. I. Co., Catalogue, excellent condition. Swap for Antique radio gear. S. Samuel, 76-13 21st St, Bellerose 26, N.Y. 11426

**RME-69** For sale. Manual included. One Band needs realignment, otherwise ok. Make offer. B. Mollenhauer, 186 West Ave, Pitman, N.J. 08071

**WANTED:** Gonset Comm 4.2 meters or other commercial 2 meter gear, state price & Condition. N. L'Heureux, 13 Libby Ave, Lewiston, Maine 04240

**WANTED:** Motor, 115V, 60 cy. For mite corp. TTy, P/N 2485 or 52-2477 or 521-104 or PD-82/U, FSN 6105-798-0347, D. R. Lee, 1228 Shelbourne Dr., Bethlehem, Pa. 18018

**QST'S** For Sale '23 to '33 incomplete '33 to date a few missing. Best offer A. Gifford, Box 313, Union Springs, N.Y. 13160

**CQ & QST** Magazines back to '54 for sale. Excellent cond. By volume or save \$ and take all. G. Thiele, 3267 Redding Rd, Columbus, Ohio 43221

**SALE:** Johnson Viking I mtr w/829B final, TVI'd FB Speech clipping built-in. Just gone thru & Checked on air. 1st 10 mtr QSO w/gd plane ant. G3. \$50. W. L. Lindblom, 512 Grandview Ave, Chillicothe, Mo. 64601

**FOR SALE:** Collins 32V-2 & 75A-2 A-1 condition, best offer. H. Rearick, 850 Washington St, Gary, Ind. 46402

**FOR SALE:** VHF/UHF equipment, converters, cavities, etc. Send sase for list. A. Bott, 340 South 24th St, Quincy, Ill. 62301

**FOR SALE:** Grimson closed circuit TV system-Camera, 21" Monitor, Sync Generator, Vidicon. Also: 17" marsan monitor. Best offer. B. Cohen, 4811 Tallahassee Ave, Rockville, Md. 20853

**TELETYPE MODEL 19**, complete, good condition, \$100. WE-255 Polar Relay and socket \$3 ppd. J. Hart, 7 Elmtree La., Huntington, N.Y. 11746

**COLLINS S-LINE:** 75 S-3B, 32C-3, 516F-2, SM-2. \$1100. G. Grothen, 710 Arnold La, Alamogordo, N. Mex. 88310

**WANTED:** 110 Volt AC Power supply for Gonset Twing. Good 2 meter Transceiver with 110 volt AC Power supply. W. Luther, Rte. 2, Colfax, Washington 99111

**FOR SALE:** Very clean valiant, 160-10 meters. Works FB \$130. R. Parson, 10726 Bordly Dr, Houston, Tx. 77042

**SWAP:** Model 28 ASR Teletype, Want Audio logging Recorder as used by FAA and others to monitor communications frequencies. Will answer all letters, J. Thomsen, 8280 Tennessee Ave., Clarendon Hills, Ill. 60514

**FOR SALE:** Pair 810's \$5. Polar Relays \$1.75. Cardwell PL-9027 \$7. Shure 1020 Mike \$3. CM-22 Comparator \$25. 4ADP1 \$5. H. Brown, 15 Fisher Dr., Greenville, SC. 29607

**NOVICES:** Sell lysco 600, 40 watt CW for \$35. Sell Heath AT1, 25 Watt CW for \$20. Both Excellent. Want CB rig, will trade or buy. A FOX, P.O. Box 2202, Huntsville, Tx. 77340

**SONY VIDEORECORDER** TV Tape recorder, 9" monitor, camera. Cost \$1400 reg. \$900 new! B. Heil, The Olde Music Shop, 201 North Main, Marissa, Ill.

**HEATH DX-60**, VFO Used to work over 200 counties & 12 countries. Grid meter needs work. \$50 prepaid. C. Smith, Box 558, St. Mary's, Ga. 31558

**SELL I-177B** tube tester with MX949 adapter and manuals \$20. Best offer. BC221AK Freq mtr w/ps. original calibration book and manual \$70, best offer. R. Randall, 1263 Lakehurst Rd, Livermore, Cal. 94550

**SELL:** Lafayette HE-30 Receiver \$40, Stromberg-Carlson Stereo Amp-New-28 watts \$35. Want precision model 110 vom. I. Seidman, 735 Greens Ave Apt. 17A, Long Branch, N.J. 07740

**FOR SALE:** Teletype machine, page printer and keyboard; Master Mobile gear; B&W \$425 filter. G. Smith, 915 Lovera Blvd, San Antonio, Tex. 78201

**FOUR NEW 3"** meters used with birdthru-line 43 or line sections \$15 each. C. Spitz, 1420 S. Randolph St, Arlington, Va. 22204

**SALE:** KW Bandswitch 2p11T, Steatite, \$4 Viking Keyer kit \$ Stereo Preamp for dual 1009 \$7. All new. J. Schultz, 40 Ros St., Mystic, Conn. 06355

**KWM-2 HIGH S. N.** 11648 \$695; 516F-2 AC PS \$80; 516E-1 Hea duty 12VDC PS \$119; 312B-4 Stn. Ctl. \$139; GSB-101 KW Line \$149. All mint. D. Burns, 4410 Reading Rd, Dayton, Ohio 454

**WANTED:** One or Two 4-250 or 4-400 Tubes. Will swap comma sets, Q mult., or Elmac PMR 7 recvr or cash. K. Seil, 66 Shar Dr., Rochester, N.Y. 14626

**SELL:** UTC GG 308 Trans., 110-220 Pri 3500-0-3500 \$75. S LaDag 431 Oakland Ave., Maple Shade, N.J. 08052

**FOR SALE:** Vhf-152A converter 2-6-10 meters \$30. Millen 908 Vhf Transmitter 2-6-10 Meter less ps/mop 100 watts \$50 Ashley, Box 254, Ware Shoals, SC 29692

**TRADE:** 1945 CQs. Send your list for mine. Ditto SRT subchasse Sell vacuum variable, low min; decade count unit. F. Schmi 405 N.W. 30 Terr., Ft. Lauderdale, Fla. 33311

**WOCVU** on the air since 1913. Look for me on 14275KC. Memb of OOTC and QCWA. C. Boegel, 1500 Center Pt. Rd, N.E. Ced Rapids, Iowa 52402

**WANTED:** USM 24A Navy Scope high-voltage transformer and scope for parts. Also need manual for meissner model-ex sigt shifter or will sell. A. Barry, 135 N W Dr., Patrick, AFB, F 32925

**FOR SALE:** Gonset GSB-100 \$175. Hammarlund HQ-110 \$12 Globe Highbander VHF62 \$80 with VFO. Just overhauled w guarantee will ship collect. M. Bronsteins, 5 Lockwood I Roselle, N.J. 07203

**TRADE NCX-3**, NCX-A, NCX-D, Hustler want 75S-1 or R4A or \$22 T. Conley, 28 Bayberry Circle W. Liverpool, N.Y. 13088

**SELL:** SB300 SSB and AM Filters SBA-300-3 6 meter convert \$225. HW-12 \$85. C. Small, Box 71, Marcy, N.Y. 13403

**FOR SALE:** Homebrew Handbook Electronic keyer. W. Kornien 129 Culver St, Somerset, N.J. 08873

**HUNTER BANDIT 2000C** used very little. Expertly wired and excellent operating cond. \$425. G. Fisher, Route 4, Solon, Io 52333

**WANTED:** Following back issues of 73, Oct '60 to April '61 inclusive (Except Dec '60) and Nov '61. L. Sharp, 19 Kelso Chermshire, Brisband, Queensland 4032, Australia.

**WANTED:** Tech Manual or schematics for the TS-47/Apr; a Navy Tdn Vfo. T. Herrmann, 2327 S. East 72nd Ave, Portlan Oregon 97215

**SALE:** Heath 10-21 scope, demod, prove, Lafayette audio generator \$50. You pay express. W. Karl, 24 Mill St, Cooperstown, N 13326

**WANTED:** Prop Pitch Motor in Good working order. State condition and price. M. Knowles, 9 Brown St, N. Billerica, Ma. 018

**WANTED:** Hallicrafters SX-16 SX-18 or SX-28 Cond unimporta State price 1st letter. E. Sjolander, 119 7th St, W., Ashlan Wisc. 54806

**FOR SALE:** Bendix 500 Hertz Mechanical filter that plugs into pin miniature tube socket. This item not direct replacement Collins filter. \$25. H. Hicks, 1911 Bermuda St., Shreveport, L 71105

**WANTED:** Heath-VX-1 Voice Control unit. For sale: Heath HX-30 HA-ZO Linear 6M SSB \$250. Hallicrafters SX-101-A mk III \$14 J. Gysan, 53 Lothrop St, Beverly, Mass. 01915

**DX-40** \$35. VF-1 VFO \$15. Globe HG-303 tx, needs work, \$30. Falk, 5665 Bartlett St, Pittsburgh, Pa. 15217

**FOR SALE:** 36 Foot self supported aluminum tower with prop pitch motor. Will accept best offer. A. Zaroni, 208 Phillips Av Trenton, N.J. 08638

**VRC 19 FM 150-174** Mhz. Transmitter, Receiver, P.S. 6-12-24 3 Units in ease with control head and speaker. 30 Watts. \$4 W. M. Richarz, 519 Davie St, Fayetteville, N.C. 28301

**ADCOM-500-12** Power New \$99. KWM2 & Power \$765. HW32 \$9 32S1-\$440. BTI-New Save or trade. F. Baker, 1 Box 546, McCom Ohio 45858

**SELL:** QST Complete set mint cond May 1929 through 1967 \$8 CQ 1947 through 1967 \$60. Both for \$100. W. H. Campbell, Cedar St, Wenham, Mass. 01984

**FOR SALE:** Spiralray, 144 mc, 25 elements \$30. Mobile R Ameco TX86, HM Brew VFO, Gonset Super 6 w/stabilized Squelch & Noise limiter, console for mtg \$100 w/Topaz power supply \$140, Package only. J. Horner, P.O. Box 533, Groton Conn. 06340

**SELL OR Trade—**Heath SB-400, \$275.HRO-60 with Calibrator a all coils for 80 through 6 meters—new condition \$260. Want NCX-5 or Galaxy V Mark II. Write for list. J. Shank, 21 Terra Lane, Elizabethtown, Pa. 17022

**75 M SSB** Heath HW-12 with xtal calibrator. Less mike & P. \$75. Will deliver 30 mile radius. R. Hutchinson, 1705 Kayw Ave, Bethlehem, Pa. 18018

**FOR SALE:** Heath DX-60 & HG-10 VFO, large collection popular electronics magazine, wanted Nov. '60 & June '62 73 mag. M Hagen, Rd 2 Box 233, Brewer Rd, Waterloo, N.Y. 13165

INT CONDITION SX 130 sell for \$115 on Swap. T. Dornback, W167 21st, Lombard, Ill. 60148.

MILWAUKEE AREA Hams-Aermotor MP-5 \$240 list. 44 foot self-supporting Galvanized steel tower, disassembled, \$75, L. Lawton, 04 Alta Vista Ave., Wauwatosa, Wisc. 53213

LOWATT MOBILE: Sbe 34 Transceiver \$300, SBE-2LA Linear 95, SBE Inverter \$195, Mount \$5, Mike SBE, \$14 package \$680. Fruehan, 1226 Westwood Lane. Fairmont, W. Va. 26554.

LEVISION DX 6 year old DX club with new format. Pictures, International column, DX reports. Dues \$3.50, samples \$.30. Worldwide, TV-FM DX Assen. F. Dombrowski, P.O. Box 5001, Milwaukee, Wisc. 53204.

LE: Heath 10-21 scope, deomd, Provel LX Lafayette audio generator. \$50. You pay express. W. Karl, 24 Mill St., Cooperstown, N.Y. 13326.

STANDING Like new Galaxy V mk II, AC Supply vox, galaxy 100 watt Linear. Factory cartons, checked out as perfect by C Licensed, first-class engineer. 10 spare finals. \$700. W2DAP, Twisting Dr., Lake Grove, N.Y. 11755.

TIQUE TUBES Still ok one 852 and one 808 tube. Also Electro-mike Crystal, model 911, Rus. Sackers, P.O. Box 218, Highland, Mich. 49423.

R SALE: Heath HW-12-A 80 meter SSB Transceiver. Good condition. \$69. A. Gerhard, 326 W 3rd St., Berwick, Pa. 18603.

LL OR Swap—Heath DX-40 xmtr. Gud shape. xtals for 80,40 & 30 thrown in. Make offer. L. Irwin, P.O. Box 55, Weston, Ga. 332.

ANTED: Collins CC-3 for 312B-5 control Antique Kennedy 110 220 receiver Heath kit "Q" Multiplier with power supply. Klein, 107 Wyoming St., Boulder City, NV. 89005.

INSON Valiant II, Perf cond \$140. Delivery locally only. W. Ve, 66 Superior Rd., Bellerose, 26, New York 11426.

ANSMITTER, Eimac A-54H, five bands, \$42.50. Typewriter 2.50. Transistor powr supply \$16.50. Transistor heat sink 75¢. Boer, 449 Hill St., Boonton, N.J. 07005.

R SALE: Motorola 2 meter FM FMtru-5 V Dispatcher, base on 5-300-30 Watts Out. A. H. Carmical, 521 Fleda Rd., Memphis, Tenn. 38117.

R SALE: Heath kit Q-multiplier, Wired, new \$10. Grown Antenna rotor New \$20. Radiart Antenna rotator, Used \$10. CQ's '46 Bu '57. D. Scher, 11 Webster St., Irvington, N.J. 07111.

LL: HQ100 5200 speaker \$125. HQ-110A used 30 hours like new 100. DX-40 a beauty \$50. Globe VFO \$25. J. Renault, Box 53 S, FPO New York, N.Y. 09544.

R SALE: Lafayette HB-500 CB Transceiver \$80. New Hy-gain tank mounted DX CB Topper \$13, Knight KG221A FM Monitor receiver \$38. R. Blizzard, 146 Fortescue Rd., Newport, N.J. 08345.

ANTED: Instructograph code machine in excellent cond with keys and tone source. Price and condition in first letter please. Landry, 15 White Birch Dr., Portsmouth, N.H. 03801.

LL: Drake 2-C omalt/speaker, calib. 2 mo., old \$265. Mint condition. Orig Cartons, Davis, 3518 Indian Lane, Doraville, Ga. 30040.

33A LINEAR Less PL-172 tube for sale or trade or will buy. Need 6 meter gear. L. Hoops, 1704 Glenn Dr, Ft. Worth, Tex. 76131

NATIONS Wanted for Ham operators Radio Club of Clark College. Have Club Call, W7AMD but no equipment. Will pay freight on any donations. Write P.O. Box 1622, Vancouver, Wash. 98663. Donald E. Simonson, Trustee.

BCOR Royal Portable tape recorder Model EP2811-1. 3 3/4" & 1 1/2" speeds. Like brand new. Cost over \$200. Used only 10 hrs. Make offer. E. Colliau, 3809 Chevy Chase Dr., Flintridge, Pasadena, Cal. 91103.

FR: Sell Globe Chief Deluxe, 90W xmtr, with three spare finals, in good condx, First \$35 or best offer. J. Randall, 86 Fairmount Ave., Chatham, N.J. 07928.

R SALE: Call books, Handbooks, Magazines such as CQ and other ham publications. E. Rasmussen, 164 Lowell St., Redwood City, Cal. 94062.

R SALE: Wheatstone oiled perf. tape, 15/32" width. P. Lemon, 4 Stony Pt. Road, Santa Rosa, Cal. 95401.

MPLETE DRAKE Station in mint cond; R4, ms4, T4X, AC 3plus re 520 SL Mic \$750 or best offer. J. Heffler, 2200 Morris Ave, Bronx, N.Y. 10453

FOR SALE: Hammarlund HQ-170C, Heath Apache, Tx-1, Knight R-100 A with S-meter. Make offer on each or as a group. W. Newsome, P. O. Box 542, Wrens, Ga. 30833

SELLING EXCESS Equipment, xmitters, receivers, CB, test equipment, tubes, xtals etc. Send SASE for list. W. Toben, 1244 W. Schafer Dr, Tucson, Ariz. 85705

SELL OR TRADE: Hallicrafters SR-2000 2 KW PEP Transceiver & P-2000 supply, mint condition \$1050, need Collins gear. D. Burns, 4410 Reading Rd, Dayton, Ohio 45420

SELL: Johnson Viking Valiant \$95; Lafayette HE-30, 9 tube 550 kc to 30 mc rcvr \$60. J. Wasiewicz, 4230 N.W. 10th St., Pompano Beach, Fla. 33063

WANTED: For preservation, any pre-war QSL's showing prefixes, D, EAR, ES, HAF, K4-7, KA, LY, YL, YM, ZT/ZU etc. F. Herridge, 96 George St, Basingstoke, Hampshire, England

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WANTED: Swan 410 VFO and Drake 2B. Samkofsky, 201 Eastern Pky, Brooklyn, N.Y. 11230

HALLICRAFTERS: S-85 for sale. Exclt condx. Perfect for novice \$45 or best. J. Randell, 86 Fairmount Ave, Chatham, N.J. 07928

FOR SALE: NC-270, with manual \$100. Want HA-10 low freq tuner. L. Allen, 6452-A 102nd St, Ewa Beach, Hawaii 96706

SBE—for sale; NCX-3 Xcvr with XCU-27 xtal calibrator and NCX-A power sup, a \$505 value for \$269. Ship wt 55. Looks, works like new. J. Miller, RFD 8 Box 364, Springfield, Missouri 65804

FOR SALE: Drake R4 all extals new cond. \$225. Ameco TX62 VFO621 New \$125. D. Parsche, 2751 Windsor Ave, Chicago, Ill. 60625

TRADE: Johnson Viking II and 122 VFO for SB-10 with manual. H. Windle, 310 W. Palace, Hobbs, N. Mex. 88240

WANTED: Used Vibro-keyer. Sale; Hallicrafter's SX110 general coverage receiver. Make offer. J. Rutledge, Box 211, Lewisburg, Tenn. 37091

FOR SALE: 1948 issues of CQ, all 12 issues in CQ binder. Offer? H. Compton, 205 S.W. 102nd St, Seattle, Wash. 98146

WANTED: Citizen band General MC-6 transceiver. B. McGwier, P.O. Box 565, Grove Hill, Ala. 36451

FOR SALE: Radio and two-way business in sunny California. Radio doctor, J. Mayr, 818 Salem St, Chico, Calif. 95926

SELL: LM 13 Freq meter & 110VAC pwr supply, manual, calib, book, calibrating instructions & graphs, \$65. W. Staudemaier, 1229 Chante Loup dr, Hendersonville, N. Carolina 28739

FOR SALE: Wheatstone perforator tape. P. Lemon, 3154 Stony Pt Rd, Santa Rosa, Ca. 95401

SELL: Galaxy V mk II w/a supp, vox, remote vfo, and rejector. New TH6DX, 70' Rohn Tower prop Pitch, Pair 4-400 GG, HW29A, Scope, Etc. J. Kreska, 2817 Lakewood Dr, Garland, Tx. 75040

2M FM & PD MON PORT. RX w/AM BCB 4 Sale. 146.6-174 MHz, STD 9V BAT, WRIST Strap, Electro-brand, \$10 excellent cond. is perfect. Knight KA-25 12W/chan Amp, Metal case, \$25 OK. Both for \$30. ENA, 204 W Wing, Arl, Hts., Ill. 60005

WANTED: RME DB-20 preselector. State price wanted. E. Sjolander Jr, 119 7th St, W. Ashland, Wisc. 54806

SALE: S-108 \$55. Mosley CM-1 \$75. BC 459 \$8. HT-18 Vfo \$25 FOB. H. Mohr, 1005 Wyoming St, Allentown, Pa. 18103

TWO Meter Station: Clegg 22'er with original box and instructions, halo never used. Make offer. G. Skloot, 158-14 85th St, Howard Beach 14, N.Y. 11414

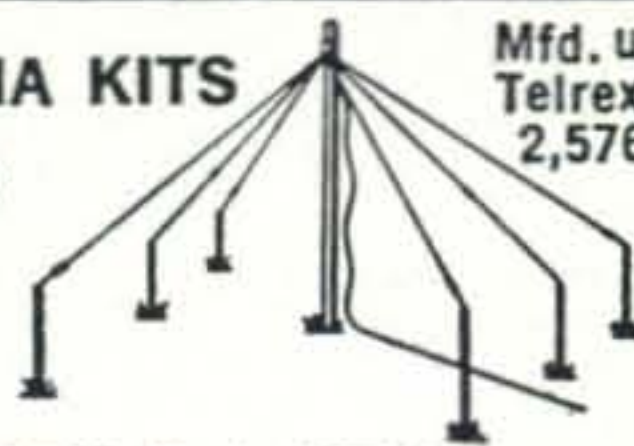
RTTY BACK Issues wanted; all '53 and mar '57. Cash, swap RTTY gear, or rent for duplicating. J. Sheetz, 5 Hansell Rd, Murray Hill, N.J. 07971



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HD	27 to 42 Ft.	33.5	503.50
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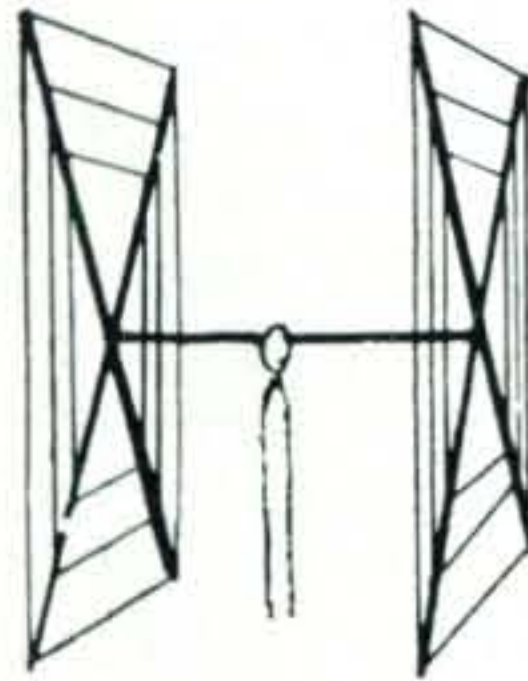
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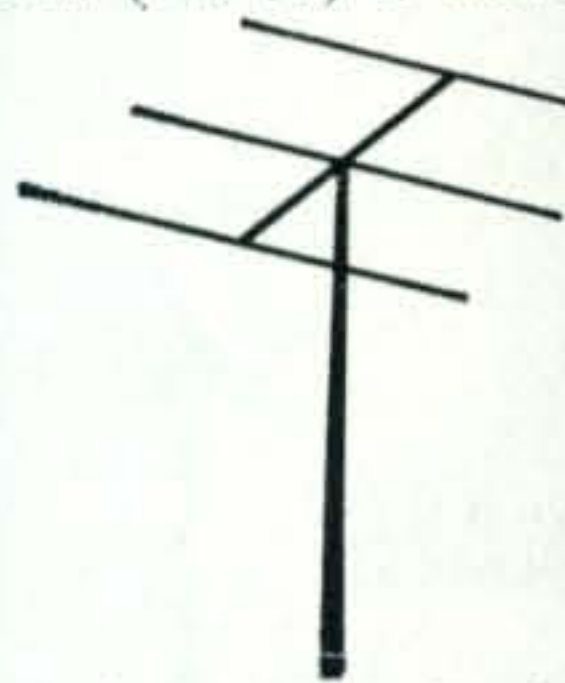
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 Power Rating: 5 KW.  
 Operation Mode: All  
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 Gain: 8.1 db. over isotropic  
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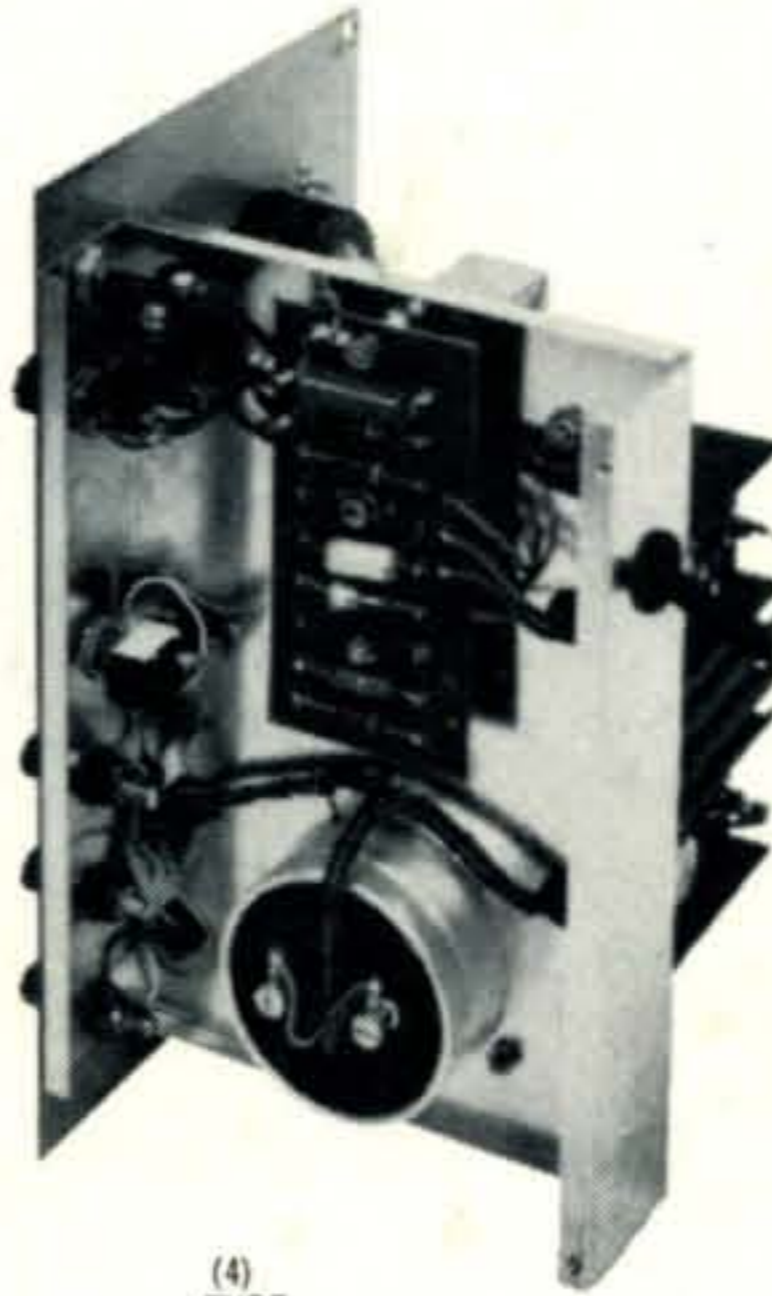
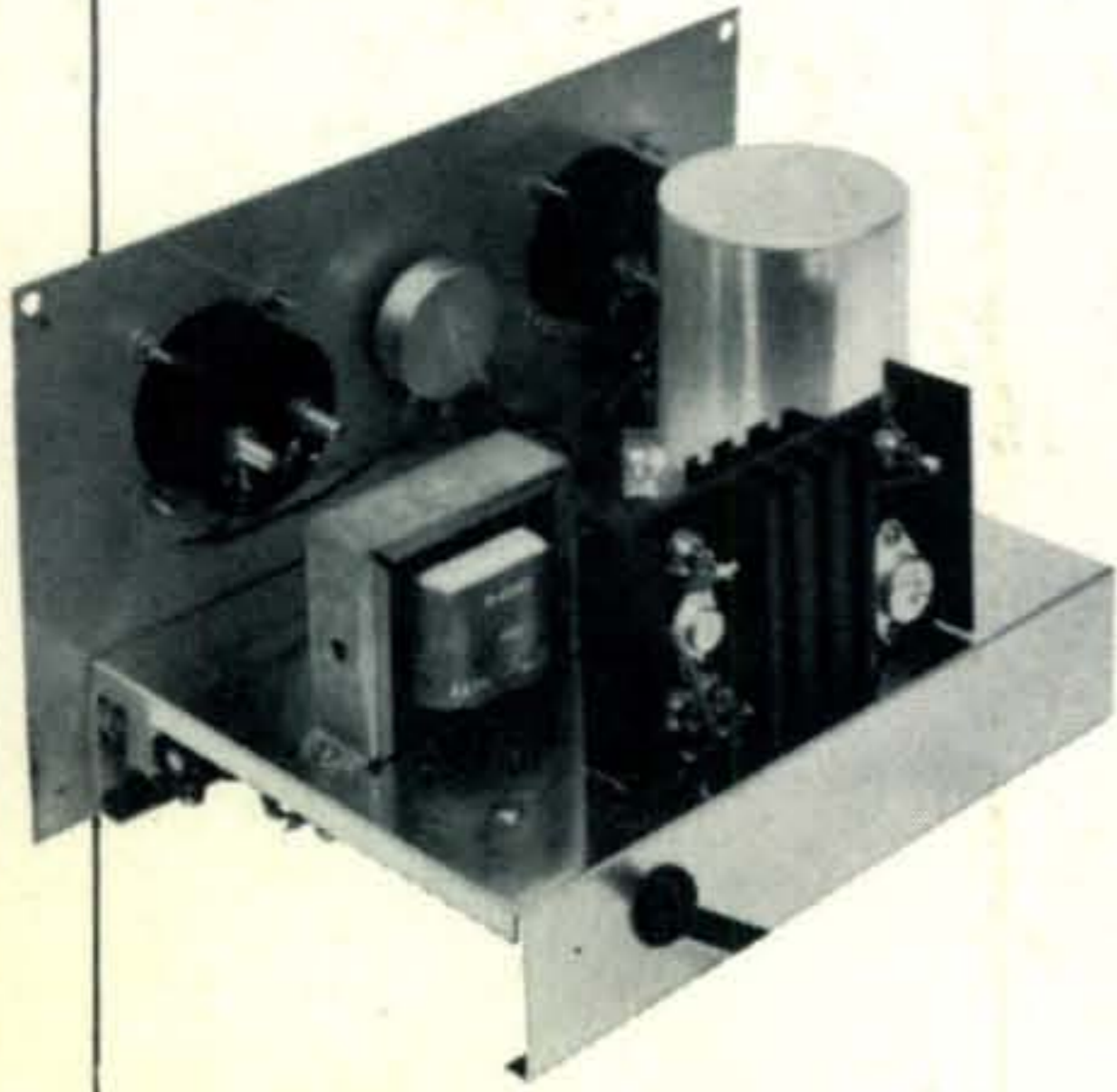
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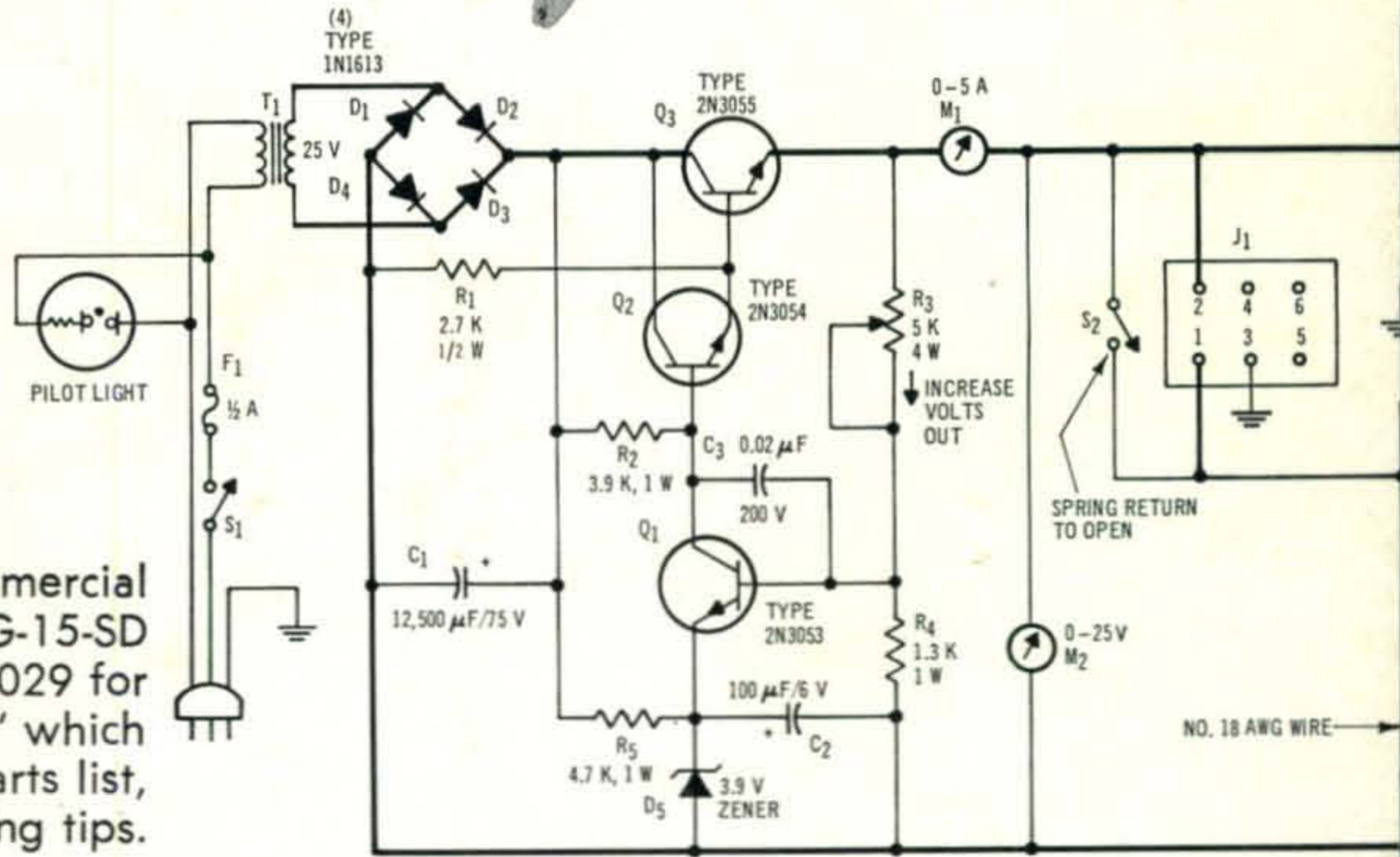
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