

Radio Communication



The Journal of the Radio Society of Great Britain

September 1991

Volume 67 No 9

THE VOICE OF AMATEUR RADIO FOR 78 YEARS

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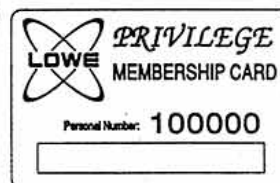
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Radio Communication

Welcome Novices: As the first UK Novices are licensed, this edition features:

- * Nineteen pages of technical information,
- * The return of the *DataComms* column,
- * Our regular full-colour section,
- * Our two-page monthly column exclusively for Novices

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COVER PICTURE:

Minutes after being presented with his Novice Licence by DTI Minister John Redwood (right), Robert Cherry, 2E1AAC, makes the first ever UK Novice contact, watched by Natasha Weir, 2E1AAE (left), Victoria Foster, 2E1AAD, and David Hull, 2E0AAB. Full story - page 5.

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RADIO SOCIETY OF GREAT BRITAIN

THE NATIONAL SOCIETY WHICH REPRESENTS UK RADIO AMATEURS
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PATRON: HRH PRINCE PHILIP, DUKE OF EDINBURGH, KG

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Correspondence to honorary officers should be passed directly to them (QTHR), not to RSGB HQ.

ANNUAL SUBSCRIPTION RATES

Once-off joining fee: £1.50

Corporate members: UK and overseas (Radio Communication by surface post): £30.00

UK associate member under 18: £12.75. Family member: £11.95

UK students over 18 and under 25: £19.20 (Applications should give applicant's age at last renewal date and include evidence of student status)

Affiliated club or society/registered group (UK): £30.00 (including Radio Communication): £17.95 (excluding Radio Communication) (Subscriptions include VAT where applicable)

Membership application forms available from RSGB HQ



HQ NEWS

A VITAL ELEMENT of our strategy is a continuing effort to consolidate and streamline our operations and improve the quality of service from

HQ. We are now in the process of changing the way the amateur radio side of the Society is dealt with.

In future, a small team of trained personnel will provide the contact between our members and HQ. The staff who will be recruited over the next few months will liaise with our Committees, RLOs and volunteers and will provide support for the volunteer field organisation. The recent survey has overwhelmingly indicated that members wish for more active support at local level. The overall cost to the Society will be no greater than at present initially, as the Amateur Radio Manager's post has been cut out. This endeavours to replace one 'chief' with several 'indians' trained in specific areas of amateur radio interest.

As a result of this change, David Evans has left the employ of the Society although I am sure he will take a continuing interest in Society and amateur radio affairs. His many friends at Headquarters and throughout the membership wish him well and every success in the future. I would like to thank him for passing on to me much of his knowledge of the Society and for his unfailing cheerfulness during a difficult period. I have much to be grateful for.

I have just returned from a visit to ARRL in the United States as part of a re-appraisal of the way societies such as ours are run. Many of the problems facing the RSGB have been encountered in the United States and, because of our good relations with our sister Society, I was able to discuss their solutions before deciding how to address ours. We were given a most generous welcome and a great deal of time by ARRL staff; this was greatly appreciated. The benefits are difficult to quantify immediately, but I expect to be selling many more publications in the United States, and have returned with many ideas and projects. The Gulf war and a new no-code licence has boosted the hobby in that country.

Back home we have the results of our survey to assess (full details next month). They provide a statistical sample of the likely opinion of the whole membership. The survey will be continued in order to ensure that August renewals were not exceptional in any way. Many of the questions beg further questions of course, but the aim was to keep the survey simple to maximise the response, and this seems to have worked. The survey will help guide the setting of objectives within a long term strategy, so sudden or immediate action should not be expected.

Philip Smith
General Manager

Council Brief

July 18, 1991.

- Minutes of the Council meeting of 12 May were accepted.
- Terry Barnes, G13USS was elected as President for the year 1992.
- Council agreed that Council Minutes would not be published until they had been confirmed at the subsequent meeting.
- The 1991 AGM will be held at the Royal Society of Chemistry, New Burlington Place, London W1.
- In view of the resignation of David Jackson, G4HYY, from the co-opted position for Zone A, and the lateness of the year, it was decided to leave the post vacant.
- Clive Trotman, GW4YKL, was appointed as Chairman of the Training & Education Advisory Group on a temporary basis. He has also been appointed Liaison Member to the Raynet Committee.
- Council approved recommendations from committees that:-
 The Company Secretary be appointed a full member of the Finance & Staff committee.
 The 70th year of the Patron be marked by a suitable presentation
 Ms Helen Sharman be made an Honorary Member of the Society for her efforts in promoting amateur radio in space.
- G3HCT presented the results of a meeting held by a working group to consider repeater charges: the report was accepted.
- Council agreed to the proposals to modify certain of the Articles of Association at the Extraordinary General Meeting to be held on the day of the AGM. These include the possibilities of the introduction of subscriptions by instalment, modification of the period of grace after expiration of subscription, and allowing the Chairman of Council to stand down as Chairman at any particular meeting where a conflict of interest could be involved, and to introduce Articles defining the position of a General Manager. Full details of these, and any other proposed changes to the Articles will appear in full in an early edition of *Radio Communication*.
- Council agreed to the award of an RSGB Certificate of Merit to Shaun O'Sullivan, G8VPG, (who is, among other things, RLO for Avon, local EMC Co-ordinator, and Chairman of Longleat Rally Organising Committee) for his work for the RSGB in his area.

Minister Presents 1st Novice Licences

THE FIRST new type of UK licence for over 25 years was issued on 25 July when Telecommunications Minister John Redwood presented Novice Licences to seven randomly selected applicants, all youngsters. Mr Redwood said that the Novice Licence (which resulted directly from detailed proposals from the RSGB) "is open to all age groups, but holds particular benefits for the young; it gives training of a practical kind." He added that the DTI would like to see more people enjoying the pleasure of amateur radio. Responding to press questions, Mr Redwood said that "if you are willing to continue learning once you are on the air . . . it may lead to a science based career".

The first Class A Novice Licence, 2E0AAA, was presented to 13-year-old Hugh McNeill who comes from Lancashire and the first Class B licensee, 2E1AAA, is Jonathan Page, (17) from Dorset. The youngest of those present at the ceremony was 11-year-old Vicky Foster, 2E1AAD, from South Yorkshire. All are RSGB members.

The ceremony was chaired by the RA's Head of Mobile Radio Licensing Stephen Spivey and was attended by a representative of the City and Guilds as well as the Press.

Following the formal pres-



The first Class B Novice, 17 year old Jonathan Page, 2E1AAA, being presented with his licence by Minister John Redwood. Watching are (l to r) Sue Tipper (City and Guilds), David Evans, G3OUF (RSGB) and Stephen Spivey (RA Head of Branch).

entations, an historic first Novice contact took place between Robert Cherry (15), 2E1AAC, and RSGB President John Case, operating as G4HWR/M. The equipment used was kindly loaned by British company AKD. Afterwards, the other Novices had an opportunity to air their new call signs.

Each Novice was given a special presentation pack by the RSGB and the G-QRP Club

The Press was well represented, in the shape of the *Early Times* (a teenagers' newspaper), the *Times Educational Supplement* and the BBC, plus of course all of the amateur radio magazines.

Next day, BBC1's award-winning *Newsround* showed

Novice Prefixes

Country	A	B
England	2E0	2E1
Wales	2W0	2W1
Scotland	2M0	2M1
I of Man	2D0	2D1
Jersey	2J0	2J1
Guernsey	2U0	2U1
N.Ireland	2I0	2I1

The Schedule to the Novice Licence showing the frequencies and modes available to Novices was published in March *RadCom*, page 56.

Natasha Weir, 2E1AAE, in QSO with G3OUF and BBC Radio 5 featured Vicky Foster, 2E1AAD. There was local

continued on page 6 ▶

Headquarters Staff Vacancies

AS A RESULT of recent re-structuring of the HQ operation, the RSGB is now looking for two radio amateurs to promote, support and coordinate the amateur radio side of the Society's business.

The successful applicants will need to be well-versed in amateur radio matters and able to pass on information from many sources.

Improving communications within the amateur radio community, and throughout our membership, is a main plank in the

current year's strategy and one of the posts will be clearly identified with this objective.

Please write to the General Manager if you feel you can make a significant contribution and would like to discuss this further.

IOM RLO

THE NEW RLO for the Isle of Man is Brian Brough, GD4PTV, Kimmeragh View, Ballacorey Rd, Bride, IOM.

Zone A

MR T D JACKSON, G4HYY, has been unable to take up the co-opted position of Zone A Council Member. Council has decided that, as the time scale was so short, it would not be appropriate to make a further co-option. To provide members of Zone A with the necessary representation until the end of the year, Council has arranged that those members seeking advice should contact the Zone B or Zone G Members of Council, depending on their location.

Minister Presents Novice Licences

continued from preceding page

newspaper interest in many towns, and more media coverage is expected.

No doubt most members will remember their first contacts, and how nervous they were. Novices should be a little less nervous because of their training but all licensees should endeavour to be as courteous and helpful as possible to Novices (including keeping Morse speeds down). They are, after all, the Class A and B full licence holders of the future.



The first Novice radio contact was made by Robert Cherry, 2E1AAC.



Simon Khan, 2E1AAB, shows off his new licence with his Dad, G3RTU, Mum and brother Daniel (9) who has also taken the NRAE.



DTI Minister John Redwood presented 2E0AAB to David Hull who has appeared on TV demonstrating his other interest – American Indian dancing.



Somewhat overshadowed by the fame of his big sister Vicky, 2E1AAD, was 10-year-old Andrew Foster who was half way through his Novice course. He assured *RadCom* he was now even keener to complete it.



Hugh McNeill being congratulated on holding the first Class A Novice Licence, 2E0AAA, by RSGB President John Case, GW4HWR, who contributed a great deal to the success of the Novice Licence.



A BBC TV Newsround team visited Natasha Weir, 2E1AAE, (r) and her sister Suzanne, who also passed the Novice exam.



The Novices

2E0AAA: Hugh McNeill (13) is from Preston and is in his school and church choirs. His brother Matthew now also holds a Novice Licence.

2E0AAB: 15-year-old David Hull lives in Telford and was taught by his stepfather, G0KYD. He passed the 12WPM Morse Test when he was 13. As a professional American Indian dancer, David has appeared on television on many occasions.

2E1AAA: A Corporal in the Air Cadet Corps, Jonathan Page became interested in radio through CB. He hopes for a career in electronics. Jonathan's brother Gareth is now 2E1ADG.

2E1AAB: Simon Khan (12) is no stranger to *RadCom* having been featured in April's *Novice News*. He has already passed the RAE but could not take out his full licence until he was 14, so the no-age-limit Novice Licence came to the rescue. According to Simon, the RSGB's Novice course was more useful than the RAE because of its practical content. He is now learning Morse.

2E1AAC: As a pupil of Douai College in Reading, Robert Cherry (14) has been involved in contacting a replica Viking boat tracing Eric the Red's voyage from Norway to America. He took the Novice course at school which now has a thriving radio club. An internal telephone system was used to practice QSOs with exotic call-signs. Robert is considering electronics as a career, though he may follow his father into the RAF.

2E1AAD: No prizes for guessing what Victoria (Vicky) Foster from Yorkshire wanted for her 12th birthday, the day after she received her licence (apart from having her ears pierced, that is). She was hoping for a 70cm handheld from Dad, G7FDV. Although a Class B Novice, Vicky proved to be a 'natural' when she tried out an iambic key at a rally, and she has strong opinions on the value of Morse code which differ from her father's! She enjoyed listening to Helen Sharman and would love to meet her. Vicky's classmates have shown an interest in amateur radio and the Barnsley ARC is holding its rally at her school.

2E1AAE: With her Girl Guide uniform packed with badges, it comes as no surprise to learn that Natasha Weir (12) first became interested in the hobby through Thinking Day On The Air.

Thousands of Potential Novice Licensees are Trained in Radio by the ATC

In the Air and On the Air

THE AIR Training Corps (ATC), a uniformed youth organisation, aims to encourage amongst young people a practical interest in aviation and the Royal Air Force. It provides training intended to be useful both in the Services and in civil life, such as fostering a spirit of adventure and developing qualities of leadership and good citizenship.

Cadets have an opportunity to fly in powered aircraft and gliders and to take part in adventurous training and many sports. Training is also provided in such subjects as Principles of Flight, Navigation, and Space Vehicles.

Another subject taught and tested is Radio Communications which includes Morse code at 8WPM. ATC squadrons have their own radio stations and an assortment of frequencies are allocated at HF, VHF and UHF.

First Novice

MANY ATC Instructors are radio amateurs and it follows that many cadets will become interested in the Amateur Novice Licence. It is no coincidence, then, that ATC Corporal Jonathan Page became the first ever Class B Novice licensee, 2E1AAA. Jonathan, who has held a full Radio Officers Certificate for the last two years, found the ATC course somewhat harder than the NRAE as it involved more theory. He has operated on ATC frequencies often, giving displays at Air Shows etc.

Royal Tournament

1991 IS THE 50th Anniversary of the ATC and many special event stations have been put on air using GB50ATC. The RAF stand at this year's Royal Tournament featured the ATC and GB50ATC was operational, together with GB8RT (a theme of the Tournament was Communications). An HF station was organised by Ray Degg of the RAFARS, and Malcolm Wood put together the VHF side which involved feeders going 200ft up an old chimney to the roof of Earl's Court. The station proved to be a great success despite competing with noise from the arena which ranged from band music to gun shots and explosions!



Cadets proudly showing their VHF/UHF Operators Certificates. L to r WO 1 A Halliwell, G6TSW; Sgt H King; Cadet G George; Cadet M Littlewood; Wing Comm J B Parker; Cadet R Halliwell (son of G6TSW); Cadet G Wood (son of G4LED); and Mrs V Middleton, G1LFD.



Part of the ATC stand at this year's Royal Tournament at Earl's Court.

RSGB Council Nominations

THE FOLLOWING vacancies exist for the term 1992-94:

Zonal Members:

Zone A: A vacancy exists in this zone.

Zone C: John Greenwell, G3AEZ, retires but is not eligible for re-election (Article 26).

Zone D: Peter Chadwick, G3RZP, retires and is eligible and willing to stand for election.

Zone F: Terry Barnes, G13USS, has been elected President for 1992 and is therefore not eligible for election to Zone F.

Ordinary Members

Francis Rose, G2DRT, retires

but is not eligible for re-election (Article 26).

George Benbow, G3HB, retires and is eligible and willing to stand for election.

Angus McKenzie, G3OSS, retires but is not eligible for election (Article 26).

Nigel Roberts, G4IJF, was a co-opted member and is eligible and willing to stand for election.

Article 26 of the Society's *Memorandum and Articles of Association* prohibits re-election after two consecutive terms of office.

Full details of how to nominate prospective Council Members is given on page 6 of August's *RadCom*.

Council Candidates

EACH YEAR there are vacancies to be filled on RSGB Council. Details of these, along with information about what is involved in this commitment and the rules for nominations were published last month. This year there are vacancies for both Zonal and Ordinary Council Members. Both have the same responsibilities at Council but Zonal Members additionally supervise RSGB affairs within their Zone and are elected by Corporate Members who reside in the Zones.

Some Members may be encouraged by others to stand for election, while some may feel that they have a certain ability or expertise to offer. What is not always appreciated by new candidates is the size of the commitment and the need to be either involved in, or to have had, active business or commercial experience. Meetings throughout the year on weekdays or at weekends, reading, preparation, correspondence and travelling all require substantial dedication and time. There is also the responsibility of a Council Member both to Members and legally as a registered Company Director.

While a prospective candidate might be willing to meet this commitment, members must be satisfied that they would be voting for, or perhaps nominating, someone who has the skills both commercially and personally to serve on a board of directors controlling the destiny of the Society for the next three years. It is *essential* that a candidate must possess qualities apart from amateur radio involvement which will allow him or her to share in making a positive contribution to the control and future development of the RSGB. In order that Members may make this important choice on their ballot form, candidates intending to seek election should concentrate on details of their abilities when submitting their CV with the nomination. Their achieved excellence in amateur radio need form only a small part of the permitted 200 words.

If you feel you can serve the Society by seeking to become a Member of Council, consider now whether you can give the time that will be required of you and whether you have the ability to participate actively in running a company with an income in excess of £1 Million. If so, then check the August edition for how to become a candidate.

John Forward, G3HTA

RAE and Morse Courses

ORPINGTON – Poverest School, Poverest Road, will start an **RAE course** on Wednesday evenings 7.30 - 9.30 commencing 18 September. For enrolment please write to Bromley Adult Education Centre, Church Lane, Prince's Plain, Bromley, BR2 8LD, Tel 081-462-9184. Early enrolment is advised. For details please contact the Tutor: A E Betts G1HIQ, Tel 0689 831 123. The course leads to the May 1992 examination which will be held at the school.

GREATER MANCHESTER – Radio Amateurs Exam course will start at the beginning of the September term from 7-9pm at Reddish Vale Evening Centre, Reddish Vale Road, Stockport, Cheshire, SK5 7HD. The course will be run on 25 Monday night sessions leading up to the May 1992 exam. Also a **Morse Code Course** of 25 lessons for all levels of ability up to about 17WPM on Thursday evenings 7-9pm. For further information please telephone Dave Wood (Course Tutor) on 061-430 6246 most evenings.

Oldham ARC is running an **RAE course** and examination at its club premises. The course starts on 2nd September. For more details contact Mrs K Catlow, 137 Haven Lane, Moorside, Oldham, Lancs, OL4 2QQ. Tel (Daytime) 061 624 7354 (Evening) 061 652 8617.

Avondale Adult Education Centre, Heathbank Road, Edgeley, Stockport, Cheshire are enrolling week commencing 16 Sept 1991, for **Morse Code Test and RAE Course**. Morse Code Course will be held on Monday evenings 7-9pm and RAE will be held on Tuesday evenings 7-9pm. For further information please contact Rik Whittaker, G4WAW (Course Tutor), on 061 427 4730 (evenings and weekends).

LEICESTER – RAE Course at Charles Keene College of Further Education, Painter Street, Leicester. Classes will be held on Tuesday evenings 6-9pm. Enrolment is 2 and 3 September or on the first night (10 September). For further details please telephone 0533 516037 ext 255/278.

KENT – Maidstone YMCA Amateur Radio Society, **RAE Classes** every other Friday 8-10pm. For further details contact Keith Maskell on 0634 831504. **Morse** Tuition every Friday. Learn CW in the relaxed and comfortable surroundings of your own club; take a 'dummy' test before the real one here in the club. Practice transmissions 8.30pm GB2CW 144.25MHz Sundays. Club net 9.05 every Sunday. **Novice** Tuition classes here in the club every Wednesday but first con-

tact Martin Nash, G0LCH, on 0622 744545.

LONDON – Hendon College is offering an evening class for the **RAE**. It will be held on Thursday evenings 7.30-9.30pm at the Grahame Park, Corner Mead site (near the RAF Museum) starting on Thursday 19 September 1991. Please phone 081-200 8300 for further information.

BUXTON – High Peak College, Harpur Hill, Buxton, Derbyshire, SK17 9JZ is running an **RAE course** on Tuesday evenings for 30 weeks. It will be of 2 hours duration and start in September. For further information please contact Clive Smith, G4FZH, on 0298 85539.

THE WIRRAL – The Wirral ARS is running an **RAE course** commencing September 1991. Norman, G3CSG and Denis, G00TD, both retired school heads of physics, are conducting the course. Prospective candidates should contact Norman Kendrick, G3CSG, at 77 Grampian Way, Moreton, Wirral, L46 0QF Tel 051-677 6368.

NOTTINGHAMSHIRE – West Nottinghamshire College, Derby Road, Mansfield is holding an **RAE course** commencing 9 September 1991 for the May 1992 examination. The classes will be held on Monday evenings, 7-9pm. Course Tutor is Alan Lake G4DVW. For further information please contact the College or ring 0602 382509.

SUSSEX – Boundstone Community College, Lancing, West Sussex will be running an evening class entitled "**Morse Code for the Radio Amateur**". The course fee is £32. Full details from the college on 0903 755895.

BRENTFORD – Brentford Community Education Centre, Brentford School for Girls, Clifden Road, Brentford, Middx, TW8 0PG (tel 081-560 6292) is running an **RAE Course and Morse Class**. Enrolment is on Thursday 5 September 6.30-9.00pm. Enrolment will also be possible by coming to the class. RAE classes start on Monday 23 September. Morse Classes start on Wednesday 25 September. Both start at 7.00pm and finish at 9.00pm. If there is sufficient interest it may be possible to arrange a **Novice RAE Course** on another evening, please contact me or the centre. For more details phone Mr Frank Coles, G3PZC, on 081 977 5343.

W.YORKSHIRE – Keighley College, offers the City and Guilds 765 **RAE Course**. Fees and course information is available by ringing Mr J Simpson, on 0535 618502.

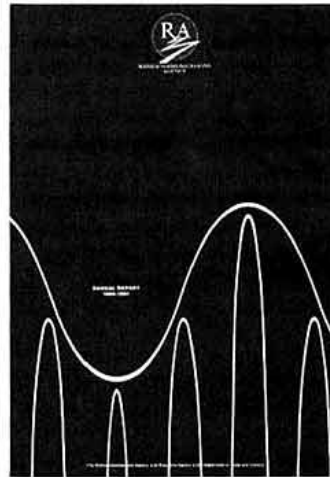
Silent Key Sale

A LARGE collection of amateur radio equipment gathered over a period of 50 years, is to be sold at a Silent Key Sale on Saturday 21 September. The sale, which is being organised by radio amateurs on behalf of Mrs E Verrinder, will start at 11am and take place under cover in the garden of her home in Dorset.

Equipment to be sold ranges from vintage receivers and books, to modern transmitters, receivers, test gear, antennas, magazines and much radio 'bric-a-brac'. Full details of how to get to the sale, with short-form listings of equipment can be obtained by sending an A5 sized SASE to: Silent Key Sale c/o 48 Priory Road, West Moors, Ferndown, Dorset BH22 0AY.

RA Report

THE RSGB was present at the launch of the Radiocommunications Agency's first *Annual Report* on 2 August (see next month for full details). This very readable glossy publication covers all radio services, including amateur radio, and is available from the RA Library, telephone 071 215 2368.



Stolen

FROM HALIFAX, W.Yorks, a Trio/Kenwood TR-751E (with voice synthesiser chip installed) S/N 7100176. Anyone with information should contact Halifax Police. A reward of £100 is offered.

On 29 July 1991, an Icom IC-280E, S/N 8902204. Information to D J Cowley, G1OUI, QTHR.

● AN EXHIBITION of Amateur radio will run from 2 to 28 September at the Central Library, Wellgate Centre, Dundee.

Writers Wanted

RADCOMs SISTER magazine, *D-i-Y Radio* features simple construction projects primarily for youngsters. We are looking for members who like experimenting with such projects and can write them up. Circuits may have been constructed 'ugly fashion', on pin-board, tag-strips, PCB or whatever, but must have been tested and found to be reproducible. Perfect English is not important but it would help if a basic technical explanation were provided. All published circuits will be paid for.

Write to: The Editor, *D-i-Y Radio*, RSGB, Lambda House, Cranborne Road, Potters Bar, Herts, EN6 3JE.

Repeater Papers Wanted

THE SOCIETY proposes to hold a technical meeting to discuss methods for improving repeater usage and a reduction of abuse. Any member wishing to contribute is invited to make a written submission to Repeater Management Group member G4NJU, QTHR, for circulation to other contributors. Submissions are due by 7 September.

Straight Key Day

THE NEXT RSGB Straight Key Day is on Saturday 5 October. It is not a contest; it is an activity period for those who enjoy using straight Morse keys. Frequencies are 7010 - 7030kHz, and times 0900 - 2000GMT. Participants are invited to send details of their key during contacts.

Appointments

AT THE LAST meeting of RSGB Council, Terry Barnes, G13USS, who is currently Zonal Member for Northern Ireland, was elected President for 1992. The current President is John Case, GW4HWR, who did much to ensure the success of the Novice Licence.

Council also appointed Clive Trotman, GW4YKL, as Chairman of the Training and Education Committee, following the resignation of David Jackson, G4HYY, for personal reasons. The appointment is until the end of 1991 when former Chairman John Case will take over the committee once again.

REALISTIC

PRO GRAMMABLE Scanners

■ Covers: 68-88, 108-136 (AM), 136.005-174, 380-512 And 806-960 MHz

A Realistic PRO-2022. Selectable priority channel, two speed scan lockout, scan delay. Also features backlit LCD display. Jacks: 3.5mm headphones, external speaker, external DC power, BNC aerial input. Mains operation or 13.8 VDC negative ground (power cord extra). Memory backup requires 9v battery.
20-9127 £199.95

■ Covers: 25-520, 760-1300 MHz

B Realistic PRO-2006. Features search and favourite channel priority functions. Sound-squelch control prevents lockups on unmodulated carriers. Backlit LCD display with dimmer. AM, FM-narrow and FM-wide modes. Jacks: tape out, 3.5mm headphone, external speaker, external DC power and BNC aerial input. Memory backup requires 9v battery. Mains operation (or 12 VDC cord, extra).
20-9145 £329.95

■ Covers: 66-88, 136-174 And 406-512 MHz

C Realistic PRO-2025. You can select up to 16 channels to scan and you can change your selection at any time. Features automatic two-second scan delay, memory backup, priority channel and lockout function that lets your scanner skip over specified channels. Squelch and volume controls. Jacks: power, external speaker and aerial. 12 VDC neg. gnd. only.
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400-CHANNEL
WITH HYPER SCAN
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16-CHANNEL MOBILE SCANNER
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IC-W2E Dual-Band FM Handheld

ICOM have produced the hand-held with the perfect combination of size and features. This exciting new transceiver is one of the smallest in it's class yet contains so many functions you'd think it would burst!

IC-W2E features include:

- Optional pocket beep and tone squelch for quiet standby.
- High speed scan and priority watch.
- Full 5W output power with external 13.5-16V power supply unit
- 24 hour clock with ON/OFF timer.
- 1750Hz tone call to access repeaters.
- Programmable offset frequency.
- Monitor function that allows you to check repeater input frequency.
- External DC power jack.
- Memory mask to hide seldom-used channels.
- Memory transfer function.
- PTT lock function.
- Keypad and tuning control lock.
- Automatic power save.

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ICOM introduces simultaneous reception of two frequencies in the same band! combine this with simultaneous dual-band receive and you have a breakthrough in features not found anywhere with any other radio. Compact design fully utilises the latest technology while using a minimum of knobs and switches. One-touch controls activate both primary and secondary functions, this ease of operation makes the IC-2410E especially safe when in mobile use.

Outstanding IC-2410E features include:

- Independent volume controls and squelch setting.
- 20db RF attenuator effective against strong signals.
- Built-in duplexer for easy dual-band antenna connection.
- Scan and priority watch functions.
- Illuminated switches and dials for night ops.
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- Optional speech unit.



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Designed with no expense spared, these transceivers offer exceptional performance combined with the ease of operation, a truly marvellous step forward in HF communications. The FT1000 and FT990 feature the very latest in electronics and microprocessor technology to ensure a highly reliable and exciting-to-use transceiver for all modes of operation on the HF bands.



FT-1000

- ★ Amateur Bands Tx 160-10m.
- ★ General Coverage Rx.
- ★ Dual Independent Rx capability.
- ★ Power output up to 200W PEP.
- ★ Auto ATU and internal P.S.U.

FT-990

- ★ Amateur Bands Tx 160-10m.
- ★ General Coverage Rx.
- ★ Power output up to 100W PEP.
- ★ Auto ATU and internal P.S.U.
- ★ 50 Memories.



FANTASTIC PERFORMANCE, REALISTIC PRICE



- ★ 160-10m HF TRANSCEIVER
- ★ GENERAL COVERAGE RECEIVER
- ★ ALL MODE (FM OPTIONAL)
- ★ 0-100W OUTPUT (25W AM CARR.)
- ★ CW NARROW (500Hz) STANDARD
- ★ LARGE CLEAR LCD DISPLAY
- ★ SIMPLE OPERATION (see picture)

All major controls are grouped together for convenience and ease of operation.

The FT-747GX is a compact SSB/CW/AM and (optionally) FM transceiver providing 100 watts of PEP output on all hf amateur bands, and general coverage reception continuously from 100kHz to 30MHz. A front panel mounted loudspeaker and clear, un-obstructed display and control layout, make this set a real joy to use. Convenient features include operator selectable coarse and fine tuning steps optimised for each mode, dual (A/B) vfos, along with twenty memory channels which store mode and skip-scan status for auto resume scanning of selectable memories. Eighteen of the memories can also store independent transmit and receive frequencies for easy recall of split-frequency operations.

Wideband (6kHz) AM and narrowband (500Hz) CW IF filters are included as standard, along with a clarifier, switchable 20dB receiver attenuator and noise blanker. User programming for more advanced control by an external computer is possible through the CAT (Computer Aided Transceiver) System. The transmitter power amplifier is enclosed in its own diecast aluminium heat-sink chamber inside the transceiver, with forced-air cooling by an internal fan allowing full power FM and packet, RTTY, SSTV and AMTOR operation when used with a heavy duty power supply.

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PS304	1-15v Variable	24A/30A max.	£129.95
RS40X	1-15v Variable	32A/40A max.	£189.00

COAX SWITCHES

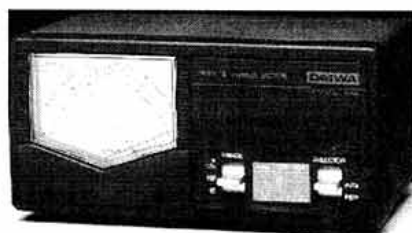
CS201	2 Way SO239	DC-600MHz	1kW	£13.95
CS201G2	2 Way N	DC-2GHz	1kW	£27.50

SWR METERS

CN101	1.8-150MHz	15/150/1500W	£59.95
CN103N	150-525MHz	20/200W N	£69.95

LINEAR AMPLIFIER

LA2080H	2m 1.5-5W in	30-80W out	£159.95
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CN 101

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B22	2m/70cms Dualbander (Black)	0.89m long	CA-14HR	20m Monobander
RS-9	Mini Trunk Mount (Black)		CA-21HR	15m Monobander
CX-702	6m/2m/70cms Tribander	2.1m long	CA-50HR	6m Monobander
CA-7HR	40m Monobander	2.1m long	CA-285	6m/2m Dualbander

TOKYO HY-POWER



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CEB-30	1:1	1.7-30MHz	1kW P.E.P.	£18.95	A
CEB-2000	1:1	0.5-60MHz	2kW P.E.P.	£25.50	A

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CH725	2m/70cm BNC	0dB/3.2dB	2m/70cm	£12.25	A
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CA2x4MB	2m/70cm	4.5dB/7.5dB	2m/70cm	£38.50	C
CA2x4KG	2m/70cm	6.0dB/8.4dB	2m/70cm	£40.75	C

DUPLEXERS

CF-305	50/144 Duplexer	UHF conn.	£25.00	B
CF416MN	144/430 Duplexer	UHF/N conn.	£26.00	B
CFX-514	50/144/430 Triplexer	UHF conn.	£36.75	B
CFX4310	144/430/1200 Triplexer	UHF/N conn.	£36.75	B

MOUNTS

TBR	Adjustable trunk mount	£11.50	B
RS17	Mini trunk mount	£12.75	A
RS16	Mini Gutter mount	£12.75	B
CK-3LX	Mini Cable Assy for RS16/RS17	£16.25	B

MINI MOBILE ANTENNAS

CHL21J	2m/70cm	0dB/2.15dB	2m/70cm	£14.75	B
CHL23J	2m/70cm	2.15dB/3.8dB	2m/70cm	£17.35	B

BASE ANTENNAS

CA350DB	6m/10m	2.15dB/6.5dB	£139.00	D
CA2x4WX	2m/70cm	6.5dB/9.0dB	£80.72	C
CA2x4MAX	2m/70cm	8.5dB/11.9dB	£102.12	C

FILTERS

CF-30MR	HF Cut off	32MHz	1kW P.E.P.	£38.75	B
CF-50MR	6m Cut off	54MHz	1kW P.E.P.	£38.75	B
CF-30H	HF Cut off	32MHz	2kW P.E.P.	£80.75	A
CF-30S	HF Cut off	32MHz	150W cw	£19.35	A
CF-50S	6M Cut off	57MHz	150W cw	£20.35	A
CF-BPF2	2m Band Pass	150W cw	£31.65	A	

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CD-120	1.8-200MHz	15/60/200W	£76.60	B
CD-160H	1.6-60MHz	20/200/2000W	£90.85	B
CD-270D	140-525MHz	15/60/200W	£79.65	B

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CSW-20N	2 way DC-1500MHz	N	£45.95	B

ACCESSORIES

CEP-M2	Earphone	3.5mm jack	£1.28	A
CES-M2	Mini Clip on Speaker	3.5mm jack	£5.62	A
CHM-M4	Mini mic + PTT	2.5mm jack	£9.15	A

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HC400L	160-10m	350W P.E.P.	£203.00	C
HC2000	160-10m	2kW P.E.P.	£365.00	D

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B	= £4.00	E	= £15.00
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HT120	20m Transceiver	10W P.E.P. SSB/cw	£305.50	C
HT180	80m Transceiver	10W P.E.P. SSB/cw	£305.50	C
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HCF100	CW Narrow filter	HT series	£39.85	A
HNB100	Noise Blanker	HT series	£19.95	A
HBK100	Mobile Bracket	HT series	£10.20	A

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HX640	6m to HF	as above	£254.50	B	



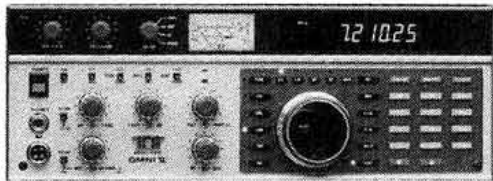
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TT285	6.3MHz 500Hz Filter	61.30	2.00
TT288	6.3MHz 1800Hz Filter	61.30	2.00
TT1140	Circuit Breaker	16.34	2.00
TT217	9.0MHz 500Hz Filter	61.30	2.00
TT218	9.0MHz 1800Hz Filter	61.30	2.00
TT219	9.0MHz 250Hz Filter	61.30	2.00
TT256	FM Transceiver Module for Omni & Paragon	61.80	2.50
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TT705	Ten Tec Electret Desk Microphone	66.41	2.00
TT238	Ten Tec ATU 2.0KW 'L' match 160M-10M	369.55	—
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IC-725	HF All Band, General Coverage Rx 12V	779.00	13.00
IC-726	HF All-Band, General Coverage Receiver with 6m Band, 12V	1,015.00	13.00
IC-735	HF All-Band, General Coverage Rx, 12V	1,000.00	13.00
IC-PS15	External PSU 20A	169.00	10.00
IC-PS30	External PSU 25A Continuous	386.58	10.00
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IC-AT150	Automatic Antenna Tuner 100W	335.00	10.00
IC2SE	2M FM Handportable inc Nicad /Charger	279.00	5.00
IC-2SET	2M FM Handportable, Keypad entry, DTMF	299.00	5.00
IC-229E	2M FM Mobile, 25W 20 Memo 12V	299.00	5.00
IC229H	2M FM Mobile 20W 20 Memo 12V	349.00	5.00
IC-275E	2M Transceiver, SSB/FM /CW 25W PSU	1,090.00	10.00
IC275H	2M Transceiver, SSB/FM/CW 12V	1,060.00	10.00
IC-4SE	70CM FM Handportable inc Nicad/Charger	304.00	5.00
IC4SET	70CM FM Handportable, Keypad Entry, DTMF	316.00	5.00
ICW2E	2M/70M FM Handportable inc Nicad/Charger	395.00	5.00
IC-24ET	2M/70CM FM Handportable inc Nicad/Charger	385.00	5.00
IC-3220E	2M/70CM FM Mobile, 25W 40 Memo 12V	510.00	5.00
IC-2400E	2M/70CM FM Mobile, Dual Watch 45W/35W 40 Memo, 12V	649.00	5.00

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MFJ1274	Packet Radio Terminal	208.69	3.00
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MFJ16010	Random Wire Tuner	46.06	2.50
MFJ1701	6-way Antenna Switch	40.15	2.00
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MFJ202B	RF Noise Bridge	64.57	2.00
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MFJ250	1KW Dummy Load	57.43	3.50
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AT250	Automatic ATU for TS140S/440S Can also be used with other rigs	373.00	10.00
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PS31	Matching power supply for TS790	190.00	10.00
TR751E	2m multi mode mobile/fixed station transceiver 25W/5W	610.00	10.00
TM241E	NEW compact 2M mobile transceiver 50/10/5W	295.00	10.00
TM441E	NEW Compact 70CM Mobile transceiver 35/10/5W	325.00	10.00
TM702E	Compact 2m/70cm mobile transceiver 25W (VHF and UHF)	455.00	10.00
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TH26E	NEW 2M FM Handheld transceiver with PB10 battery	254.00	10.00
TH46E	NEW 70CM FM Handheld transceiver with PB10 battery	275.00	10.00
TH27E	NEW 2M Mini FM handheld transceiver, PB13 battery	254.00	10.00
TH47E	NEW 70CM Mini FM Handheld transceiver PB13 battery	275.00	10.00
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R2000	General coverage receiver with host of features	599.00	10.00
MC50	Deluxe dual impedance desk microphone 4 pin plug fitted	47.08	3.00
MC60A	Deluxe desk microphone with built in pre amp	90.00	3.00
MC80	Electret desk microphone with UP/DOWN facilities	55.15	3.00
MC85	Deluxe desk microphone with built in Audio Level Compensation	101.00	3.00
MC43S	Up/down hand microphone for TS930S etc	22.70	1.50



YAESU

FT1000	HF Transceiver General Coverage RX	3,060.00	—
FT990	HF Transceiver, General Cover Rx	1,849	—
FT767	HF Transceiver Expandable to VHF/UHF	1,633.00	—
FT747GX	Budget HF Transceiver	673.00	—
FT757GX	HF Transceiver	990.00	—
FP700	20A PSU	223.76	—
FC700	Manual ATU	152.23	3.00
FP757HD	Heavy Duty 20A PSU	264.37	—
FT290	2M Multimode 2.5W	438.00	—
FT690	6M Multimode 2.5W	438.00	—
FT290	70CM Multimode 2.5W	509.00	—
FT411	2M Handheld with Keyboard	229.00	—
FT811	70CM Handheld with Keyboard	244.00	—
FT470	2M/70CM Handheld	397.00	—
FT23R	2M Mini Handheld	213.00	—
FT73R	70CM Mini Handheld	233.00	—
FNB9	Nicad Battery Pack for FT23/73	35.15	2.00
FRG9600M	60-950MHz Scanning Receiver	520.00	—
FRG8800	HF Receiver	663.00	—
FT736	2M/70CM 25W Multimode Base Station	1,388.54	—
FL3035	25W Linear for FT290	117.50	3.00

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A LETTER HAS been received from VK3MI with an apology saying that he is receiving a lot of QSLs for contacts he is supposed to have had in early July 1990 with UK stations on 14MHz CW. Unfortunately the person responsible was not VK3MI and was probably located much nearer to Europe.

John, G3HCT, tells me that propagation indices can be obtained at any time by calling WWV on +1 (for USA) 363 297 3235. They give the solar flux, A and K indices, and a propagation forecast for the next 24h.

Sad news for those who knew Dave Porter, ZD8DX. He sustained serious back injuries some weeks ago and has since died. He must have given many their first contact with Ascension Is.

72 FROM RUSSIA

ANGUS, G8PG, has sent along the following which is believed to be the first operating code to be introduced for specific use by QRP operators. He writes "Some months ago the U QRP Club suggested to the G QRP Club that a new operating code - namely "72" - meaning "wishing you good QRP" should be adopted by QRP operators. The G QRP Club organised a worldwide poll of major QRP clubs to ascertain their views on the subject. The result was a unanimous vote to accept 72 as a new operating signal. It will now be brought into general use by the low-power fraternity, so if you hear a station sending "72 es 73" you know now what it means. The fact that this suggestion came from our Russian friends is particularly pleasing, as it is a sign of their ever increasing integration into the world-wide network of QRP operation.

CONTESTS

CONGRATULATIONS to G4PIQ who headed the UK entry in the 1991 Bermuda Amateur Radio Contest and will therefore be travelling to Bermuda to collect

his trophy at the RSB annual banquet in October. There were 14 British entries whose scores were as follows : G4PIQ (884,400), G4CNY (820,160), GU4IUW (564,185), G4SZD (398,800), G0CCH (132,600), G0HAS (91,460), GD4HOO (70,760), G4MKT (50,255), G4SDJ (28,350), G0MMI (23,625), G0NYL (22,980), GM3BCL (12,420), G4OYY (12,240), and G4MGZ (800). As a matter of interest other top scores were - Germany Y33UL with 190,050 points, US WB2YQH with 294,295, and Canada VE3RM with 174,995. The organisers are worried by the low level of interest which they believe the contest attracts and are seeking your views - if you have any please write to Edward O'Brien, VP9LO, President, Radio Society of Bermuda, PO Box HM 275, Hamilton, Bermuda. The next contest will take place on 21 and 22 March 1992. Modified rules will be given nearer the time.

VK-ZL-OCEANIA CONTEST

1000 5 October - 1000 6 October (CW)

1000 12 October - 1000 13 October (SSB)

ALL BANDS (except WARC). One QSO per band with stations in VL, ZL, or Oceania which each count two points. Final score is total QSO points multiplied by the total of VK/ZL/Oceania prefixes worked on all bands added together. Exchange consists of RS/T plus serial QSO number beginning from 001. Separate logs for each band and indicate each new prefix worked. Logs must reach Frank Beech, VK7BC, 37 Nobelius Drive, Legana, Tasmania, Australia 7277, no later than 25 January 1992. I can supply photocopies of the rules (SASE please).



Colin Sykes, G3XJZ, with his very impressive HF set-up.

XIV CONCURSO IBEROAMERICANO

2000 5 October - 2000 6 October

SSB ON 1.8 to 28MHz (no WARC bands) observing IARU recommended band-segments. Exchange RS plus serial QSO number from 001. Three points for QSOs with Latin American stations, one with others. Latin Americans for this purpose include CE, CO, CP, CR, CT, CX, C3, C9, DU, EA, HC, HI, HK, HP, HR, HT, KP4, LU, OA, PY, TG, TI, XE, YS, YV, ZP, 3C, and their DXCC dependencies. Final score is total QSO points times sum of multipliers from all bands. Logs must be sent before 30 November to Concurso Iberoamericano, Gran Via de les Corts Catalanes 594, 08007 Barcelona, Spain. I can supply copies of rules (SASE please).

LZ DX CONTEST

0000 - 2400 1 September

CW ONLY. 3.5 to 28MHz (no WARC bands) in IARU Region 1 designated segments. Exchange RST and ITU zone (UK is 27). I can supply copies of rules (SASE please). If you chase awards you can apply for the BFRA awards NRB, W-100-LZ, 5 Band LZ, W-28-Z, Black Sea, and Sofia using a submitted log instead of making a separate claim if your log contains evidence of the relevant contacts.

EUROPEAN DX CONTEST

1200 7 September to 2400 8 September (SSB)

RULES FOR THE CW section of this one were given in last month's column. However, if you would like a copy of the official handout please send me a SASE.

AGCW HTP 40

1300 - 1600 7 September

CONFINED TO 7MHz CW using straight keys only. Logs to be sent to F W Fabri, DF1OY, Wolkerweg 11, D-W-8000 Munchen 70, Germany. SASE for rules please.

SCANDINAVIAN ACTIVITY CONTEST

1500 21 September - 1800 22 September (CW)

1500 28 September - 1800 29 September (SSB)

THESE CONTESTS cover 3.5 to 28MHz (no WARC bands) and the object is to work stations in Scandinavia only. I can supply copies of the 1990 rules but there may have been changes.

QSL ROUTES

I HAVE received a copy of this new publication, compiled by Y41VM and Y58ZA. It contains lists of 38,000 QSL managers, 4,000 QSL managers' addresses, and a section on 40 "top managers" and lists of the stations for whom they act. This pretty comprehensive guide consists of 234 pages in A5 size and costs US\$ 15.00. Copies are obtainable from Theuberger Verlag Berlin GmbH, Oberwasserstrasse 11/12, D-O-1080 Berlin, Germany.

DX NEWS

IT SEEMS THAT VK9 stations are once more being issued with call signs according to the island on which they are located. Thus VK9C = Cocos-Keeling Is, VK9M = Mellish Reef, VK9N = Norfolk Is, VK9W = Willis Is, and VK9X = Christmas Is. The *Long Island DX Bulletin* says that C21NI, in Nauru usually appears near 10.105MHz at 1030 and will arrange schedules on other bands.

The DX Advisory Committee of the ARRL has voted unanimously to recommend that North Korea be added to the DXCC countries list. The new prefix block E2A - E2Z has been allocated to Thailand. Novice stations in Sri Lanka are now being given the 4S6 prefix - they are allowed to operate on CW between 3.5 - 3.6, 21.125 - 21.200, and 28.000 - 28.500MHz.

Stations in Botswana will be celebrating their country's 25th independence anniversary during September and October by using the A25 prefix. The four currently licensed Botswanan novice stations will use A26.

T5RR is active again from

continued on page 17

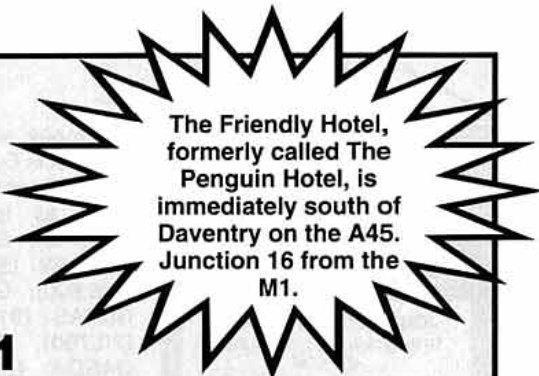


Radio Society of Great Britain

HF Convention

28 and 29 September 1991

Friendly Hotel, Daventry, Northants



The Friendly Hotel, formerly called The Penguin Hotel, is immediately south of Daventry on the A45. Junction 16 from the M1.

Programme

(SUBJECT TO CHANGE WITHOUT NOTICE)

Saturday 28 September

BOOK IN ADVANCE

- 12.00 } Visits to BT Radio Station, Rugby*
- 13.30 }
- 15.00 }

- 19.30 DX Dinner, Speaker John Forward, G3HTA. Tickets £18**
Followed by informal slide show and presentations

Sunday 29 September

ADMISSION £4

(DOORS OPEN AT 9.30 AM)

- Marti Laine, OH2BH Where do we go next?
- Peter Hart, G3SJJ High quality transceivers
- Al Slater, G3FXB Contesting
- Roger Western, G3SXW Pile up operating
- John Allen, DTI, Baldock What's on 80m tonight?
- Roger Balister, G3KMA Islands On The Air Award
- John Clayton, G4PDQ (with W6GO/W6HHD) DX Packet Cluster

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* Booking for BT Radio Station Visits and General Information:

** Dinner Tickets (cheques payable to R C Whelan):

Bob Whelan G3PJT 36 Green End, Comberton, Cambridge CB3 7DY. Tel: 0223-263137.

Hotel bookings direct to Friendly Hotel. Tel: 0327-77333, quoting HF Convention.

Lunches available or bring your own sandwiches.

HF NEWS

continued from page 15

Somalia and has been worked on 14MHz SSB. According to *DXpress*, 5R8AL will be back in **Madagascar** this month. TL8MB, in the **Central African Republic** often appears on 18.069MHz around 1730 and will make skeds on other bands.

FR5ZU is expected to be FR5ZUI/G from **Glorioso Is** this month before going on to **Tromelin Is** in October, and to **Juan de Nova Is** in November. FR5AI should be on Juan de Nova Is in October.

RSGB DX News Sheet says that KA3DBN will be in Africa for the whole of this month and hopes to be on the air as ZS6JR and KA3DBN/ZS1 and later from **Botswana, Lesotho, Swaziland and Mozambique** if a licence can be obtained. QSLs should go to his home QTH (see under VP2EBN in *QTH Corner*).

The UR prefix will in future be used for stations in the Ukraine, and ES will be used as a primary prefix for Estonia.

DXPEDITIONS

K1RH HOPES to be on from **St Pierre & Miquelon Is** early this month. He expects to have the callsign FP9SPM (the first time this prefix will have been used) and will have other operators with him. FP5DX has probably left the islands by now and returned to France.

Rumours at the time of writing suggest that the projected visit to **Myanmar** by Romeo Stepananko may take place this month. A group of Romanians was planning to climb in the Himalayas and their schedule means that there is a possibility of some operation from **Bhutan** at the end of this month, and from **Tibet** in the first half of October.

The expedition to the **South Sandwich Is** which was planned to take place last winter seems to be being re-scheduled to take place from 6 to 20 December. A team of eight operators will be on Thule Is. (Having said this, it is rumoured elsewhere that the expedition may take place earlier). Donations are still being solicited by AA6BB.

JA2NQG, JH2BNL, and JI2UAY will appear as KC6CW, KC6DX, and KC6MZ respectively from **Belau Is** from 8 to 12 September. They will be on all bands 1.8 to 50MHz on CW, SSB, RTTY, and FM.

According to *DXpress*, 3B8CF is preparing an operation from **St Brandon**. This will be an all-bands affair with SSB and CW covering the WARC bands too. No dates fixed but probably this year. The same newsletter says that UA3DK is planning a new operation from **Spraty Is** sometime before the end of 1991.

From 2 to 9 October a group of Dutch amateurs will be visiting Luxembourg. They will use their own callsigns preceded by LX/ and will be on all bands from 1.8 to 28MHz, SSB, CW, RTTY, and packet. If you have three QSOs with them you can apply for the 'DAGOE Award' by sending your QSLs to the DAGOE Foundation, PO Box 356, Dordrecht, Netherlands (NB - there is no charge).

RSGB DX News Sheet reports on a rumoured expedition to **Albania**. According to information received two Hungarian amateurs would be there for four or five weeks commencing 2 August. This should cause quite a flutter on the bands and if you need Albania their signals should not be hard to find!

UA9's XC, XLN, XBE, XLZ will be on from **Vaygach Is** until 2 September. This is in Oblast 114 and is IOTA EU-86. They will use their own calls with the 4K3 prefix on CW and SSB on all bands 3.5 to 28MHz. Afterwards they will go to Amderma as UV1P/UA9XC, RZ1P/UA9XLN, RV1P/UA9XBE, and RW1P/UA9XLZ. Any contacts with this group will count for the 'RAEM Award'.

AWARDS

3A CW AWARD

ISSUED BY the 3A-CW Group for CW contacts (or confirmed reports) with stations in Monaco since January 1981. Each counts one point and repeat contacts with the same station may be made on different bands. There are three classes - (for Europe) Basic (four points), First Class (eight points), and Excellence (12 points). Stations outside Europe need half these points. 3A0CW, 3A2ARM, 3A200SM, 3A7A, 3A8A, 3A9A, and 3A7JO count as 'jokers' which count two points but can only be worked once. Send log entries certified by "an official country CW club" plus 20 IRCS or US \$8.00 to Claude Passet, 7 rue de la Turbie, MC 98000 Monaco.

THANKS

THANKS GO to *DXpress* (PA3DZN), the *Heard Is DX Bulletin* (VK9NS), *DX-NL* (DL3RK),

BAND REPORTS

A lot of complaints about disappointing conditions this month. G3KSH has found the DK0WCY beacon on 10MHz very useful during disturbed periods and recommends listening to the whole of its transmission - not just the callsign. This month I have to thank G2HKU, GM3CSM, G3GVV, G3KSH, G4DXW, GW4KGR, G4s MUW, NXG/M, G0s JZA, KDS, LRX, and the UK Packet Cluster (via G4PDQ). Calls in italics were stations on CW.

14MHz
0600 D2ACA, FK0BK, FO4DL, KL7, KH6IJ, P29DX, VK9ND, 3D2AG
0700 *FK8FS, KE2AA/KH3, VK9NS, VR6KY*
0800 HL9HH, VR6TC, VR6YL, *ZK1CQ, 9K2HA*
1100 EJ7FRL, VY2TD, 3A2LZ, 4K5ZI
1400 *4K1A*
1500 AP5HQ, JT1CS, VU2NI, 9M8FH
1600 V3AO, 4S7VK
1800 ST0DX, V51/7Q7JA, ZD9BV
1900 C9RTC, JA, T5RR, T6AS, TU2XB, VQ9IO, Y11BGD, 3X1AU, 5Z4BP, 8Q7PJ
2000 A71BK, BV2CI, BY5RY, *FH5EJ, V85IR, XU1NQ, ZD7XW, 3D2CA, 7Q7JH*
2100 *HL9HH, JA, JY9SR, ST0DX, TT8SA, V63WP, VK5, 9M8PV*
2200 *EP2ASZ, HS0AC, S79KMB, SU1DZ, TL8FD, 4K5ZI, 8Q7P*
2300 HC8GR, T6AS, V85IR

18MHz
0800 VK7GK
1100 VS6BD
1900 HF0POL, PZ1AP, UM8MBA, VP8CBL, ZD8LII, ZP6DW
2000 A22AA, J37AJ, JY9SR, PJ8AD, XT2BW, 4K2BOU
2100 HZ1HZ, JA, 7Q7JH, 9L1US
2200 CE3OXZ, DU4DX, H8A, VP2EE, ZC4TJ
2300 OA4US, T15GLF, 4S7EA

21MHz
0700 FO5FO, HL9TK, JT1BG, 4K4/JA0KBZ
0800 AH6HB, D68JM, VU2DPG, *3W4DK*
0900 BY5RA, FO5CS, KH3AE, TT8SA
1000 A35KB, 5W1IU
1100 FK8CP, VP2EY, 5W1JA
1300 T6AS, VP2MAO
1400 *FR5FA, TY2AB, 9M8s FH, LL, 3B8FK, 3B9FB*
1500 *FH5EJ, HF0POL, T5RR, TT8SA, 9V1YC*
1600 BV3AI, BV4AS, *D2ACA, HS0AC, P29DX, TA9/F1LXZ, TZ6VV, VQ9RS, 5B9A, 9V1US*
1700 VQ9RR, VS6CT, 5R8JD
1800 A92EV, SV2ASP/A, YB8NA, 3X1AU, 7Q7RM, 9L3BM, 9U5BZP, 9M8MK
1900 A22AA, BV4CG, BY5SY, HS1BV, PY0FF, 3B9FR, 7Q7JH
2000 A71BP, HL, JA, S01A, TR8RLA, *XU1NQ, 5Z4FN*
2100 T100SUN, V31PC, ZF2QJ, 9M8ZZ
2200 *TL8FD, VP2EI, VQ9RR*

28MHz
0800 T5RR, VQ9IO, *XU1NQ, 4K5ZI, ZS6AIS/7P8*
0900 1AP2AC, BZ4RBX, TR8XX, V51P, VK6BA, 5T5HH, 9U5BZP
1000 FR5ZA, 3B8FU, 3W4DK, 9L1US
1100 TR0D, VU2KFC, 7Q7LA, 9K2SH
1300 A22AA, JY5FA, VQ9IO, ZD8WD, 7Q7JH
1400 BY7QH, V51SW, ZS9A, 3DA0BK
1600 VP8AWU, 3B8DB, 5R8JD
1700 WP4KAG, V51P, Z21DL, 6V1A
1900 S79KMB, WP4EPC, 5N9BHA

QTH CORNER

GW3INW/HK3 via RSGB or A Davies, A. 93780 Bogota, Colombia.
T6AS IT9AZS, Dr Salvatore Alescio, Corso La Masa 67, I-90010 Trabia (PA), Italy.
VP2EBN KA3DBN, 2703 Bartlett Lane, Bowie, MD 20715, USA.
VR6YL via WD6GUD, George Stevens, 11130 Dempsey Av, Granada Hills, CA 91344, USA.
XU1NQ via OK1NQ, Josef Kordac, Liunskych 3 888, CS-14000 Prague 4, Czechoslovakia.
4K3/UA9XC etc PO Box 1247, 167001 Syktyvkar, USSR.
8Q7PJ PA0CRA, Fagelin 1, NL-3445 EZ Woerden, Netherlands.

1991 28MHz COUNTRIES TABLE

G0JZA	190	G4YNG	72
G0DOO	187	G2FOR	63
G0AEV	166	G4NXG/M	62
G4DXW	159	GM0GEI	55
G0KDS	146	G0DUS/M	54
G4MUW	133 (SSB)	G4XAH	43 (RTTY)
LA0GC	113	G2AKK	31 (CW)
GM4CHX	81		

the *Ex-G Radio Club Bulletin* (WA8TGA), the *Long Island DX Bulletin* (W2IYX), the *RSGB DX News Sheet* (G4DYO), and the *Lynx DX Group Bulletin* (EA2KL). To be included in the **November** column everything to reach me no later than **18 September**.



THE LAST year when there was so little Sporadic-E propagation on 144MHz was 1979, when there were two openings in May and one in June. But although well passed the sunspot peak, the sun continues to be very active geomagnetically, producing many significant flares. These were the root cause of two more big auras in July, so the DX-chasers were able to work many countries that are more usually contacted via Es.

BEACON NEWS

THE MID-CORNWALL Beacon and Repeater Group's beacons were due to change to their new callsign, GB3MCB, on 28 July, but the 144MHz one was still signing GB3CTC that evening. Secretary TJ Cooper, G4XOP, wrote that the group, which runs five beacons, is planning to build new equipment, so would welcome donations. These can be sent to either G4XOP or G4WVD, who are both QTHR.

REPEATERS

THE AYLESBURY VALE Repeater Group has 158 members according to its July *Newsletter*. Its two repeaters, GB3VA (R4) and GB3AV (RB2), have been operating faultlessly. For details of membership contact the AVRG Secretary G8BQH, who is QTHR.

Talkthrough is the newsletter of the UK FM Group (Western) and the Summer 1991 edition is the first issue for a year. The group manages four VHF, nine UHF and two microwave relays, so the proposed RSGB levy of £25 plus VAT per repeater will doubtless be a major topic for discussion at the AGM on 16 September. For membership details write to G4WSS at PO Box 3600, Altrincham, Cheshire, WA15 9LU.

BAND PLANNING

THE ITEM ABOUT proposed additional packet radio frequencies in the 144MHz band in the August *VHF/UHF News* brought a letter from Reg Belshaw,

G3UTS (DHM). He strongly opposes the suggestion that 144.475MHz be designated for AFSK packet radio, pointing out that a lot of SSB MS skeds are deliberately arranged in this part of the band to avoid the main area of SSB activity.

If you have any comments on this important topic - see pages 7 and 19 in the August *RadCom* for full details - please write immediately to either Peter Burden, G3UBX, chairman of the VHF Committee, or to me, so that we can consider your views during our meeting on 14 September.

NOVICE NOTES

THE FIRST NOVICE licences having been issued, we can expect to hear new prefixes in some of the VHF/UHF bands. On 6m, only data transmission is allowed in the 50.620-50.760MHz section, but Morse, telephony and data in the 51.250-51.750MHz part. On 70cm, Morse, telephony and data are the permitted modes in the 433.000-435.000MHz section. Licensees have all-mode access to the entire 23cm band, but no permission to use 70 or 144MHz.

All novice callsigns begin with the figure 2 - see page 25 of the March issue of *RadCom* for full details. The maximum power is 5W DC input, 3W RF output. The final draft text of the Amateur Radio (Novice) Licence (A) and (B), to use the official title, was published in the June 1990 issue of *RadCom*.

DX NOTES

JOHN HUNTER, G3IMV (BKS), reported that PA3BZL and PA3FOC will be QRV on 144MHz from Ischia Island (JN60) 9-20 Sept. Their equipment will comprise a Ten-Tec Paragon HF transceiver, transverter, 3CX800 PA and 17-ele Yagi with MGF1302 masthead preamp. Tropo QRGs are 144.045 and 144.225MHz; MS skeds 144.115 and 144.215MHz, random CW MS on 144.125MHz. No prearranged skeds but they will be QRV on 14.345MHz daily at 1600. No calling on sked QRGs. Callsigns should be IC8/own call.

Another group of Dutch amateurs, members of the DAGOE Foundation, plan to operate from Luxembourg, 2-9 October. They will be QRV on 144MHz CW, phone, RTTY and packet radio. No frequencies, times or equipment details were given, but calls will be LX/own call. An award is offered for contacting at least three, different LX/PA stations or

making three QSOs with a single one. Apply to PO Box 356, NL-3300 AJ Dordrecht, Netherlands; no money or IRCs necessary but QSLs required.

INTERFERENCE

FOLLOWING THE comments on page 17 of the July *RadCom*, a reader has sent a copy of the RA's leaflet *Low Power Devices Information Sheet* which lists the many low power devices that are now exempted from licensing, together with the bands in which they are permitted. These include telemetry, telecommand, alarm, model control, etc.

To quote from the leaflet, RA 114: "The 49.82-49.98MHz band is intended for a very wide range of general purpose use, such as toy model control, baby and car alarms, walkie-talkies, etc. The current performance specification is MPT 1336." The maximum ERP is 10mW. Copies of RA 114 and MPT 1336 can be obtained from: The Information and Library Service, Radiocommunications Agency, Room 605, Waterloo Bridge House, Waterloo Road, London, SE1 8UA.

RA 114 mentions illegal devices on the UK market which do not conform to MPT 1336. They are cordless phone base stations on the low end of 49MHz, the associated handsets often using our 70MHz band. Complaints of interference from these should be sent to your local RIS office, the addresses of which are in the current *RSGB Amateur Radio Call Book*.

Al Harvey, GU7DHI (GUR), had problems with a close neighbour who uses a 'Tomy Walkabout' baby alarm. He receives it on 51.035MHz and elsewhere in the band. After a lot of haggling with the shop which sold the alarm, he was given a UK telephone number for technical queries and learned that they use 49.875 and 49.902MHz. The two-way interference was largely overcome after Al re-sited his antenna.

Mr G Pollitt, G4NPQ (YSN), reported receiving FM telephone conversations on 144.23MHz which he traced to a nearby cordless telephone. The owner became very aggressive when he used a 2m handheld to demonstrate the phenomenon, so with hindsight, G4NPQ thinks it was a mistake to tackle the problem that way. The unspecified model was bought from a well-known, nationwide chain store.

Most users do not appreciate that 'wireless' baby alarms and cordless telephones are radio

transmitters and what they say could be broadcast over some considerable distance. Obviously one has to be very diplomatic when dealing with these kinds of interference. For example, it would be unwise to infer you have been deliberately listening into, let alone recording, intimate family conversations.

MOONBOUNCE

THERE IS NOT much EME activity to report this month so here are the Moon data for September. 31 Aug/1 Sept is a day sked weekend. For a London QTH, moonrise on the Friday night is about 2030UTC at an azimuth of 59° with moonset on Saturday morning about 1220 at 304°. The next moonrise is at 2100 at 53° with setting around 1335 at 309°. Moonrise on 1 Sept is at 2145 at 49°.

The declination at 0000 on 31 Aug is 20.6° and at 2400 on 1 Sept it is 25.2°. For about 75min from moonrise there is an Asian window and from about two hours before moonset a North American one; in between these times, when the Moon is high in the sky, only European stations will be workable.

New Moon is on 8 Sept so the 7/8 Sept weekend will be marred by Sun noise. During the following two weekends the Moon will be in the south. 28/29 September will be another good, near-perigee weekend, similar to 31 Aug/1 Sept.

50MHZ

The following items were taken from Ted Collins', G4UPS (DVN), *6M Information* pages for July. The 9H1SIX beacon is now running on 50.0245MHz with 10W to a ground plane antenna. During an opening to Brazil on the 10th, several Gs copied beacon PY2AA on 50.060MHz using FSK, and PY1AA, probably using A1A keying, on the same frequency. Is this a time-share operation?

EA4CGN telephoned G4UPS about a meeting with Spanish PTT officials on 16 July. Joe reported that an official announcement in September would give details of 50MHz operation. In summary, only Class A licensees will be invited to apply for permits for one year duration on a secondary, non-interference basis. Suggested band 50.000-50.200MHz, CW and SSB only, 30W ERP. No beacons but the unofficial EA3VHF on 50.070MHz will probably continue. About 100 licences could be issued before the year end.

OK3CM suggests that it might not be too long before some Czechoslovakian stations are issued with 50MHz permits, following discussions with the PTT. There is a similar chance that Polish amateurs might gain access to the band by about the same time.

Ted is the QSL manager for A45ZN who reported that talks are still going on with the authorities to try to get 50MHz permits for operators in Oman and for a beacon. Tony has been operational from a yacht in the Arabian Sea and worked into DL, ON and PA on 16 June using his other call ZS1D/MM.

ACTIVITY

While Es propagation was lacking on 144MHz in July, it was almost a daily occurrence on this band, up to the 22nd. Longer distances seem to be workable on this mode on 50MHz than on 144MHz; for example, Ela Martyr, G6HKM (ESX), contacted 5B4JE on 29 June for a new country.

Several readers submitted extensive lists of DX worked from Scandinavia, through central Europe and the Balkans, down to the Mediterranean including Gibraltar. Some new Italian squares were activated by people on holiday in various Italian districts. G4UPS reported a major opening to Scandinavia on the 20th, 2300-0100 - very late.

There were significant auroras on 9 and 13 July. The first one started at about 1400 and produced many QSOs with DL, G, GD, GI, GW, LA, ON, PA and SM stations up to about 1530, with some more in the mid-evening. The second event was a major affair which started about 1400 and faded by 1800. It yielded QSOs with DL, EI, F, G, GD, GI, GJ, GM, GU, GW, ON, PA and SM stations.

An opening between the Mediterranean and North America occurred on the 7th when 9Hs worked into W1 and VE1. On 10 July, PY5CC (GG54) was worked by a few readers around 2015. On the 15th Paul Baker, GW6VZW (GWT), heard KH4S at 1715 and 9J2HN shortly afterwards. G4UPS heard 7Q7RM on 50.110MHz at 1712 on the 21st; he was RST599.

70MHZ

GARY PARKHURST, G3TOZ (NOR), reported Es most days from 7 July. On the 22nd he worked ZBOW at 1455 on 70.20MHz, using just 400mW to a 3-ele Yagi at 15ft AGL; he got

Callsign	50MHz		70MHz		144MHz		430MHz		1.3GHz		Total Points
	Cty	Ctr	Cty	Ctr	Cty	Ctr	Cty	Ctr	Cty	Ctr	
G6HKM	62	45	-	-	72	16	30	7	31	6	269
G4FCD	9	11	-	-	79	13	42	10	26	4	194
G0NFH	39	9	17	2	29	2	27	3	6	2	136
G4LDR	23	9	8	2	43	11	32	3	-	-	131
GW6VZW	75	51	-	-	-	-	-	-	-	-	126
G0EHV	-	-	25	5	48	9	28	9	-	-	124
G0FYD	9	21	-	-	62	22	3	1	-	-	118
G8XTJ	28	20	-	-	46	10	-	-	-	-	104
G8ESB	4	2	13	3	36	6	25	6	4	2	101
G8PYP	15	32	1	1	24	11	8	4	-	-	96
GI4OWA	11	28	-	-	38	14	-	-	-	-	91
G3FPK	-	-	-	-	66	19	-	-	-	-	85
G4OUT	-	-	25	6	33	9	-	-	-	-	73
G3FIJ	-	-	-	-	39	10	7	2	-	-	58
G7CLY	-	-	-	-	32	6	-	-	-	-	38
GW7EVG	-	-	-	-	17	5	-	-	-	-	22

British counties are those listed on page 64 in the January 1991 *RadCom*, but excluding HBN; 77 in all. Up to three different stations allowed in all 12 GM regions. Do not include EI counties. Countries are the usual DXCC ones plus IT9.

an RS31 report. Ian Cornes, G4OUT (SFD), worked into EI, GD, GM and GW on 6 July in VHF NFD and added ten more 1991 counties.

144MHZ

THE MAIN EVENTS in July were the two major auroras. The first, on the 9th, was a 27-days repeat of the 12 June one. In a QSO with LA1K (JP53) on the 20m VHF net at 1147, operator Mange relayed the strong auroral signal he was getting from SK4MPI. My first QSO was at 1342 with OZ1BVW at QTE 30°. Best CW DX were SPs 4MPB (KO03), 5EFO (KO02) and 9EWU (JO90) at 35-40° in the mid-afternoon period.

This was an unusual aurora since, between 1800 and 2000, reflections were from the west at 270-290°. Only local British Isles and near-continentals were heard in this phase.

The second event on the 13th was every bit as good as the memorable one on 5 June. It started around 1300 and became a very southerly affair. Lyn Leach, GW8JLY (GNS), worked eight EA1s on SSB, some of them being up to S9. Mark Holloway, G4YRY (DOR), worked EA1WY (IN73) at 1642 for his first Spaniard via aurora. Does anyone know if EAs have been worked via aurora from the British Isles before?

G0CUZ's best DX was HG0HO (KN07) and Colin also contacted the Fastnet Rock station, EJ7FRL. The main event fizzled out around 1800 but at 2108 he worked DL1EJA (JO42) at 300°. In a further phase at 2336 he worked GM4AFF (IO87). The most southerly DX seems to have been IW0AKA (JN61), contacted on CW by GW4LXO.

Steve Crane, G0CUH, is now QRV from St Mary's (IOS/IN69QV). He found 40-60° the optimum QTE for this aurora. He worked EA1EBY in northern

Spain but couldn't penetrate the strong wall of Gs in IO91-93 to contact any deeper Euro-DX. G6HKM made 79 QSOs including HB9/HE7, F, one LX, Italians in JN35, 44, 45 and 55, and many DLs.

There have been a few fleeting Es openings. GW8JLY caught a two minutes one on 8 July when he worked 9H5L at 1132. At 1807 on the 12th, Lyn contacted IW8BZN (JN70), also worked by GW4HDF (IO81). Andy Steven, GM4IPK (SLD) had an auroral-E contact with LA6HL/TF (HP95) at 2215 on 8 July.

Some reasonable tropo propagation was reported in July. On the 4th, GW8JLY worked DL2LAX (JO43) at 2229, but heard no other DX. On the 10th, G0CUH, G0CUZ, G4YRY and GW8JLY worked into EA1 and EA2, squares IN63, 73, and 93. Richard Girling, G4FCD (OFE), has been back on the band since mid-April. On July 11 he worked FC1NZK (IN96) and EA2ARD (IN93).

There were more openings to SW France and northern Spain on 20, 22 and 23 to IN52, 63, 93 and JN03. GU6WDK/P was a welcome signal from Guernsey, worked by Terry Chaplin, G1UGH (SFK), at 2146 on the 22nd. Frank Howe, G3FIJ (ESX), enters the Annual Table and used NFD weekend to enhance his scores; he intends to get going again on 50, 70 and 1296MHz.

430MHZ

WELCOME TO ROB BRIGGS, G1GHA (SFD), who reported for the first time. He is "... irritated by the constant repetition of the self-perpetuating myth that 70cm is virtually dead. Nonsense!" he insists. He runs an FT-726R, 100W to a 21-ele Yagi at 40ft AGL with LDF4-50A feeder and a preamp. Rob reckons he can work into DL, F, ON and PA under flat conditions.

In NFD he manned the station at Thorpe Cloud, Dovedale (DYS), but suffered sun stroke so had to return home early but not before he had worked 60 stations, best DX being PE0MAR/P (JO21). Tropo conditions were good on the 22nd with HB9F copied at S4 at 1905.

G4FCD got going again in May and wrote that GD4s GCM/P and XUM/P were "fantastic signals" on this band and on 1.3GHz throughout NFD. G6HKM collected useful table points in the contest including a couple of GM regions. G0CUH should have put IOS on the map by now and Steve has ideas to assemble an EME station later "... if the XYL allows a QRO amplifier for the band."

1.3GHz

G1GHA (WMD) IS QRV on the band with his FT-726R and SSB Electronics transverter running 10W to a 23-ele Yagi at 30ft AGL. He operates from his parents' home in IO92CM - or ZM31d as he prefers - as he has severe TVI problems in Featherstone. He started on the band on 18 July and suggests anyone wanting a sked should telephone him on 0902 722830. He is QRV every Monday evening and at most weekends.

G6HKM concentrated on this band in NFD and says it restored her confidence. Ela made 31 QSOs in 14 squares, JO00 being new. She worked G0NFH (AVN) on the 15th and carried out SSB and FM tests with ON5NY on the 22nd. G4FCD started up at the end of June in time for NFD; Richard still needed Wales as of 20 July.

DEADLINES

THAT'S ALL for this month. Please send your **November** reports by **Thursday 26 September** and the **December** ones by **Thursday 24 October**.



SWL NEWS

BOB TREACHER BRS 32525
93 Elbank Road, Eltham, London
SE9 1QJ

IT APPEARS that HF conditions at the end of May/beginning of June were among the worst experienced for a long time. Listeners (and amateurs) can blame several sunspot regions which together produced an almost continuous stream of M-class flares.

These flares caused several short-lived shortwave blackouts on the sunlit side of the earth, and kept the geomagnetic field very active for days at a time. The polar paths that pass through polar latitudes were useless, and signals strengths on the other paths were low.

Thankfully, propagation improved through the rest of June and early July, although at the time of penning this piece, conditions were poor again. We will find out what has been on the HF bands later on, but first, it might be worthwhile looking at Solar Cycle 22.

It seems that come autumn 1992, the decay of Cycle 22 will commence. The DX type propagation we experience now will gradually decline for four or so years until the winter of 1996/97 at which time Cycle 23 will be born. It now seems most likely that, looking well forward, we will bring in the new century with the beginning of the peak in good propagation.

MORE ILA NEWS

THE LATEST *ILA News* hit the mat before the deadline. It seems as though the subscription increase did not go down too well in some quarters, resulting in a loss of some members.

Such a mood is always experienced in whatever society or organisation you belong to if the words "subscription increase" are mentioned. However, the subscription is still only £5 per year which really is peanuts when you consider the service which GW4OXB provides. The latest Newsletter provided the usual mix of interest ranging from HF DXing, Medium Wave DXing, news about the Marine bands and a piece on the Airbands.

CQ AWARDS

THIS IS THE third mention I have given to trying to attract British Listeners to support the Belgian SWLs who are trying to get *CQ Magazine* to open the doors for listeners to claim these prestigious awards. It doesn't matter if you are not a keen DX-hound or an awards chaser, I really do need some support from British listeners so that a 100% licensee domain is opened up to the listener. The American magazines are, dare I say it, considered to be 'anti-SWL' so anything which can be done to change their way of thinking towards the SWL has to be a plus. All you need to do is drop me a line saying you support the move to bring listeners into line with their amateur brothers in being able to claim listening achievement awards.

50MHZ AWARD

ALTHOUGH IT appears to me that the number of listeners who scan 50MHz for interesting DX can be counted on one hand, it is worth noting that the UK Six Metre Group has organised ten special plaques for proof of working/hearing 100 countries on the band. Eight plaques are available to the first eight Class A licensees to present proof of working 100 countries and their is one on offer to the first class B, too. However, the good news for listeners is that the group has organised one for the first SWL to show proof of hearing 100 countries. Of the 'regulars' there is some way to go, with heard totals ranging from 48 countries up to 77, but I should like to congratulate the Group for taking the time to spare a thought for the SWL, who we have shown do sometimes get forgotten.

HEARD ALL BRITAIN NEWS

AT THIS year's WAB Annual General Meeting, Dennis, GW6JNE, had the pleasure to present Awards to Ged Coker, Chris Gibbs, Frank Parkhurst and Anne Hague. Trophies were presented to listeners who won HAB contests this year, which is good news indeed, with listener activity in contests seemingly at an all time low.

Judging from the long list of recent certificate winners it would seem that the HAB movement is attracting listeners at a faster rate than ever before, not just here, but overseas as well. This can only be good for the listener

movement. If any SWL wants details of the HAB Award scheme, they should write with a large SASE to: Dennis Sartin GW6KMA, at 7 Penrhos Crescent, Rumney, Cardiff CF8 8PB.

ISLANDS ON THE AIR

ANOTHER AREA which is beginning to attract listeners' attention is the Islands On The Air Award scheme. Roger, G3KMA, is the Awards Manager and he has just issued a new 50 page Directory which is a must if you are collecting Islands for any of the awards. Any one listener who wants more information about the scheme should write to G3KMA at "La Quinta", Mimbridge, Chobham, Woking, Surrey, GU24 8AR enclosing a large SASE and a cheque for £5.

50MHZ

THE MAIN NEWS to report this month is of the superb conditions over the weekend of 15/16 June, when even your scribe caught eight new countries on the band.



An interesting QSL card from a Russian SWL who does all his listening from a boat in the Caspian Sea. Even more surprising was that the report was for a CW QSO. The receiver in use was a Wolna-K (whatever that is!) and the antenna a long wire.

The weekend got off to a very slow start, but at 1653 CN8ST was heard rag-chewing with G4UPS. Soon after, Tarik was involved in an immense contest-style '59, IM64' type operation to give as many people as possible their first contact with Morocco while conditions held. IK6HMG in JN72 was a good signal at 1724, and at 1740 EA6/DF5JJ was heard - a good one if the license was OK, (if permits had been issued). George, GD3AHV, was heard via backscatter working an ISO at 1842. The Sporadic-E propagation lasted until 2054 when FC1BLL in the South of France was heard.

On the Sunday, an early morning telephone call from David Whitaker, BRS25429, alerted me to good conditions to Austria, the

first YU - YU3EU, and YO2IS. A rare island for the IOTA chasers then showed in the shape of ID8/IK8MCK from Dino Island (EU144), but then, at 0900, the prize catch of HV3SJ, who had special permission to use 50MHz for a few hours that day. Amazingly, there was an Es opening in full swing for many to log a choice piece of DX on the band. The band still held surprises, and at 1321 SM1ALH on Gotland Is (JO97) was 59+. What else could happen? At 1333, EJ4VNX was 59+ from I043. After a good spell of SMs, including SM3BIU, an old 3.5MHz DX man from JP73, amazingly A22BW in Botswana was heard at 1507. More Scandinavians followed until at 1929, a phone call from Mick Toms, BRS31976, again alerted your scribe to an outstanding signal from OY9JD!. Anyone who says 50MHz is boring should have witnessed the amazing activity over that weekend.

Other openings came and went, mainly while Dave, Mick and myself were at work, but other notable scalps during the period in question included IK2GSO/IM0 (JM48), SV1OE (KM18), OH6MPC (KP12) at 0004 on 24 June, and OH2MZA/5 (KP41).

HF LOGGINGS

VERY FEW reports to take account of this month, but at least conditions seemed better than they were at the beginning of June. Some DX has been noted on the LF bands, but the best band was, once again, 21MHz. Quite a lot of IOTA activity was mentioned and the WARC bands continued to provide some interesting loggings without the QRM. To put some detail on these comments, we had CE0ZIS (Juan Fernandez) heard on 3.5MHz, while 9J2HN seems to have been the best on offer on 7MHz. 28MHz has been poor, as had 14MHz, but 21MHz provided AP2KAH, BY5TS, CE9GEW, D2ACA, HS0AC, KH3AE, HH2BN, TU2VM, VP2EY and XU1NQ.

FINALE

ONCE AGAIN, space has well and truly beaten me. Please, please send in your news. At the moment, it seems that everyone is relying on everyone else to provide it. There are many stories for the SWL and about listeners out there. How about letting this column into some of the secrets? Copy for the November issue should be with our scribe no later than Tuesday, 10 September.



THE SECOND RAE Novice exam is about to be faced by the next group of Novice students. The very best of luck to every one of you. Waiting for the result is harder than sitting the exam - ask the first group!

By now, also, the first morse tests are upon you. Again, I wish you luck. To anyone who is unfortunate enough to fail - in either field - you may not believe me at first, but the world does not stop. What you do is try again.

Perhaps you weren't quite ready, perhaps you were too nervous, perhaps it was just a bad day. The experience gained in the first exam should help you in the next. Whatever you do, don't give in, you'd miss far too much fun!

Just a thought. More novices, more contributions for this column? I'm trying to twist your arm!

A NOVICE NEWSWRITER

RICK SAT the NRAE in June. I shall not be able to report his success in this column due to holidays starting before the results are published, but I am sure he will be successful, and he is already deciding to put something into the hobby.

He has written to the others who took the exam with him, offering to be the East Kent Novice Newsletter writer, bringing news and views together for the first Novices there, and for those to follow in the months ahead.

I wish him great success and I am sure he will enjoy the role. Rick is thirteen years old so he has very many years ahead in amateur radio. He is making an excellent start! [His contributions to D-i-Y Radio would be welcome, too - Ed]

Anyone in the area with anything to say that could be of interest to young Novices, or indeed anyone likely to read Rick's newsletter, please get in touch with him, Richard Marks, 146 Ramsgate Road, BROAD-STAIRS, Kent CT10 2ER.

... AND A CLUB

THE SOUTH Dartmoor School Amateur Radio Club has been formed and will be active after the school Summer holidays. All eight members of the Committee are in the middle of the Novice training course.

Nine students and one teacher from the school and five more from Knowles Hill Comprehensive School will all be ready for the NRAE in September. They will be the first Devon exam takers and there should be Novice callsigns by the end of October. Support from parents, teachers and headteachers has been total and there are plans to put the whole project to good use.

Headmaster Ray Tarleton, Head of South Dartmoor school is keen enough to make a room available for a radio club and some funds for some equipment. So that the room can justify its existence, there will also be weather satellite facilities and then the Geography and Science departments can benefit too. Local radio amateurs will help and a club callsign is proposed. Summer holidays will be busy with final preparations for the exam and setting up the station ready for those first calls in September, and the Novice calls by the end of October

Thanks to Peter, G6ZKQ, for the information. I, and many others, wish you all the best of luck and hope to hear further news of the project. Like little Topsy, this can only grow, so Peter you will have a very busy time ahead.

Assuming 100% success, fifteen new Novices four times a year in one area alone, is a prospect I find rather exciting.

REAL NOVICE NEWS

TWO LETTERS have reached me from youngsters - apart from the one from Rick. One from ten-year-old Andrew in Peterborough asking for information on how to gain a Novice licence and one from Louise who sat the first NRAE in June.

I have sent the information to Andrew and asked for a progress report, and have replied to Louise, asking her to tell us more about herself. She says in her letter that she was very nervous, and gives a hearty "Thankyou" to her Granddad, Eric, G4MXS, who roused her interest, and to her teacher, Duncan, G3TLI.

This is really what this column is about - news from and for

Novices. Please keep them coming - I promise to answer all letters as soon as I can.

FROM LITTLE ACORNS GROW!

A PHONE CALL during our Novice class told us of successes in the June NRAE. Congratulations to all, and to the two dads awaiting the RAE results - I hope that you are equally successful.

A general invitation to take part in Thinking Day on The Air started it all, and Elizabeth was hooked. Husband Richard was to run a construction stand at the local primary school and Brownie daughter Rowena was to wave the magic soldering iron and build the prototype.

Tony, G6YTW, and Terry, G0LUQ, were most helpful, inspecting the potential radio station, and on hearing that Richard was considering the RAE, swept everyone, including Rowena, off to the first Spring lecture on 'propagation' at Harwell ARS. No escape now!

Details of the proposed TDOA station and the unveiling of Richard's prototype radio were highlights of the Christmas Dinner menu, with copies of the the phonetic alphabet being the take-

home presents. It paid off. GB4KGB was a great success. Seven year old Clare built a radio. Sarah, G0MSR, a Guide who had gained her licence at fourteen, was given pop-star treatment and a list compiled of those wanting to go for the Novice licence.

When Bob, G0KNJ, Senior Novice Instructor visited the station, he was surprised to find a class formed, a ready workshop, and eight pairs of eyes waiting for him to agree. What could he and Roy, G0KNV, do but say "Yes"? The course started in March. Another father, Mark, joined Richard on the RAE course, sitting the exam in May.

With Novice exam results out there are more plans to make. Licence applications to send, QSL cards to order, Morse to practise, shack organisation and a radio club to plan to encourage others. An added bit of excitement is for Natasha to collect her licence from the DTI on 25 July. Where will it all end? Not here for Elizabeth, she intends to sit the RAE in November.

Up and down the country similar stories can be told, the satisfaction and sense of achievement felt can only be guessed, but to all of you and those who follow, "Welcome".

NOVICE	RAE
1. Examined & identified components.	1. Didn't touch a single piece.
2. Understood resistor colour code. Worked out values of resistors.	2. Didn't see a single resistor.
3. Learnt how to use a soldering iron. Soldered two test sets, a piece of Veroboard, an audio amplifier and a simple radio.	3. Didn't touch a single tool and constructed nothing.
4. Used a multimeter (analogue & digital). Measured - Volt, Ohms, Amps. Calculated - Input power - Resistance of active component, eg, an LED.	4. Didn't touch a single piece of test equipment.
5. Practical application of: (a) Ohms Law, (b) Frequency and Wave-length (c), SWR, (d) Detecting Harmonics.	5. ditto
6. Used a receiver, got to know the controls, listened and filled in a log sheet. Set up a transceiver using dummy load.	6. Saw a transceiver but not allowed to touch. Heard nothing.
7. Fitted a PL259 plug, BNC plug and a 13 Amp plug.	7. No practical work.
8. Simulated QSO - Audio.	8. Theorised about QSOs.

Table 1: GW0ABL's comparison of the Novice and RAE training courses (see What's In a Name)

WHAT'S IN A NAME?

I HAVE HEARD many comments and discussions on the value - or otherwise - of the Novice licence. They have ranged from: "I think it's the best thing possible", to "But they won't be *proper* amateurs if they didn't take an exam like me". I would ask you to read **Table 1** carefully and then make further comment. It came to me from Dewi, GW0ABL, who has been licensed since the '70s, so is not a newcomer to the hobby and has obviously given the matter some thought.

Speaking personally, the Morse test itself was not difficult, but *using* the stuff frightened me to death. Why? Because I was totally unready to mix abbreviations, numbers and the conversational bits between. I know that that fear was shared by others. The Novice way seems a much more relaxed and pleasant way to become proficient. Back to the heading. Amateur? Novice? You choose.

SPECIAL EVENT HELP

SPECIAL EVENTS are often enthusiastically planned with volunteers aplenty for all sorts of jobs. When the day itself comes around for the big event, the number of bodies around is often less (occasionally many less) than expected or hoped. There may well be very good reasons why individuals cannot appear, but that does not make the prospect of running the station any easier with all the jobs to be done behind the scenes. And in front of them for that matter.

A visiting public needs information, possibly on the walls. Visitors need to be welcomed, the local press perhaps who *must* get the facts right, refreshments for the operators - a supply of coffee is always welcome and needed if the station is as successful as hoped. What else? Spare operators, loggers.... Ah! Loggers! They are often in short supply. But help is now possibly at hand.

What good listening practice it would be for student Novices to sit in on a Special Event station. Logging calls is part of the training, and this is a station where a greetings message could be sent by the trainee, and his or her own QSL card sent and received. Spare operators too can come from the same source. Fully fledged Novices can work any part of the amateur bands using



Pupils of Jurby Community School, Isle of Man, with Darryl Hall, GD4DEL at the microphone of GB2MSR.

higher power than their licence allows *under the direct supervision of a Class A licensee (or Class B above 50MHz)*.

Come to think of it, Novices and Novices-under-training could be a tremendous help in all similar cases. I am sure that they would help with other chores, (but not to be made 'dogsbodyes'), and would meet local amateurs who would in turn see that Novices were getting the sort of introduction that will stand them in good stead in later years. Now, isn't that a good idea?

A REMINDER IF NEEDED

I PROMISED to mention Jamboree On The Air (JOTA) well in advance for those intending to run such a station. Those who have run stations in the past will have their arrangements under control and those breaking new ground have had guidance, so this is just to jog memories if necessary depending on whether you are an amateur helping or a Scout Leader needing help. You are possibly both, in which case you are permitted to ignore the rest, as you have probably done all this many times.

The licence is arranged, the callsign for the station and the design for the special QSL cards decided and ordered. As September arrives, with about seven weeks to go, there are still things to do. Aerial requirements, electrical power, catering arrangements to discuss with the Scout group. Check on insurance arrangements for equipment, aerials, liability etc. If you do this for yourself, you know that it is done.

Send for the JOTA special callsign listing from the RSGB, (Self-Addressed Stamped Enve-

lope (SASE) please) so that the Scouts can check the other JOTA stations contacted during the event.

Among the Scouts who will visit the station, there will possibly be both Novices and budding Novices. Some may be already known to you, others not. Why not make use of them? They will probably be hoping that you will - they may already have read through this column and know they would be valuable as loggers. Given super-efficient loggers keeping an eye on logbooks there will be no incomplete reports sent in because "the operators took the logbooks away with them" They will also be able to help filling in QSL cards (including their own?) If you spend some time during September getting to know one another the event itself will be even more fun for all.

Local amateurs will be giving their time and possibly using their own equipment for the event. Novices, would-be Novices, Scouts, and anyone interested should locate these amateurs and offer their services in advance. That way lies new friendships and no-one turns those down.

JOTA will be held over the weekend 19 and 20 October. Where *has* this year gone?

MORE MANX ACTIVITY

JURBY COMMUNITY School held an indoor camp at Ardwhalin Outdoor Pursuit Centre at West Baldwin, Isle of Man, 24 - 28 June. Under the supervision of Head teacher, Mrs Carol Beck, and two other teachers, 17 pupils had an experience to remember. There were educational trips to the Manx Museum, Cregneash

Village Folk Museum, Laxey Wheel and mines, Langness and Peel. The children went to see stock car racing and Silverdale Glen plus a swimming trip to the Aquadrome in Douglas.

In case that was not enough excitement, Denys Hall, GD4OEL, the IOM Scout and Guide Adviser, set up a Special Event station with the callsign GB2MSR at Ardwallin. The children heard from Denys about amateur radio. How the station was set up, how the aerials worked, QSL cards, and how, through radio, friends could be made worldwide. This point was proved as the youngsters heard Denys contact many countries.

As Denys was also active at Ardwallin for the Guides' Thinking Day with the callsign GB4MGR, he certainly gives a lot of time, help and encouragement to youngsters in the IOM. Well done, Denys, your efforts could lead to many 2D callsigns in the future!

SCROOGE'S CORNER

REMEMBER THOSE 35mm film containers? Geoff, G4NPQ, finds that they make good coil formers. I'll give you his other tip next time - it's a beauty!

When building radio equipment - a kit perhaps - egg boxes make useful holders for smaller components, and the sort of cases which originally contained 'exceedingly nice' apple pies for larger ones. Riley, G7GOD, sent that one.



And from David, G7GPR. The magnet of an old loudspeaker holds those screws that would otherwise take a walk after removal, in the length of time it takes to blink. [It can also be useful to magnetise a small long-bladed screwdriver so that lost nuts and bolts can be retrieved from being dropped into the depths of a radio - Ed].

Those brass paper fasteners with legs and a head have been found another use by John, G3BDQ. Any insulating board with holes made in it will do. Push the fasteners through the holes and Hey Presto! you are in business. Soldering can be done on either side, but do work out the layout on paper first or you may have more holes than board. This idea was used successfully with ten and eleven-year-old boys.

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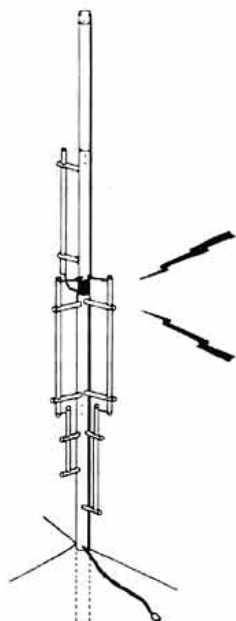
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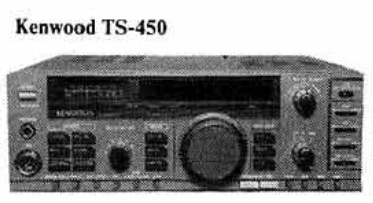
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TOPICS

PAT HAWKER G3VA

DIRECT-CONVERSION CW RECEIVER WITH SIMPLIFIED PHASING-TYPE DEMODULATOR

AS MENTIONED BRIEFLY in *77* (November 1990, p29), Tim Walford, G3PCJ, has been developing a phasing-type demodulator for use in a CW-only 7MHz direct-conversion transceiver taking advantage of the fact that the accurate quadrature (90°) phase difference needs to be maintained only over the relatively small AF bandwidth involved in CW reception through fairly sharp audio filtering.

His prototype transceiver (Fig 1) has its audio bandwidth restricted to about 800+/-300Hz and is based on the use of NE602 double-balanced mixers, BC109 band-pass AF filters centred on 734Hz, all-pass plus and minus 45° phase shifters using a TL072, sharper 734Hz audio filter (TL071) and audio amplifier (LM380). In effect, it requires an extra mixer, filters and audio-phase-shift networks compared to a conventional DC receiver, but reduces the unwanted audio-image sideband by -35dB (voltage). He writes:

"The receiver (Fig 2) uses NE602s (or 612s) whose oscillator section can be driven by an external signal from low-impedance RF phase shift networks to obtain +/- 45° phase shift relative to the local oscillator. I used a 3.5MHz VFO with doubler in order to improve stability but this is not essential for the phasing aspect of the receiver.

The incoming signals are fed to both 602 devices, in this case from the two windings on the output of the RF amplifier stage. Outputs from the 602s are filtered with a resonant load (0.1H and 470nF) and further filtered/buffered with a two-pole low-pass filter. These drive the op-amp all-pass phase-lead and phase-lag stages which provide the +/- 45° audio phase shifts required to obtain phase cancellation at the centre frequency of 734Hz.

"The two audio signals are 'added' (combined) at the input to

the final narrowband CW filter. The desired audio sideband is most easily selected by changing over one of the 602 outputs to its other output (the two outputs differ by 180°).

"The circuits are set up by tuning a steady signal to produce the undesired beat note at its loudest frequency (which should be about 734Hz) and then adjusting the RF phase-shift trimmer capacitor (65pF) and the audio-balance potentiometer (10k) for minimum signal.

"My measurements show the undesired audio sideband level to be at least 54 times down (-35dB voltage) over the whole audio band compared to the desired 734Hz sideband. While this is not as good as could be achieved by a more complex phasing-type or filter-type receiver it is very good for the small amount of extra circuitry involved. Digital RF phase shifters might be used for a multiband receiver but then the complexity approaches that of a filter rig and is much more complex than the two-capacitors, two-resistors used in this 7MHz receiver.

"At present I am working on a 3.5MHz CW phasing design with improved roll-off of the audio response (hence selectivity for a direct-conversion receiver), and with better strong signal performance by avoiding an RF amplifier stage and incorporating audio AGC. I hope to have this 3.5MHz design available in kit form in the region of £45."

ELECTROMAGNETIC FIELD EXPOSURE

THE PUBLIC IS STILL BEING confused by the wide difference of expert opinion on possible biological (athermal) effects of long-term exposure to electromagnetic fields. An article by Robert Pool in *Nature* (14 February 1991, p554) was headlined 'EMF - cancer link still murky' and pointed out that the mystery surrounding the claimed connection between EMFs and cancer was deepening as more epidemiological studies showed up such odd and inexplicable correlations between childhood leukaemia and black-and-white (but not colour) television and with hair-dryers but not other domestic appliances! One sometimes feels inclined to quote the old adages that statistics can prove anything and that there are 'lies, damned lies and statistics'.

Perhaps more relevant was a BBC Research Report last year (RD 1990/4 'Electro-

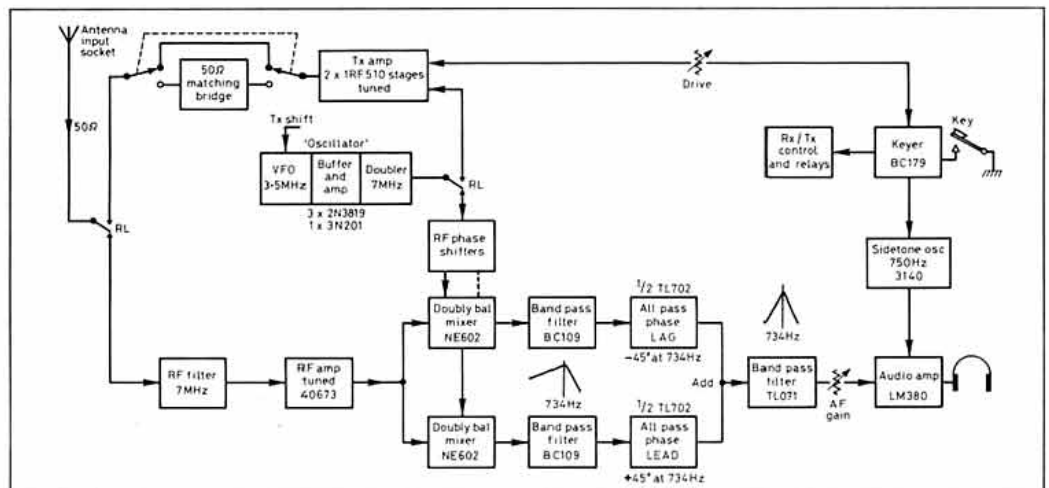


Fig 1: Block outline of G3PCJ's 7MHz CW transceiver incorporating a phasing-type direct-conversion receiver.

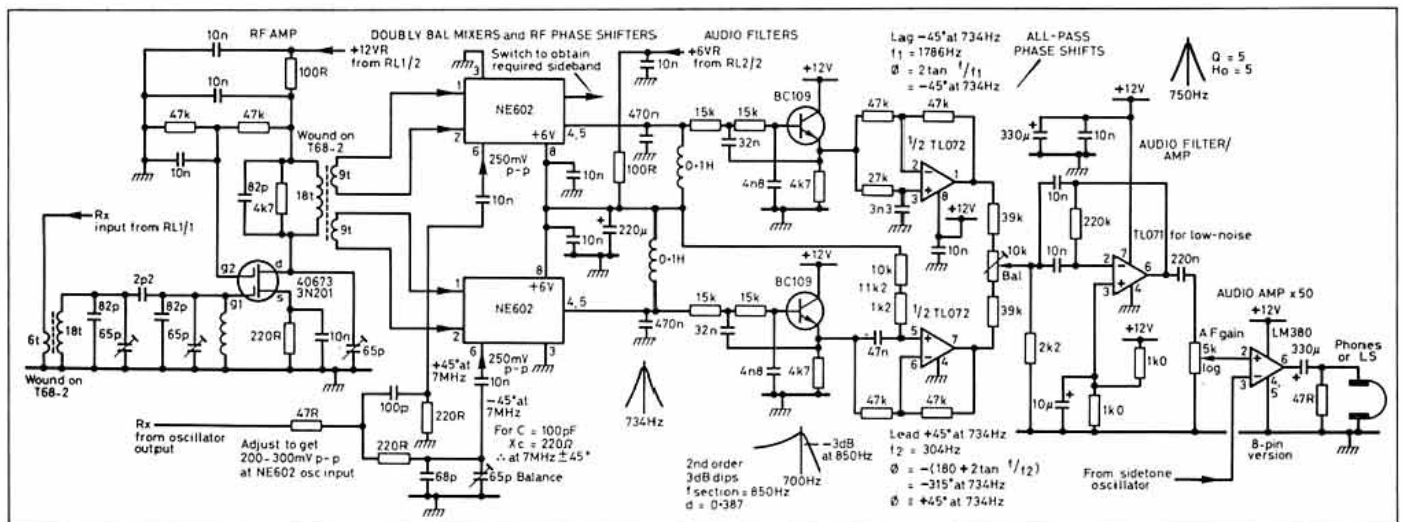


Fig 2: G3PCJ's 7MHz phasing-type receiver which reduces the unwanted audio-image sideband by a factor of 54 (-35dB voltage) measured overall. The 65pF balance trimmer for the NE602s and the 10k balance potentiometer at the output of the TL072 phase-shifters are adjusted for lowest level of the unwanted 734Hz sideband.

magnetic field exposure in broadcast environments' by S Wakeling). To quote from the introductory remarks: "Recently, there has been renewed concern at possible deleterious health effects from exposure to electromagnetic fields with international authorities recommending ever more stringent exposure levels . . . the areas around broadcast antennas to which a person can safely gain access are becoming increasingly restricted. Broadcasters face a variety of problems when trying to ensure safe operational practices in areas with significant levels of electromagnetic fields, such as exist close to transmitting antennas. The exposure guidelines have become more stringent each time they have been updated . . . international authorities are tending towards an 'as low as reasonably achievable' principle in the light of inconclusive biological evidence which will create more problems in future . . . Safety factors are being compounded by incorrect assumptions regarding exposure conditions. The derived field strengths of exposure standards are calculated assuming optimum coupling conditions and far-field, plane-wave exposures whereas, in broadcasting, the potential for hazard is generally confined to the near-field around the transmitting antennas and hence the derived field-strength values are inappropriate for determining true SAR (specific absorption rate) levels and hence the actual level of potential hazard."

SAR is the power (in watts) absorbed per

kilogram of tissue, and the BBC Report points out that the biological effect (heating) of a given SAR will depend on the thermoregulatory system of the animal being exposed; humans, it is pointed out, have a very efficient thermoregulatory system.

The Report covers such questions as RF shocks and burns, thermal effects, athermal effects, epidemiological studies etc. It notes that the cancer links have been found only in some studies; others have not found any significant correlation.

An American study, reported by F P Ziemba (*Nature*, 21 February 1991) into possible hazards from the electric and magnetic fields emanating from TV and VDU screens suggests that natural radioactivity (from radon gas) and high electrostatic fields are more likely than EMF to be the cause of various common complaints from computer operators. Radiation levels as high as 6000 alpha disintegrations per minute per 100cm² of viewing-screen area have been detected in computer displays and TV screens. He considers his measurements show that this phenomenon is caused by the electrostatic deposition of charged radon progeny onto the faces of viewing screens. Radon-22 gas is formed by the radioactive decay of naturally occurring uranium-238 and comes from the first metre of underlying soil and rock in many areas. This enters living areas by diffusion, convection and ventilation, with charged clusters of dust and aerosol particles attracted to

CRT displays by the electrostatic fields that build up on CRT screens, providing a pumping action that can continue even after the TV or VDU has been turned off. VDU colour monitors show the highest levels of activity.

EARTH LOOP FEEDBACK

AN ARTICLE 'EARTH CURRENTS' by Bob Vernal, ZL2CA, which originally appeared in *Break-in* (date unknown) has been reprinted in *Radio-ZS* (February 1991, p4). It draws attention to what can appear to be a mysterious RF-feedback problem that can occur when a solid-state transceiver and an auxiliary unit such as an external speech-processor are fed from the same high-current 12V PSU or battery.

ZL2CA points out that a transceiver rated at 100W RF output fed from a nominal 12V supply may draw up to about 20A at full output which, with SSB, occurs *only* on audio peaks. Even if the wires between transceiver and PSU have a DC resistance of only 5mΩ, then each lead will drop 100mV at the peaks, and this voltage appears between transceiver earth and the mains-earth of the PSU. With a speech processor, handling audio input voltages of about 10mV, connected both to the transceiver earth and the PSU earth line, there can exist the type of earth loop that so often results in problems with assemblies of hi-fi units, but in this case varying along with the SSB waveform. These earth loop cur-

MORE ON THERMISTOR TEMPERATURE COMPENSATION

JOHN BEECH, G8SEQ in describing the most effective VFO temperature-compensation technique using an NTC thermistor/varicap-diode (TT, April, p33) wondered whether he could claim genuine originality, or whether the idea had been used in TV tuners or somesuch.

No claims have been received of any use of this technique in professional electronics but Derek Money, G3MKD, who ran the now-closed Hamgear Electronics of Norwich has sent along evidence that he also hit upon using this idea in an amateur-radio VFO in "early 1989" which may or may not have been before G8SEQ began to use it "a couple of years ago". What matters more, is that he also found the system effective. After building a prototype, he advertised "The Hamgear 3-band VFO" intended for use by QRP operators and providing a switched output on three CW bands (3500-3585, 7000-7050 and 10,100-10,150kHz):

Fig 3. He still has the prototype built in early 1989 but lost interest in the technique when he received no enquiries from his advertisements. Temperature compensation was optimised at room temperature to around 15Hz per degree shift. Long term stability (3 hours on 7MHz) at room temperature the shift was less than 20Hz.

Postscript: Since writing the above notes, further evidence of thermistors providing temperature compensation of oscillators has come to hand. D A Bunday, G3JQQ, described a similar system to that of G3SEQ in *Two Improvements to the FT7B* (*RadCom*,

July 1982, pp582-3). In July 1981, Mike Walters, G3JVL, used an STC G24 thermistor in a stabilised crystal oscillator providing a reference signal at 10,368.000MHz (described shortly afterwards in the *Microwave Newsletter*). The idea of using thermistors to stabilise oscil-

lators (including an 8GHz Gunn diode oscillator) is discussed in the book *Thermistors* by E D Macklen (1979). Clearly, this idea is an excellent and thoroughly practical method of improving the temperature stability of a VFO and should become an established part of the amateur's armoury.

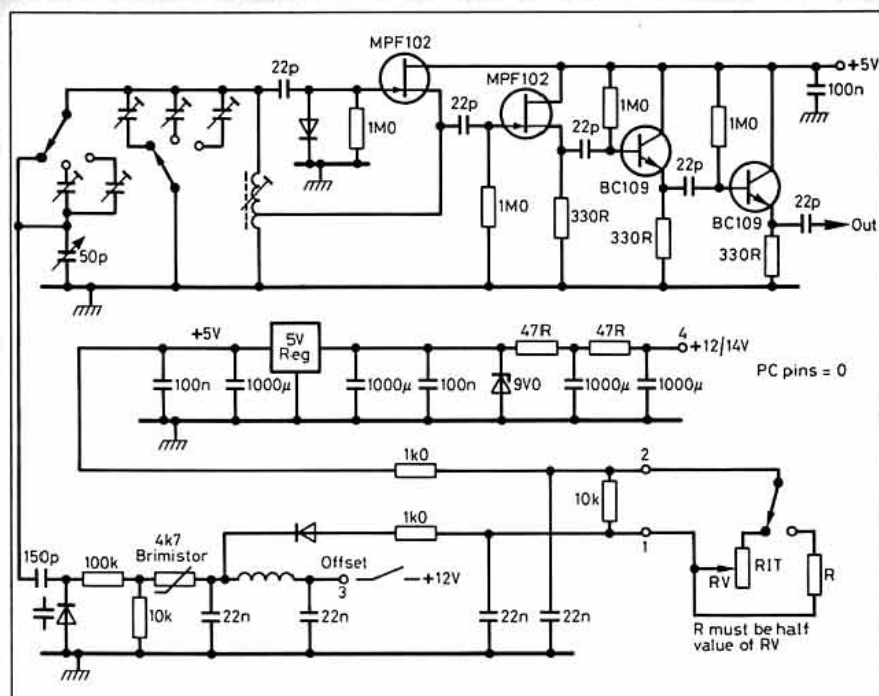


Fig 3: 'Hamgear' three-band VFO with Brimistor (KED 472CY) temperature compensation as announced in 1989 but which never went into production. The prototype built in early 1989 still exists.

rents and voltages can then result in audio distortion not unlike that produced by RF feedback, although in this case RF is not involved and the distortion does not disappear when the transmitter output is fed into a non-radiating dummy antenna.

ZL2CA writes: "A fairly sensitive test of 'power supply feedback' is to use an SSB two-tone tester in place of the microphone. Look for RF envelope variation on an oscilloscope. The two tone signal produces maximum envelope changes and consequently the current drawn from the main power supply is similarly modulated and 'lumpy'. As two-tone drive is increased, look for a form of hum modulation showing up on the RF envelope. If this occurs then it is either a poor power supply or the result of an earth loop causing a form of audio feedback provided that RF feedback is discounted by using a dummy load and provided that the two tone tester is not itself introducing a new earth loop."

If audio feedback of this type is detected, a possible solution is to use genuine double-insulated PSUs for all accessories. These usually have split bobbin transformers, and ZL2CA points out that this is a similar approach to that used for hi-fi audio systems in countering hum loops by using equipment with two-wire mains cords. If the transceiver PSU has negative earth then the station will have all connected accessories earthed, but with a minimum of loops.

For a TNC set-up, a mains isolation transformer can be used to feed power to the computer. An alternative approach is to provide a DC break in every cable that is required to carry low-level audio signals to the transceiver. Audio isolation transformers rated at 600Ω impedance, 1:1 ratio can adequately isolate low or medium impedance audio inputs or outputs. ZL2CA adds that if the PTT control is a DC type (usually grounded to transmit) then an opto-isolator is one of the only ways of providing an equivalent DC signal past a DC break. He also gives further advice on using opto-isolators in connection with TNC installations but points out that each solution usually needs to be customised to the particular combination of TNC and transceiver.

ZL2CA, himself, uses a combination of solutions. An external speech processor has a double-insulated power supply. A TNC cable has 1:1 audio isolation transformers and a 4N33 opto-isolator for PTT control.

I have no idea how common is this problem of 'power supply feedback'. As ZL2CA points out, no such problem exists with SSB linear power amplifiers using valves since the HT currents vary at most by a few hundred milliamps rather than the tens of amperes of all-solid-state transceivers with their external power supplies and connecting cables.

THE UNIVERSAL VFO

IN AN UNUSUAL coincidence, the June 1991 issue of both *QST* and *CQ* included articles on building general-purpose VFOs by the same author (Doug DeMaw, W1FB) with much in common, although some circuit details of the two VFOs differ. In 'Build a Universal VFO' (*QST*), W1FB describes a straight-forward VFO suitable for a variety of applications, such as tunable oscillator for superhet

FERRITE-BEAD CHOKE BALUNS

JOHN S BELROSE, VE2CV, in 'Transforming the Balun' (*QST*, June 1991 pp30-33) shows how the W2DU choke 1:1 balun, comprising simply a number of ferrite beads slipped over a short length of coaxial cable, can serve as the basis for excellent ferrite-bead-choke current baluns with 4:1 and 9:1 impedance transformations. He considers that the W2DU balun is: "The best so far devised. By *current balun* I mean a balun that, with each of its balanced output ports terminated in unequal resistances, forces essentially equal, opposite-in-phase current into each resistance. The traditional toroidal balun is a *voltage balun* in that, terminated as just described, it produces equal, opposite-in-phase voltages across the two resistances.

"For minimal radiation from a balanced transmission line, the currents on both its conductors must be equal in amplitude and opposite in phase; that is, there must be no current discontinuity on the radiator at the antenna feed point. . . . For antennas fed with a coaxial transmission line, the goal to achieve is little or no current on the outside surface of the coax shield. In general, these requirements cannot be met without a *current balun*."

The original W2DU balun (as described some years ago in *TT*) used 50 beads of No 73 ferrite (eg Amidon No FB-73-2401) on about twelve inches of Teflon dielectric cable, with suitable connectors to make a practical balun for 1.8 to 30MHz.

VE2CV provides a de-

tailed resume of the differences between the performance of toroidal and choke baluns, but also breaks new ground by showing how two ferrite-bead baluns can be used to provide a 4:1 transformation (50Ω to 200Ω-balanced) using short lengths of 93Ω cable (RG62A up to 100W, RG-133A for 1kW level), and three 1:1 baluns for 9:1 impedance transformation (50Ω to 450Ω-balanced) using 150Ω cable (RG-125 is difficult to obtain even in the USA and VE2CV suggests that other impedances can be used rather less effectively). Fig 4 shows the connections for 1:1, 4:1 and 9:1 impedance transformations.

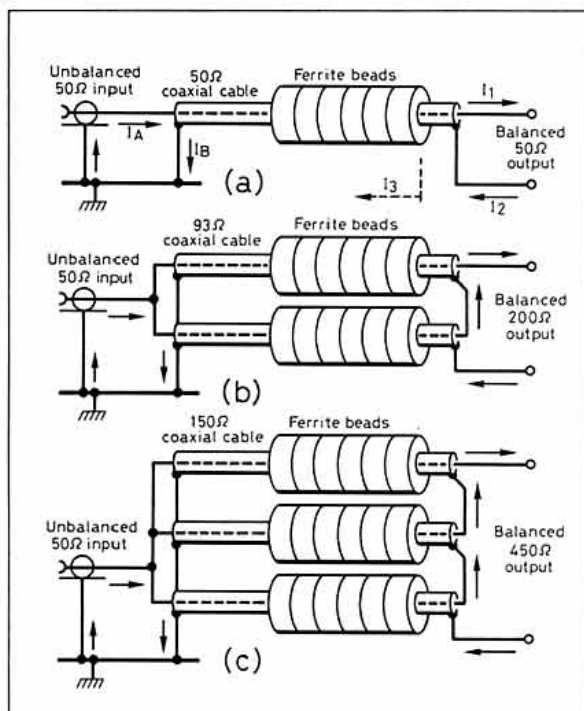


Fig 4: Ferrite-bead choke baluns as described by VE2CV (*QST*, June 1991). (a) The basic W2DU 1:1 choke balun using about 50 ferrite beads threaded on 12-inches of coaxial cable, using 50Ω coax for 50Ω balun; 75Ω cable for 75Ω balun, etc. (b) A 4:1 current balun based on two ferrite-bead coax-shield chokes. (c) Three ferrite-bead-choke baluns can be combined to form a 9:1 impedance transformation.

or direct-conversion receiver, transmitter/transceiver VFO, signal generator etc. His unit covers 2.137 to 2.586MHz but, with an appropriate tuned circuit, can work in any required band between about 1.8 and 10MHz. It has two output levels for driving active or passive mixers; with a 12V supply the 'high' output is about 22.3dBm from an extra bipolar amplifier stage (not in the 6.45 to 6.75MHz *CQ* design) which provides about 6.6dBm (4.2V P-P over 500Ω). Both designs use 2N4416 FETs as the oscillator with a source-follower FET isolating buffer, although the *QST* oscillator is a Hartley with tapped coil; the one in *CQ* is a Colpitts, with a source-follower buffer: Fig 5.

W1FB's *CQ* article 'The practical aspects of VFO design plus how to build one' concentrates on the choice of VFO components, advice on obtaining good stability, questions

of short and long-term stability/drift, etc. The following is a digest of some of the points made in this article:

- (1) Avoid using silver-mica fixed capacitors in VFOs; although once a popular choice they do not exhibit uniform temperature characteristics. W1FB prefers NPO ceramic types, with polystyrene capacitors (slight negative drift characteristic) as a low cost second choice.
- (2) An 'ideal' VFO would have no magnetic core in the tuning coil but would be air-cored on a ribbed ceramic former, seldom suitable for modern 'miniature' equipment. W1FB uses No 6 material toroid cores (eg Amidon T50-6; yellow) or equivalent slug-tuned core material. Coils after winding should be doped twice with, for example, General Cement polystyrene Q Dope.

- (3) Select the right oscillator device: W1FB dislikes bipolar transistors for this application as they tend to exhibit greater changes of internal resistance and capacitance with temperature than a JFET or MOSFET. He considers that the 2N4416 is his favourite device for VFOs since it has a high pinch-off characteristic and gives more output than is available from the MPF102 family of FETs. Dual-gate devices (40673, 3N211, 3N212) provide good performance and gates 1 and 2 can be tied together so that they function as single-gate devices without the need to bias gate 2.
- (4) If possible, use a good mechanical tuning capacitor rather than an electronic tuning capacitor (which changes capacitance with temperature): "Double-bearing capacitors that turn freely are best; avoid using capacitors with aluminium vanes - plated brass or iron vanes are better."
- (5) Use 1/2W carbon-film or carbon-composition resistors. Because of their greater physical size they tend to be more stable than 1/4W or 1/8W resistors as they can absorb more heat.
- (6) Two-or-more fixed capacitors in parallel (eg two 50pF NP0 ceramic capacitors to provide 100pF) provide more surface area than a single capacitor, minimizing heating from RF current.
- (7) W1FB uses single-sided G-10 glass epoxy board material for VFO PCBs and advises against using double-sided

PCBs or phenolic-base board material. He thinks that with double-sided boards, the etched-side conductors form unstable low-Q capacitors in combination with the ground-plane side of the PCB. He does not mention constructional practices not based on etched PCBs but see G3KMG's remarks in July TT.

- (8) Physically separate, with a dividing heat-shield made from PC board, the oscillator from the buffer/amplifier stages. The cover for the VFO box can then be vented above the buffer/amplifier stages

with the PCB-stock shield acting as a heat baffle.

- (9) Use lowest practicable oscillator voltage (eg 6 to 8V) to reduce internal heating, regulated by a zener diode or a small three-terminal regulator.
- (10) Filter the DC leads entering the VFO box with an RF choke and 0.001µF feedthrough capacitor to keep RF energy from entering the VFO circuit.
- (11) Do not use low-cost plastic trimmer capacitors in a VFO. Use miniature air trimmers or NP0 ceramic units.

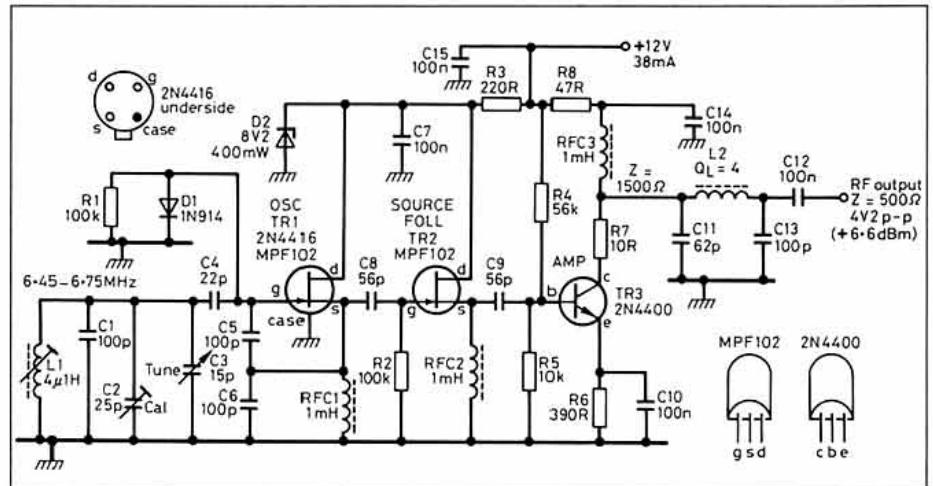


Fig 5: The VFO described by W1FB in CQ covering 6.45 to 6.75MHz but suitable for other frequency ranges by appropriate changes to L1/C1. C1, C4, C5 and C8 are NP0 ceramic or polystyrene types. C2 is a ceramic trimmer and C3 a miniature 15pF air variable. L1 is 32 turns of No 28 enamel wire on Amidon T50-6 (yellow) toroid. L2 has 25 turns (No 28 enam) on Amidon FT-37-61 ferrite toroid.

SHUNT-TYPE CRYSTAL LADDER FILTERS

TO THE BEST OF MY knowledge, the first appearance in the amateur radio press of a description of constructing ladder-type crystal MF filters was by J Pochet, F6BQP, in *Radio-REF*, May 1976, with an English-language digest in *TT*, September 1976 (and a full translation in *Wireless World*, May 1977). This was soon followed by the excellent series giving full design data by J Hardcastle, G3JIR (*RadCom*, December 1976, January, February, September 1977). Both F6BQP and G3JIR drew upon the classic paper by M Dishal (*Proc IEEE*, September 1965). Since then, most designs have followed basically similar lines but show that it is possible to cut costs by using low-cost colour-TV crystals (4.43MHz PAL, 3.58MHz NTSC).

"A different approach to ladder filters" by John Pivnichny, N2DCH, (*Communications Quarterly*, Winter 1991, pp72-76) is subtitled "Another way to make crystal filters". In effect, N2DCH puts the crystals in shunt

with the signal rather than in the usual series configuration. The main difference between them is that the shunt filter has its steeper cut off on the low-frequency side (termed an upper-sideband filter) whereas the series filter has its steep cut off slope on the high frequency side (lower-sideband filter). N2DCH considers that the shunt filter may be preferable for narrow bandwidth filters (eg CW filters) particularly when using relatively low-Q plated crystals in HC-18 holders, although he admits that the series-type lower-sideband filter is usually preferable for the wider SSB filters. He points out that it is possible to create a pair of filters (one shunt, one series) to provide switched sideband selection with just one BFO crystal. N2DCH provides design data for

shunt-type filters plus an example of a CW filter designed for 3470Ω termination; Figs 6 and 7.

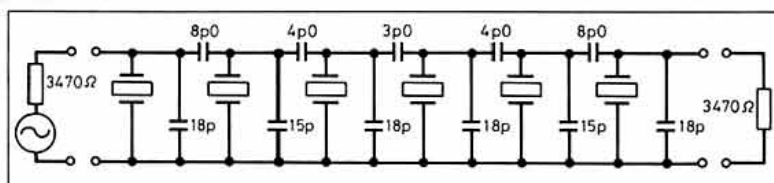


Fig 6: Shunt-type crystal ladder CW filter using six 3.58MHz NTSC crystals designed for 3470Ω terminations. Crystals should be matched to within 100Hz (TV crystals are often only specified as within 300Hz but usually are within 200Hz).

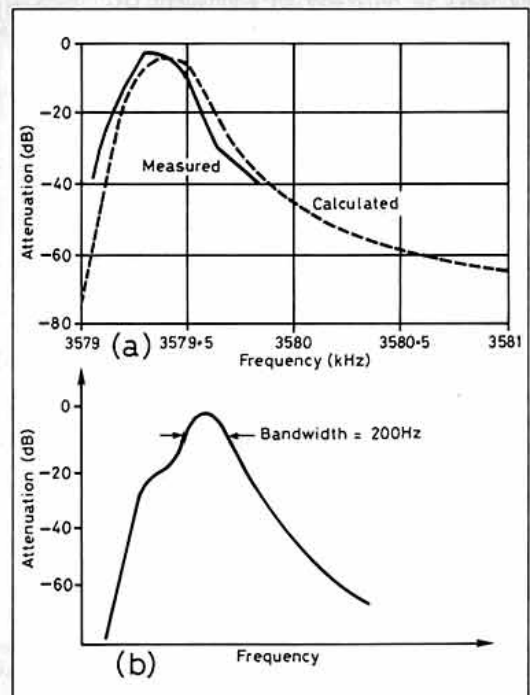


Fig 7: (a) Calculated and measured response curves for the CW filter. (b) Filter response resulting from use of poorly matched crystals.

Performance tests for the CQ unit are given for a frequency of 6.7MHz with a room temperature of 70°F (21°C). Short-term drift amounted to 2Hz during the first 5 minutes of operation; over a period of some 35 minutes, the frequency drifted 75Hz lower, then back to within 10Hz of the initial frequency before stabilization occurred. This was with the unit terminated with a 560Ω resistor; when this was shunted with a 10Ω resistor, the frequency shifted by 4Hz showing good isolation. The ARRL Laboratory test on the QST unit at around 2MHz gives the frequency drift as less than 4Hz in the initial 4 minutes.

MODIFIED G2DAF LINEAR AMPLIFIER

IT IS NOW AROUND 30 years since publication by G R B Thornley of the G2DAF series of SSB designs, including his high-grade HF receiver, his Mark 1 and 2 SSB transmitters, and the G2DAF 400W PEP linear amplifier. The linear amplifier, first published in the April, 1963 *RSGB Bulletin* (former title of *RadCom*) with additional notes in the May issue, was later published in a condensed form in *SSB Equipment* which also reprinted the G2DAF SSB Transmitter Mark 2: Fig 8.

The linear amplifier was based on the passive-grid technique suitable for being driven from an SSB exciter/transmitter of around 50W PEP. The original model used two 4-125A (Mullard QY3-125) valves but it was noted that the method of operation was suitable for any of the commonly used tetrode or pentode amplifier valves including the 4-65, 4-125, 4-250, 4X150A, 4X250B and 813. The valves were operated under zero bias conditions without any of the complications of carefully regulated screen supplies, the screen voltage derived by rectifying a small portion of the input signal in a voltage-doubler.

G2DAF pointed out that "in many ways the 813 is a quite remarkable valve - its performance in the G2DAF amplifier is quite outstanding. With 2.5kV anode potential, it is possible to run *one* 813 valve to 400W PEP output. This is possible without degradation of linearity, and 'on the air' reports indicate that the intermodulation distortion products are at a level 45dB down in relation to the wanted voice sideband signal. This is about 5dB better than the writer's amplifier using a pair of 4-125A valves."

The G2DAF linear amplifier still in the 1990s represents a valid approach but the input circuit may require a minor modification for use with current solid-state transceivers and/or for different valves. A modified 2DAF amplifier has been described by P J Liebenburg, ZS2PL, (*Radio-ZS*, January 1991) with additional suggestions by Lou Gatzke, ZS6AOZ, (*Radio-ZS*, April 1991). ZS2PL, (formerly ZE5JU) has been using a modified 2DAF with two 4X150A valves since 1970, driving it from a Collins KWM-2 transceiver, but then added a 1:3 step-up toroid transformer to avoid a mismatch to his ICOM 730 solid-state transceiver.

Fig 9 shows modification to the original G2DAF design which had two 4-125A valves and a single passive-grid resistor (300Ω) made up from five 1W resistors for SSB operation. The three 50Ω, 50W dummy-load resistors used by ZS2PL would seem very generously rated, even when driven by an

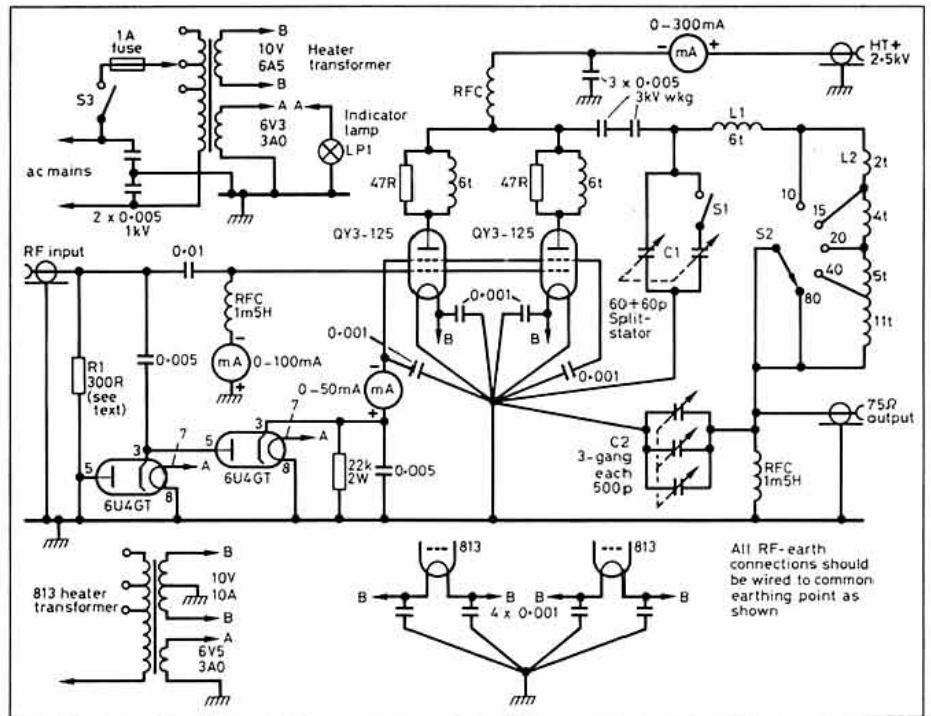


Fig 8: Circuit diagram of the 1963 G2DAF linear amplifier. S1 open for 28, 21 and 14MHz, closed for 7 and 3.5MHz. Fixed capacitors are mica except the three 3kV 0.005μF disk ceramics. The anode RFC should be of the split-winding type without series resonances on any of the HF bands, particularly if the amplifier is intended also for use on 10, 18 and 24MHz.

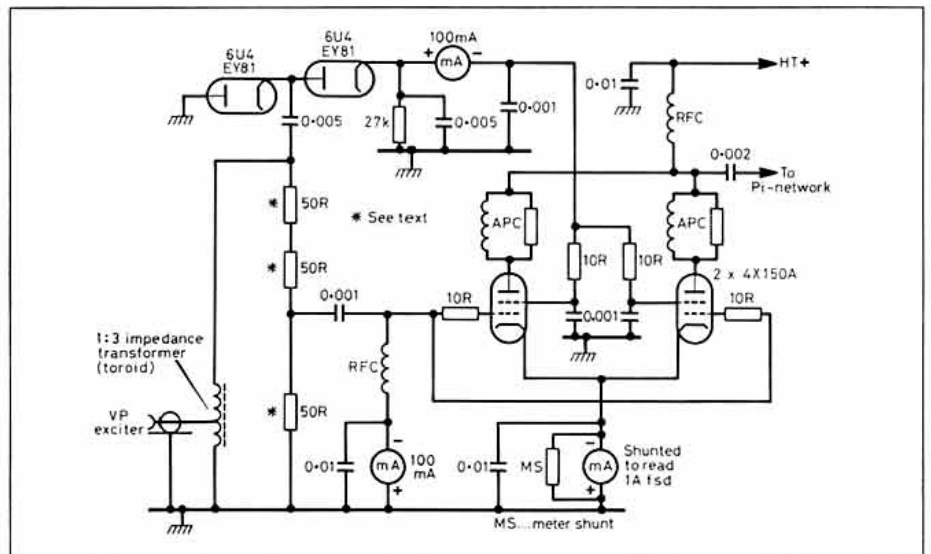


Fig 9: Modified input arrangement of the G2DAF linear as recently described by ZS2PL/ZS6AOZ.

ICOM 730. ZS2PL states: "The 1:3 toroid step-up transformer provides a better match to modern solid-state rigs. The RF voltage at the top of this resistor chain is of the order of 100V or more and is rectified and doubled as an 'audio varying DC voltage' and applied to the screen-grids of the amplifier valves, with excellent linearity. In the absence of RF drive there is no screen voltage and the standing current is very low.

"The reason for the voltage divider input circuit was due to the fact that 3W of drive would destroy the 4X150As ($\mu = 12\text{mA/V}$) and the grid drive is therefore taken from the lower end of the chain. This will have to be taken from higher up the resistor chain, even from the top as G2DAF did in his original design, for driving a pair of 4-125A valves.

"This type of linear has many desirable features, including low cost, low component

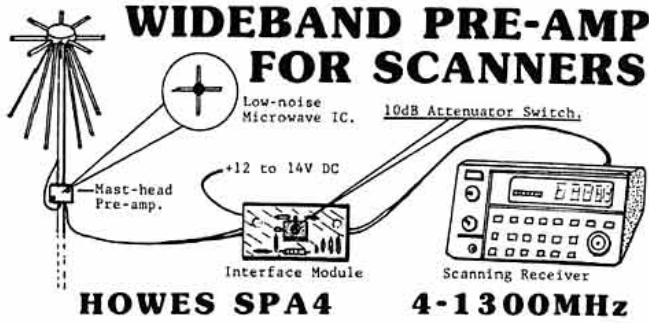
count, stability due to the swamping effect of the passive grid input load and simplicity of construction. To the best of my knowledge there are no solid state diodes which will reliably handle the RF input voltages, and thermionic diodes are used in the voltage-doubler arrangement as in the original circuit; note that the cathodes and heaters of these rectifiers must not be connected; I have used two EY81 television rectifier valves without failure since 1970 and can recommend them. The meter shunt is earthed right at the amplifier cathodes, and the leads run in shielded wire away from RF to the meter which is mounted in a shielded can."

It must be stressed that a linear amplifier with an EHT supply of around 2.5kV calls for very careful construction and generously rated components as well as stringent safety precautions during setting up and testing, etc. □

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Hugh Mehal (13) 2E6AAA, Simon Khan (12) 2E1AAB, Robert Cherry (15) 2E1AAC, Natalie West (12) 2E1AAB, Vicky Foster (11) 2E1AAD, David Hunt (13) 2E6AAB, John Redwood, MP, Parliamentary Under Secretary of State for Corporate Affairs, Jonathan Page (17) 2E1AAA in the background.

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First Steps in Home Construction

A series of articles by John Case, GW4HWR

THE ONLY DISCRETE diode used on the PCB is a voltage reference or zener diode. However, the method of marking is the same for almost all small diodes. Type numbers are either printed on the body in 'plain language', eg OA91 or 1N914, or in coloured bands when each colour indicates a digit, eg yellow-brown-yellow-grey = 1N4148. '1N' indicates a diode and is not coded.

It is my opinion that a very large number of failures in projects built from published designs are due to incorrect fitting of diodes! This is brought about by the apparent anomaly in the marking of the polarity. Fig 9a shows the various ways commonly used. The + sign often found at the cathode causes the unsuspecting to believe that this must be the anode because the theory tells us that the anode must be positive with respect to the cathode to cause conduction. The simple circuit shown in Fig 9b gives the reason; the + sign indicates the positive end of the load when the diode is used as a rectifier.

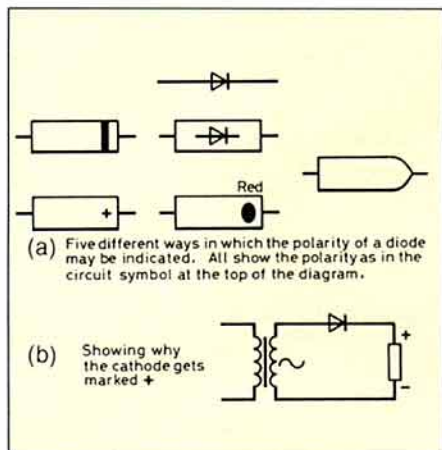


Fig 9: (a) Diode markings; (b) The markings on a diode can confuse.

To test a diode, measure its resistance in both directions as shown in Fig 10a. Again, note that the actual polarity of the meter terminals is reversed while in the resistance mode. If the meter has several resistance ranges, use the lowest one. The forward resistance should be in the region of 1000Ω or less depending on type, and the reverse value should be 1MΩ or more. If a zener diode is being checked, a low reverse resistance may be indicated if any other range of the meter is selected. This would be due to the battery voltage, on the higher ranges, exceeding the zener voltage.

PART FIVE: DIODES, TRANSISTORS AND THE PCB

How to test diodes and transistors, plus (at last!) putting the components onto the printed circuit board.

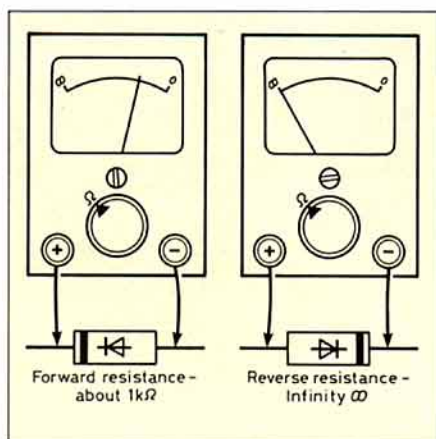


Fig 10(a): Testing semiconductors - diodes.

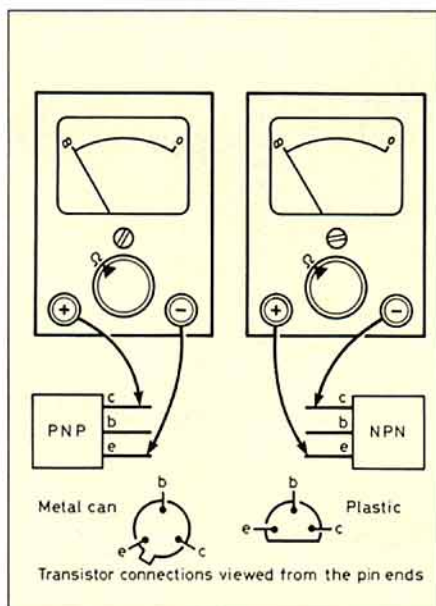


Fig 10(b): Testing semiconductors - transistors.

TRANSISTORS

THREE DIFFERENT TYPES OF silicon transistor are used in the PSU circuit. Q1, Q2 and Q5 are NPN general purpose types and Q3 is a PNP complementary type. They are not critical but the pin out must be correct. A number of alternatives are suggested and any combination will work equally well. The inset of Fig 10b gives the pin connections. Q4 is not mounted directly on the PCB but is bolted to the heatsink. The overlay diagram (Fig 11) shows the pin out. Test the transistors using the Ohms range of the meter. Connect them as shown in Figure 10b. Note the polarity for each of the types, PNP and NPN.

In each case the resistance indicated should be very high; 1MΩ or more is quite normal for silicon types. Now connect a resistor of between 47 and 100k between base and collector (I always use a wet finger!) and the resistance should fall towards zero. The amount that the resistance decreases depends on a number of factors such as the meter range used, the value of the resistor (or the wetness of the finger) and the gain of the transistor. The fact that the resistance falls proves that the device is working even if its gain is not as high as it should be. A few tests will enable the relative 'goodness' of transistors to be assessed. You have now tested all of the PCB components and greatly reduced the chances of PCB failure.

THE PCB

THE FOIL PATTERN IS GIVEN full size in Fig 12 for those who wish to produce their own, but it is generally assumed that a ready-made board will be used [details of PCBs and full kits for the PSU Project will be published next month - Ed]. Before mounting any components, mark through the fixing holes onto the heatsink, noting the position from Fig 13. Be sure that the board is held with the copper



side towards the heatsink and that the holes for Q4 are at the bottom.

Insert the nine terminal pins from the print side of the board so that the shoulders of the pins are flush with the copper. This kind of statement appears in many published projects. It sounds easy but can be surprisingly difficult and frustrating in practice. The board must be supported very close to the pin as quite a lot of pressure is required to push the pin so that the splined section enters the hole.

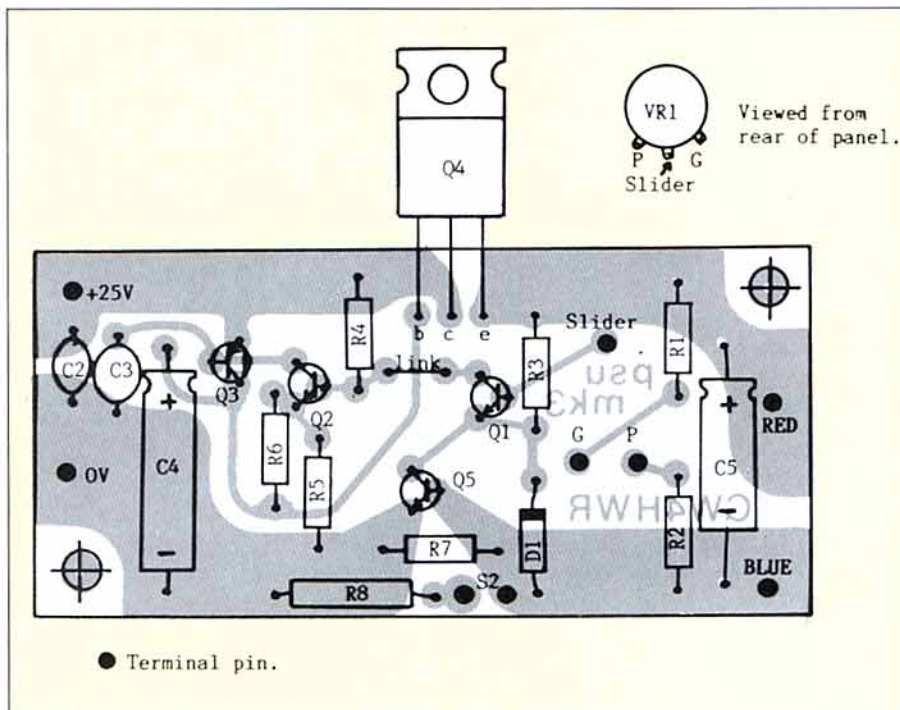
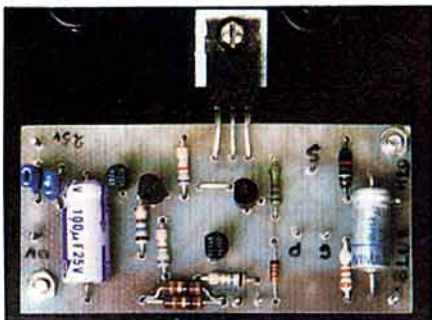


Fig 11: PCB Component overlay.

A very simple jig (Fig 14) makes all the difference. A short piece (25mm is plenty) of brass or steel tubing, about 5mm outside diameter is required. Car brake pipe, caravan gas pipe or a spacer from a rotary switch are all ideal. Fix vertically in the vice with a few millimetres sticking out. Pass the pin through the correct hole, rest the component side of the board on the tube with the end of the pin inside. If the pin is a single-ended one, press it home with the flat end of a pair of pliers, etc. Double-sided pins are a little more difficult and it is worth making a 'pusher'. A small pin chuck pushed into a small file handle makes the job easy. Pins on the print side of the board are not required and should be cut off with side-cutters if double-sided pins have been used. If a pin needs to be inserted after the board has been completed, the above technique makes an impossible task easy! Solder the head of each pin but look out for excess solder either filling adjacent holes or causing 'solder bridges'.

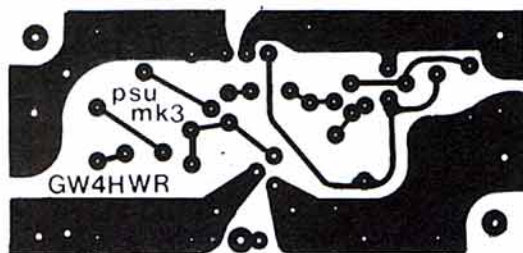


Fig 12: The PCB layout (actual size)

If the board is being built for a fixed voltage PSU, do not put in the pins marked: slider, G and P, but instead insert a miniature, horizontal 4.7k preset in the holes.

Now insert the eight resistors and C4 and C5, all of which should lie flat on the board. Check that the polarity of the last two items is correct. If the markings are not clear, remember that the 'crimp' at one end of axial type electrolytic capacitors indicates the positive. Double check - insert them the wrong way round and you have a miniature time bomb! C2 and C3 are mounted as close to the board as possible, depending on type. It is good practice to keep the leads above the board as short as possible. It will probably be easier to fix one component at a time if this is your first PCB. Bend the leads to about 45° on the copper side of the board to stop the component falling out, then clip off close to the copper. About 0.5mm - 1.0mm protruding is ideal. Solder, then proceed to the next component. The link is made from one of the off-

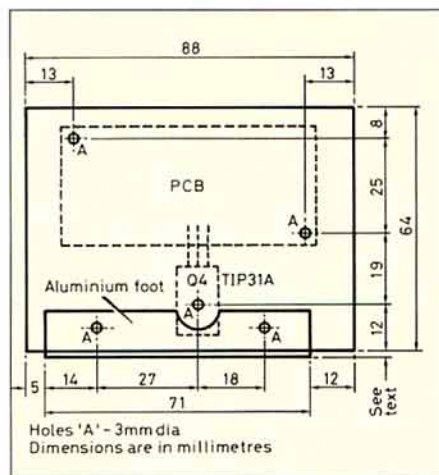


Fig 13: Positioning the PCB and heatsink.

cuts from a resistor. D1 is treated in the same way as a capacitor - note the polarity.

Transistors Q1, 2, 3 and 5 are now fitted. Push them down so that the body is no more than 5mm above the surface of the board. Check that Q3 is the PNP type. Finally, fit Q4. Carefully push the leads into the PCB until they protrude by 1mm, then solder. The marking TIP31A should be facing the opposite edge of the board. Leave it in a vertical position for now. To complete, label the terminal pins, on the component side of the PCB, with a fine fibre tip pen.

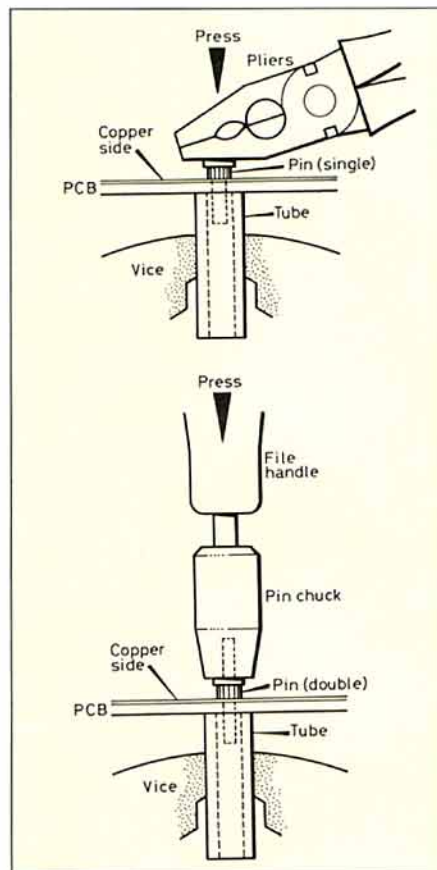


Fig 14: A simple jig makes pin inserting much easier.

... to be continued

NEXT MONTH

Adding the heatsink, and testing the power supply

AN IDEAL HF RECEIVER FRONT END

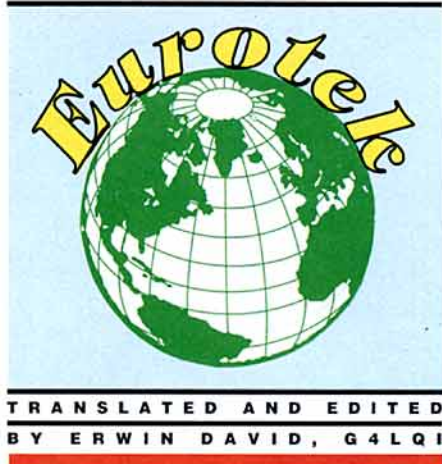
JAPANESE DESIGNERS are surprised when they try their products amid the European 'aethersoup' containing hundreds of strong and superstrong HF broadcast stations. In Japan, Australia and in parts of the USA their night-time carriers produce antenna voltages of a few mV while here in Europe the closely spaced broadcast signals from simple dipole or Windom antennas often exceed 50mV. Expert users demand ever better rejection of both close-in and out-of-band 'super-signals'.

REJECTING FAR OUT QRM

TWO STRONG out-of-band signals or their harmonics, mixing to produce a strong in-band beat, can distort or even swamp a weak wanted signal by overloading the first mixer. The multitude of strong broadcast stations, spaced at 5kHz intervals, actually can and do create a 'comb' of whistles throughout an amateur band. This is called intermodulation; 2nd order if this beat is of the form $f_1 \pm f_2$, 3rd order if $f_1 \pm 2f_2$.

Assuming this mixing of offenders takes place in the first mixer, there are two defenses; the FT-1000 scores well in both.

First, one can prevent offending signals from reaching the first mixer by preselection, ie by placing between antenna and first mixer a multi-pole LC filter which, ideally, attenuates all frequencies but the wanted one, or at least all outside the amateur band in use. In



Guenter Schwarzbeck, DL1BU, devotes 15(!) pages of *cq-DL* (March, April and May 1991) to Yaesu's FT-1000 top-of-the-line transceiver. Surprisingly, he finds that the compromises causing the greatest deviation from 'ideal' receiver front-end behaviour can be avoided by a home builder.

an amateur-band-only receiver this is not hard, but in a general coverage receiver things are different. Our percentually widest ama-

teur band, 1.81 - 2MHz, is just over 11% wide. To constantly cover the range of 1.8 - 29.7MHz with filters of that width would take 27 filters, unaffordable in space and cost even in top-of-the-line radios.

In the FT-1000, 12 filters cover this range, while some of the amateur bands are favoured with additional filtering for a total of 17 segments. This is a big improvement over the eight half-octave filters frequently seen in general coverage receivers.

Second, one can design the first mixer to remain linear up to very high signal levels. While ten years ago third-order intercept points of +5 to +15dBm were acceptable (much earlier even -30dBm), in present-day receivers +20 to +25dBm is expected and the FT-1000 double-balanced 4-FET first mixer complies; **Fig 1**. Note that balanced local oscillator injection of $2V_{RMS}$ is required but this is not a problem because of the high impedance of the FET gates.

What then if, in spite of all this sophistication, the 5kHz comb of whistles is still there? One must conclude that the intermodulation takes place in non-linear components ahead of the mixer; the RF pre-amp is not the culprit, as its being switched in or out does not make any difference. I established, sometimes by quite tricky test procedures, that the sub-miniature ferrite cores in the coils in the pre-selector filters saturate due to high circulating currents when one of the intermodulating signals falls within the filter's pass band. This affects 3rd order intermodulation. Worse, however, is 2nd order intermodulation oc-

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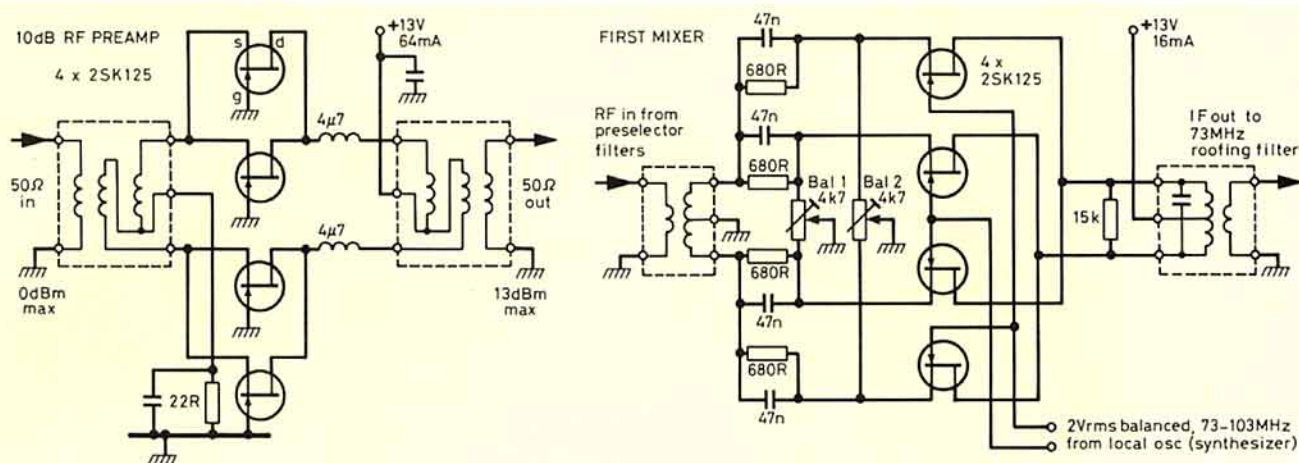


Fig 1. RF preamp and 1st mixer of main receiver in the Yaesu FT-1000 transceiver.

curing in the switching diodes between antenna and preselector, sometimes three of them in cascade! Shorting any one of them improved intermodulation performance by 4dB at an antenna signal level of -10dBm.

REJECTING CLOSE-IN QRM

AFTER THE FIRST 73.62MHz IF with a 16kHz-wide roofing filter, there is a second IF at 8.215MHz with four crystal filters as standard equipment: 2.4 and 2kHz wide for SSB, 500 and 250Hz wide for CW. These can be backed up by optional filters in the 455kHz 3rd IF to permit pass-band tuning and further

improve selectivity. Before buying expensive optional filters, however, remember that their selectivity is meaningful only to roughly 60dB down; beyond this, reciprocal mixing caused by synthesizer phase noise broadens the selectivity curve. In this respect the FT-1000 is good but by no means outstanding.

CONCLUSIONS

THE FT-1000 WAS designed as a Jack-of-all-trades. As such it is remarkable.

Experienced constructors willing to trade flexibility for optimum performance on few bands or spot frequencies might combine the

excellent FT-1000 mixer circuit with preselector filters using air-wound coils, or formers with cores of more generous dimensions. Each filter would be no wider than the band of interest, or even be hand-tunable across that band. Filter selection would be with wafer switches or miniature relays.

The reciprocal mixing problem, at least for spot frequencies, could be solved by using a simple crystal oscillator having low phase noise; even a good FET VFO followed by the usual buffer and amplifier would outperform all but the best commercial DDS synthesizers; the latter apparently still are too expensive for amateur radios.

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Sideband Can be Simple!

by Steve Price, G4BWE

ALTHOUGH SSB IS A HIGHLY popular mode, if a survey were to be carried out in order to ascertain what kind of equipment amateurs home-construct most, the SSB transceiver would almost certainly come way down the list.

Is this ironic situation understandable? Yes, because the very obvious complexity of modern factory built sideband rigs is enough to discourage the vast majority of homebrewers. That said, there has been something of a renaissance lately in the construction of QRP CW transceivers for the HF bands. Many of the operators who are responsible for this trend have openly declared that they are depressed by the current state of affairs within our hobby. "You need a degree in electronics and computer science to understand how transceivers work nowadays" is a typical reaction.

However, when arguments become emotive it is sometimes all too easy to lose sight of the real issues. Modern commercial transceivers are highly complex, but their complexity is due in large part to the application of digital frequency synthesis - a technique which has been made almost mandatory in the case of HF transceivers because of the need to provide reliable operation on no less than nine separate bands, with general coverage receive thrown in for good measure!

Yet SSB is not, in itself, a difficult mode, and when drawing comparisons between CW and SSB transceivers it is important to make sure that we compare like with like. Indeed, a simple sideband rig does not necessarily have to employ many more components than its CW counterpart.

In short, a good deal of fun can be had from the construction of rudimentary sideband transceivers if we are prepared to accept certain limitations in their functionality. Firstly, it is far easier to start with a single-band rig, as the requirements of multiband operation lead inevitably to compromises in performance when using simpler design techniques. Restricting the transmit power to around 5W PEP is also advisable because a small PA is much cheaper and easier to construct. Provided we make our choice of band with this in mind, many enjoyable QSOs can still be made: I have found that 7MHz is a particularly good band for low-power SSB operation during daylight.

Having accepted the restrictions outlined above, the constructor may console himself/

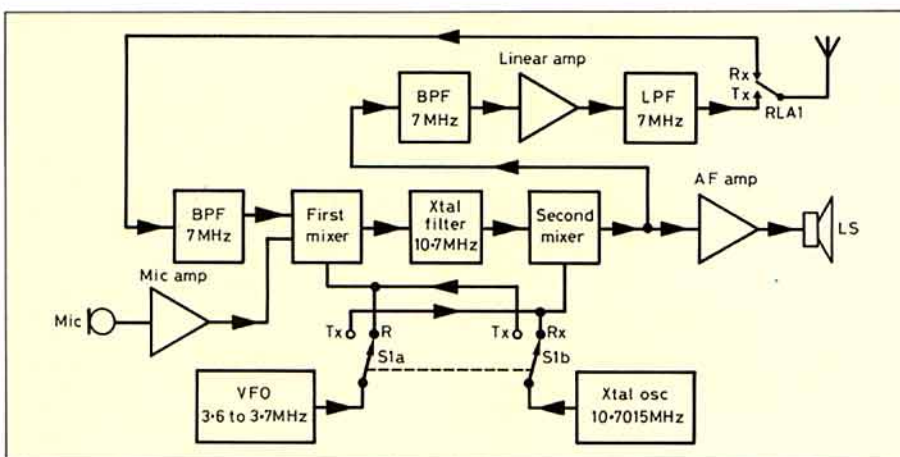


Fig 1: A simple SSB transceiver for 7MHz.

herself with the fact that a VFO-controlled single-band SSB transceiver giving 5W PEP can still be built with high quality components for under £100. Although some of the front panel features associated with commercial rigs may be missing - digital readout, for instance - the 'essentials' such as PTT operation can easily be provided. Furthermore, the receive performance of the homebrew transceiver will probably exceed that offered by many factory-built multi-band designs.

BACK TO BASICS

FIG 1 SHOWS THE BLOCK DIAGRAM of an SSB transceiver for the 7MHz band. In deciding on this architecture two fundamental decisions have been made. Firstly, the filter method of SSB generation is adopted. Much has been written in recent years about various phasing techniques for SSB, but although phasing systems appear to offer certain advantages - notably the elimination of an expensive crystal filter - further investigation throws up so many performance shortcomings that in the final analysis phasing systems are shown to possess little more than curiosity value. This is perhaps a rather harsh judgement and there are those who would argue with my conclusion. Nevertheless, it is a decision I have reached after much careful thought. It is based, ultimately, on the realisation that the filter method not only outperforms practical phasing systems, but does so using far simpler circuitry. As a footnote to this argument it should be pointed out that the phasing method may yet have its day, but only because DSP (Digital Signal Process-

ing) offers the prospect of almost perfect implementation of phasing in the digital, rather than analogue, domain. DSP transceivers are bound to appear over the next few years but at the moment it would be a brave homebrewer who decides to try and 'knock one up' on the kitchen table!

The second decision is to use a single-conversion signal chain, ie there is only one intermediate frequency. This may seem an unwise choice when the majority of commercial HF rigs use either double or triple conversion. Remember, however, that these transceivers are multi-band and also multimode, with possibly general coverage receive as well. In complex transceivers multiple IFs are a necessary evil, although they can easily cause problems of their own - spurious responses/outputs and receiver 'birdies', for instance. In contrast, the single-band transceiver presents a glorious opportunity to eliminate whole blocks of signal circuitry without compromising performance in any way. Choosing the right intermediate frequency involves a number of important considerations, not least of which is the resultant image frequency (more about this later). As a general rule, however, the higher the IF the better, even though this may result in received signals being up-converted by the first mixer.

On receive, the transceiver operates as follows. Incoming signals are routed via the antenna changeover relay (RLA1) to a band pass filter. This filter, which will typically comprise a pair of closely coupled parallel-tuned circuits, is fixed tuned and has sufficient bandwidth to cover the range 7.0 to

7.1MHz, thus eliminating the need for a pre-selector control. In the interests of achieving absolute simplicity, constructors might be tempted to use just a single tuned circuit here - be warned, however, that paring down the design at the very beginning of the signal chain will result in performance degradation 'across the board' with a reduction in the receiver's effective dynamic range, poor image rejection and the increased likelihood of spurious responses.

The first mixer is driven directly from the output of the bandpass filter. Provided that a mixer of reasonable quality is chosen, there is absolutely no reason to employ an RF amplifier. It might be suggested, of course, that the increase in sensitivity provided by RF amplification could facilitate the use of electrically short antennas (ie less than $\lambda/8$). This is a spurious argument in the case of low-power transceivers because it would be foolish to compromise very much on the size of the antenna when it will inevitably reduce the radiation efficiency on transmit.

During receive, S1a couples the VFO to the first mixer. Although shown conceptually as a double pole switch, S1 will in practice be either a relay or some form of semiconductor gate which is controlled by the PTT. The IF is 10.7MHz and so for reception of a signal on 7.05MHz, for instance, the VFO must be tuned to 3.65MHz (ie $7.05 + 3.65 = 10.7$). The mixers must be balanced types in order to satisfy the requirements of SSB generation on transmit, and the receiver also performs better if balanced mixers are used. The crystal filter, which has a bandwidth of around 2.4KHz, selects the wanted signal and presents it to the input of the second mixer or product detector. The 10.7015MHz crystal oscillator drives the second mixer's LO port via S1b. This enables the second mixer to function as a product detector so that it gives an audio output.

An IF amplifier is not shown in Fig 1 be-

cause the transceiver is quite capable of functioning without one. This does of course mean that the audio amplifier must have a much higher gain than would otherwise be necessary. It also helps if active mixers configured to give a modicum of conversion gain are employed, rather than the alternative diode ring mixers which have a conversion loss. If an IF amplifier is used, this should be placed between the filter output and the input to the second mixer. In the interests of avoiding instability it is best to restrict any IF gain to no more than 50dB. This latter statement may cause a few raised eyebrows - it is, after all, not unusual for commercial designs to employ 90-100dB of IF gain. Remember, however, that a major reason for this is to enable superb AGC characteristics to be achieved. Admittedly, it is nice to know that the level of signals arriving at your antenna can vary over a range of 90dB without there being any noticeable change in loudspeaker volume - especially if you have just forked out £2000 for the rig - but in the context of a simple homebrew project such performance amounts to overkill.

When transmitting, S1 is toggled so that the amplified microphone signal can be mixed with the output of the crystal oscillator. A double sideband, suppressed carrier signal at 10.7015MHz now appears at the output of the first mixer. This signal is passed through the crystal filter which removes the unwanted (upper) sideband, leaving us with 10.7MHz SSB. Note that the carrier crystal frequency may need to be changed to match the available SSB filter. The second mixer, which is now coupled to the VFO, produces two outputs - $10.7 + 3.65 = 14.35\text{MHz}$ and $10.7 - 3.65 = 7.05\text{MHz}$. It is, of course, the latter output that we desire to transmit and so this is selected by the bandpass filter interposed between the second mixer's output and the linear amplifier. At the output of the linear amplifier is the obligatory low-pass filter. This

serves to attenuate not only the harmonics of the 7.05MHz signal but also any residual image and crystal oscillator leakthrough at 14.35 and 10.7MHz respectively.

CIRCUIT IDEAS

FIGS 2 TO 4 FEATURE CIRCUITRY developed for a homebrew 7MHz SSB transceiver. Despite having a transmit power of only 5W PEP this rig, when used in conjunction with a half-wave dipole antenna, has provided a host of effortless day-time contacts.

Hopefully, the circuits themselves and the notes which form the rest of this article will inspire many home constructors who until now have stopped short of attempting to build a fully-fledged sideband rig. Although the frequency-dependent component values have been calculated for 7MHz these may, of course, be scaled accordingly for other bands. My own transceiver is housed in a commercial metal case and apart from the potentiometers, switches and sockets, all components are mounted on Veroboard.

Fig 2 shows the major part of the signal chain, including the microphone preamplifier and PTT switching circuitry. IC1 and IC2 are the first and second mixers (refer to Fig 1 for clarification). The SL6440C integrated circuit bipolar mixers [1] are strongly preferred to the alternative diode ring types for the following reasons:-

- Diode ring mixers require a high local oscillator drive power (typically 10mW), accurately matched into a 50Ω LO port. In contrast, the SL6440C features an integral local oscillator buffer. The input impedance of this buffer is 1.5kΩ (typical) and a drive voltage of 250mV RMS is perfectly adequate. This means that in many applications an external VFO buffer is unnecessary. Furthermore, it is far easier to implement the Tx/Rx LO switching discussed earlier.

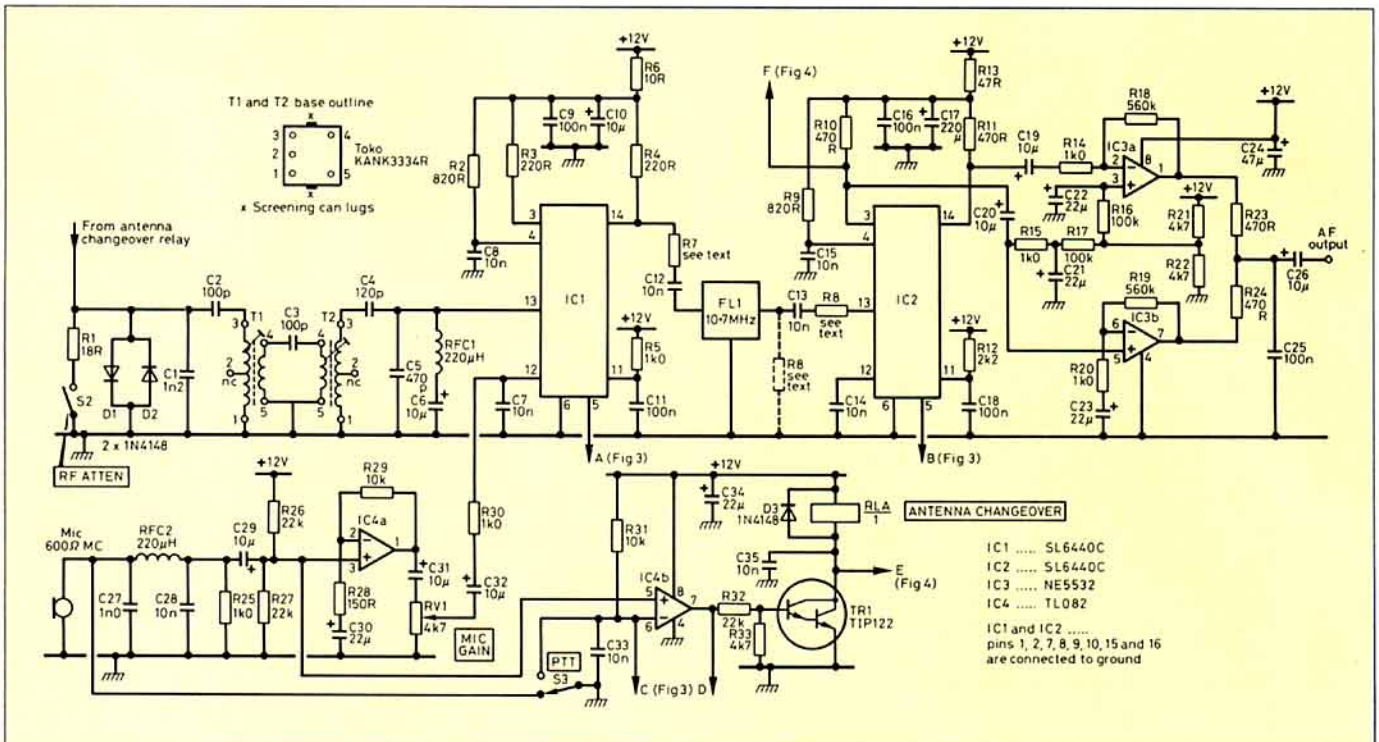


Fig 2: The transceiver signal chain and PTT circuitry. C1-C5 may be polystyrene or ceramic plate.

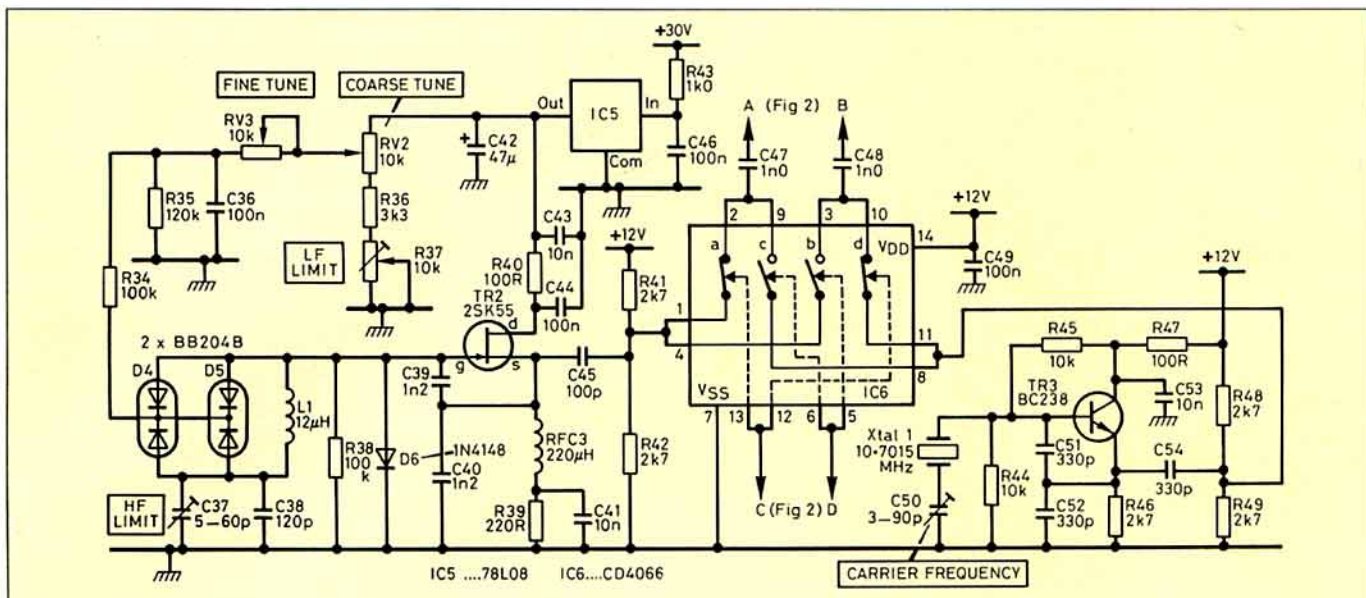


Fig 3 The oscillators and their switching circuit. L1 is 51 turns of 26SWG enam on a T68-6 powdered iron toroid.

- The SL6440C is a programmable device and can be operated so that the best trade-off between dynamic range and gain is achieved. In practice, this means that it is possible to design for entirely adequate 'intercept' performance while still obtaining a useful degree of voltage gain. Diode mixers, however, will always incur a signal loss (typically 6-7dB).
- The input impedance of the SL6440C, when used in the simpler single-ended mode adopted by the author, is 500Ω. The required terminating impedance of typical crystal filters is close to this value, so filter matching is particularly straightforward. Diode ring mixers normally have an input impedance of 50Ω which necessitates either transformer matching or, alternatively, the use of a buffer stage.

The receiver has a very simple RF attenuator consisting solely of resistor R1. This is activated by closing S2, whereupon R1 will shunt the receiver's input, thus reducing the level of signals presented to the first mixer via protection diodes D1, D2 and the bandpass filter comprising T1, T2 and C1-C5. Rather than trying to re-invent the wheel I have based the bandpass filter on designs published by Lorin Knight, G2DXK [2].

IC1 has two inputs. Although originally intended for balanced input, one is used here

for RF and the other for AF. Pin 13 is used as the RF input on receive and pin 12 as an AF input on transmit. IC4(a) is the microphone preamp and provides a voltage gain of 36dB which is adequate for close speaking into a communications-quality 600Ω moving coil microphone. C27-28 plus RFC2 remove unwanted RF from the audio input. C7 bypasses pin 12 at RF, thus effectively grounding this input on receive. C6 and RFC1 provide a low-impedance path to ground for audio frequencies, thereby introducing a complementary action on transmit.

The microphone must be muted on receive in order to prevent ambient noises from modulating the incoming signals. This is easily achieved by using an SPDT PTT switch (S3), the normally-closed contact being wired to the microphone insert as shown. Microswitches are usually double-throw types (eg Maplin FP42V) and make excellent PTT switches.

Positioned at the heart of the signal chain, between the output of the first mixer and the input of the second, is the all-important crystal filter. The values of R7 and R8 are calculated to provide correct terminating impedances at each end of the filter. For instance, if the filter requires 800Ω terminations then the values are calculated as follows: R3 and R4 provide external collector loads for IC1 and thereby set the first mixer output imped-

ance at 220Ω. This means that R7 must have a value close to 580Ω (ie 220 + 580 = 800). In practice, the use of a 560Ω resistor is perfectly acceptable. We can assume that the input impedance of IC2 is 500Ω and thus R8 needs ideally to be 300Ω (500 + 300 = 800). The 300Ω value is indeed available from the E24 series, but once again the nearest preferred values in the E12 series - 270Ω or 330Ω are also suitable.

If a filter requiring 300Ω terminations were to be employed, R7 would need to be 80Ω so 82Ω would be the obvious value to choose. As the input impedance of IC2 is greater than 300Ω, R8 must then be re-positioned so that it shunts the mixer's input (ie it must be connected between the junction of FL1, C13 and ground). The appropriate resistance is 750Ω (750 in parallel with 500 = 300Ω) - either this E24 value or the more common 680Ω would suffice.

The 10.7MHz filter employed in my transceiver was obtained for a ridiculously low price from Birkett [3]. Another way of saving money is to roll your own - G3UUR has shown that it is possible to fabricate a high-performance ladder-type filter using the 4.43MHz crystals intended for use in domestic TV receivers [4]. Because these crystals are manufactured in huge quantities they are very inexpensive. Needless to say, there is no particular reason to avoid an IF of 4.43MHz.

On receive IC2 functions as a product detector. The recovered audio appears at pins 3 and 14 in antiphase. It is not strictly necessary to employ both outputs but doing so will result in the cancellation of any common-mode components. By the term 'common-mode' I am referring to in-phase outputs that typically result from supply line modulation. Modulation of the supply voltage can occur when a later stage - possibly an audio output chip - draws a varying current according to the level of the signal it is passing. Even though there may be a number of decoupling components present (and possibly some 'active decoupling' courtesy of voltage regulators), it is difficult to avoid this phenomenon completely.

In a receiver where there is little or no IF

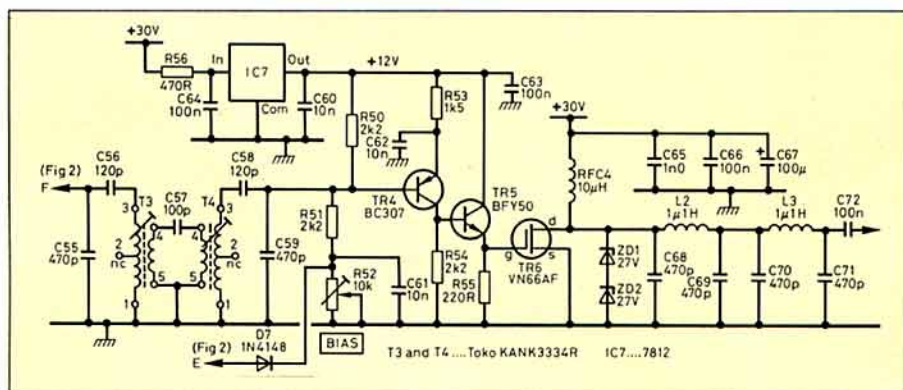


Fig 4: A simple 5W PEP linear amplifier for 7MHz. The RFC is 12 turns of 22SWG enam on a FT50-61 ferrite toroid. L2 and L3 are both 15 turns of 22SWG enam on T50-2 powdered iron toroids.

amplification, the audio stages must provide very high gain. In these circumstances it is likely that instability, even oscillation, will occur if common-mode signals are allowed to appear at the input of low-level stages, thus establishing a positive feedback loop via the supply line.

A differential audio preamplifier based around IC3 (a) and (b) raises the level of demodulated signals by 55dB. It is possible to configure a differential amplifier by feeding antiphase signals to each input (inverting and non-inverting) of a single op-amp. However, through summing the outputs of two separate amplifiers, we increase the signal to noise ratio by 3dB.

The audio stage(s) which must follow IC3 are not shown. Of the many possibilities, I chose to employ a VOGAD IC (SL6270C) which provides approximately 40dB of AGC. The VOGAD drives an LM380 audio output chip via the AF gain control. In order to help prevent audio instability, the LM380 is powered from an entirely separate voltage regulator. The output stage must be silenced during transmit. This can be achieved by placing an audio gate ahead of the output stage, or alternatively an audio chip having a mute pin (eg the Plessey SL6310C) could be used.

The transmit SSB signal is taken from pin 3 of IC2 and fed to the input of the linear amplifier. IC4 (b) in conjunction with the relay driver TR1, provides the necessary PTT switching. Instead of the usual 13.8V power supply I have employed 30V - the higher voltage being more suitable for the type of linear amplifier used (see later). The internal 8 and 12V rails are generated by a number of IC voltage regulators. My 30V PSU consists of just a mains transformer (secondary approx 21V RMS), a 5A bridge rectifier and a 6800µF reservoir capacitor. Because my transformer has beefy 6.4A secondaries the voltage drop on speech peaks during transmit, when the rig draws around 500mA, is less than one volt. An alternative PSU might comprise a smaller transformer, having a 30-35V secondary rated at 1-2A, with a series regulator comprising perhaps a TIP122 Darlington power transistor and a Zener reference.

Fig 3 shows the VFO, crystal oscillator and a switching circuit based around a CD4066 (IC6) which provides the DPDT function of S1 shown in Fig 1.

The 3.6 to 3.7MHz VFO is a standard Clapp arrangement using a JFET (TR2). Varicap tuning is employed as this avoids the need for an expensive variable capacitor and reduction drive. The coarse tune potentiometer (RV2) is a slider type - thus allowing the use of a straight frequency scale which looks more contemporary. The fine tune control (RV3) is rotary and has a range of plus or minus 5kHz. This tuning system is basically the same as that developed for the RC14 Beginner's Receiver [5]. C37 sets the HF limit (3.7MHz) while R37 dictates the range and therefore the LF limit. The calibration procedure involves adjusting C37 first (making sure, of course, that RV2 is in the appropriate position and RV3 is at mid-travel) and then, after re-setting RV2, R37.

TR3 is used in a simple Colpitts oscillator circuit with the 10.7015MHz crystal. C50

enables the output frequency to be trimmed slightly to facilitate alignment with the crystal filter passband - this allows an optimum level of carrier rejection to be obtained and tailors the audio response accordingly.

The CMOS quad bilateral switch (IC6) contains four signal gates which are controlled via pins 5, 6, 12 and 13. On receive, pins 12 and 13 are held at +12V (logic 1), thus closing gates a and d. Pins 5 and 6, which are connected to the output of the inverting op-amp IC4 (b) - see Fig 2 - are held at a potential close to 0V (logic 0), so opening gates c and b. This means that the output of the VFO will be coupled to the oscillator input (pin 5) of the first mixer, IC1 (Fig 2). Conversely, the crystal oscillator drives the second mixer, IC2.

When S3 is pressed in order to transmit, thereby reversing the potentials at points C and D, the opposite situation pertains. The CD4066 functions perfectly well as an RF switch in this application, although account does have to be taken of the through loss, which rises with frequency. Luckily, the SL6440C mixers require only 250mV of drive so a significant degree of attenuation can normally be tolerated. For instance, the 10.7MHz xtal oscillator has an output of approximately 2V peak and the CD4066 loss (nearly 20dB at this frequency) conveniently serves to reduce this voltage to the appropriate level! Surprisingly, the specification of the CD4066 published by National Semiconductors in their CMOS Databook (I have a 1978 edition) indicates that the attenuation of each gate is only 3dB at 40MHz (where $RL = 1\text{ k}\Omega$). Perhaps I should also mention that the CD4066 used in my prototype is a Toshiba device. Clearly, when using the CD4066 in RF applications it would be prudent to make some voltage measurements using either a diode probe and a multimeter, or an oscilloscope, before finalising the circuitry and/or component values.

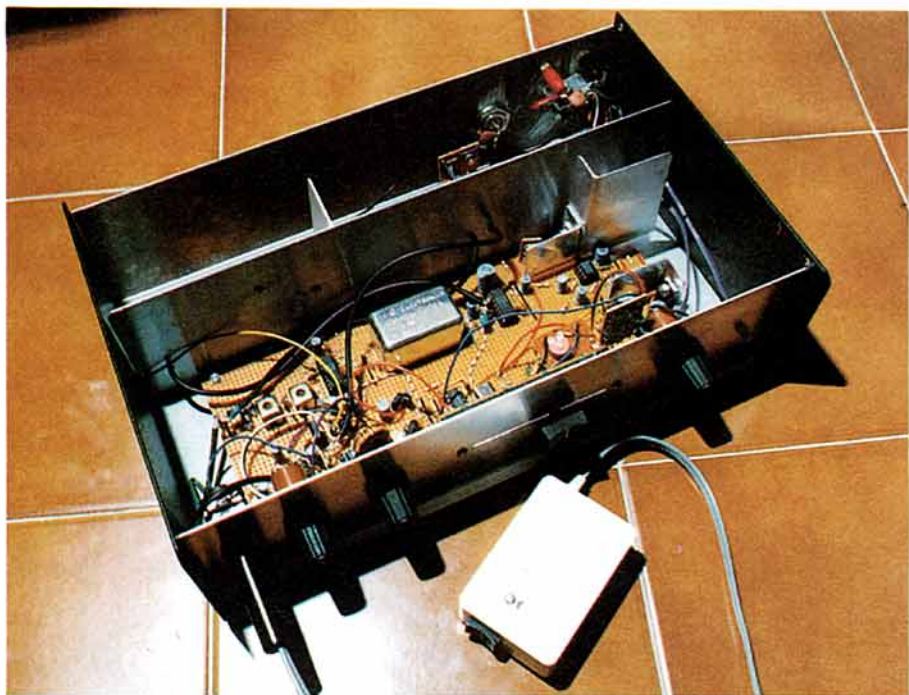
The linear amplifier (Fig 4) features a simple single-ended output stage using the popular VN66AF VMOS transistor. Much has been written about VMOS devices over the last few

years and I will therefore try to avoid too much repetition. Suffice it to say that this type of transistor has two main disadvantages - namely Rds and gate capacitance. Rds refers to the residual resistance that exists between the drain and source connections even when the device is turned hard-on. Rds varies between device types and figures are available from the relevant data sheets.

However, as a general rule the ohmic losses attributable to Rds may be minimised by using the highest possible supply voltage - ie reducing the drain current for a given power input and so lowering the voltage drop across the device. This is the primary reason for choosing a 30V supply.

The gate capacitance of an RF VMOS device is normally about 50pF and this must be taken into account when designing the driver stage (remember that the reactance of 50pF at 7MHz is only 455Ω). In the circuit of Fig 4 an emitter follower (TR5) provides the required 'slew rate' and can therefore develop the necessary drive voltage of 1 - 2V at the gate of TR6. Many experimenters have sung the praises of audio VMOS transistors which are available quite cheaply. The first point to make here is that the RF types are hardly expensive (my VN66AF cost just £2.07!). Secondly, the audio devices have a much higher gate capacitance - typically 1000pF. The circuit of Fig 5 is unsuitable for an audio VMOS transistor.

As TR4, TR5 and TR6 are direct coupled, the PA bias current is determined by TR4's base voltage. This is controlled using the preset R52 which should be adjusted to give a standing current of 60 mA through TR6 under no-drive conditions. The connection via D7 (labelled E) to the collector of TR1 (Fig 2) kills the PA bias on receive - it is important that this is done because the antenna changeover relay will disconnect the antenna from the PA during receive and, if forward biased, TR6 would probably oscillate. There is, indeed, a tendency for TR6 to oscillate whenever the antenna is incorrectly matched - the good news is that TR6 does not appear to be



harmful by the self-oscillation! Constructors who wish to reduce the possibility of PA instability might like to consider a push-pull output stage using a pair of VMOS devices. Push-pull configurations are attractive because they obviate the need for an uncoupled drain choke, thus removing a potentially troublesome reactance. Recently, G3PCJ [6] has had published some reasonably straightforward push-pull VMOS circuits, albeit for higher power levels.

The input signal to the PA is bandpass filtered by T3, T4 and C56-59. The output lowpass filter comprising L2, L3 and C68-71 attenuates any harmonics. ZD1 and ZD2 combine to produce a 54V Zener which helps protect TR6 against excessive voltage. I have constructed this linear, which develops an output of 5W PEP, on a strip of Veroboard measuring approx 40 by 180mm. An aluminium screen isolates the PA from the rest of the transceiver and also serves as a heatsink for TR6. A word of warning here - it is the drain and not the source which is connected to the VN66AF cooling tab. You must therefore use an insulated mounting for TR6.

IF AND IMAGE CONSIDERATIONS

FINALLY, WE RETURN TO THE choice of IF. I stated earlier that in the case of single-conversion transceivers, the higher the intermediate frequency the better.

As an example, let's assume that we wish to build a transceiver for 21MHz and have

acquired a 455kHz crystal filter for this purpose.

In order to receive a transmission on 21.200MHz the VFO could be set to 21.655MHz (21.655 - 21.200 = 0.455). The image frequency will be 22.110MHz (21.655 + 0.455 = 22.110). Readers with long memories, or perhaps those with an interest in vintage equipment, might well point out that valve receivers such as the legendary AR88 and the earlier Eddystone models offered an acceptable level of performance despite their use of a single IF in the range 300 to 600kHz. That may well be the case, and in the final analysis it is simply a matter of personal judgement as to whether the relatively poor suppression of signals at the image frequency, a deficiency noted especially when listening on the higher frequency bands, can be tolerated.

However, the situation becomes somewhat alarming when we consider what might happen on transmit. In our example, the first mixer is required to generate a DSB signal close to 455kHz which is then fed through the crystal filter to produce SSB at 455kHz - so far, so good. The second mixer is now coupled to the VFO and this generates the 21.200MHz transmit signal by subtracting 455kHz from 21.655MHz. Unfortunately, this mixer also produces another, equally strong, SSB signal at 22.110MHz (21.655 + 0.455 = 22.110).

Clearly, the task of designing a filter to precede the linear amplifier which will pass the wanted signal at 21.200MHz and yet attenuate the 22.110MHz 'image' by at least

60dB is going to prove quite formidable. Furthermore, even if you were successful, it is almost certain that the circuit would have a very narrow passband. This, of course, implies that it would need to be completely retuned for operation in another part of the band.

It should not be assumed from the above that an IF as low as 455kHz is completely unsuitable for use in any single conversion design. A transceiver for Top Band (1.8MHz) might well use 455kHz because the image spacing (910kHz) is a much larger proportion of the transmit frequency, -making the construction of the necessary filter a practical proposition.

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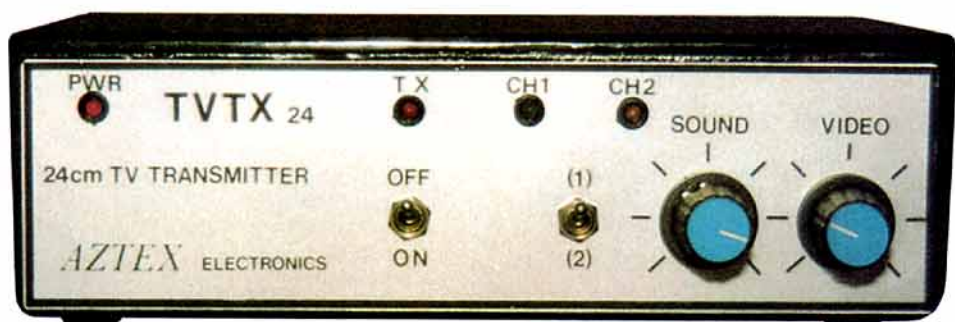
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Amateur TV Equipment

The Aztex TVTX 24 FM Tx and the Ulna 23-24 GaAsFET Pre-amp

by Mike Wooding G6IQM



THE AZTEX 24cm FM ATV TRANSMITTER was first seen at the 1990 Leicester Show and created a lot of interest. Since it was first advertised in *CQ-TV*, I have often been asked for details of this unit so I contacted the Severnside TV Group, through whom it was marketed, and arranged to obtain one for review. At the same time I also requested a look at one of their G4BVK 24cm preamplifiers.

THE AZTEX TVTX 24 FM ATV TRANSMITTER

DEVELOPMENT INFORMATION

According to the designer, Ken Stevens G4BVK, the need for a stable output was one of the governing factors, so the SP5060 Phase Lock Loop chip was an obvious choice. Using surface-mounted components was another way of maintaining stability. The video pre-emphasis network, although based on the standard CCIR circuit, was designed to give an extra HF lift to overcome the HF losses within the modulator. DC restoration of the signal was also deemed necessary before injection into the modulator, and the circuit adopted to achieve this is very effective in preventing the video content from altering the black-level position.

The two sound inputs are actively mixed using a TL072 op-amp before they are fed to the modulator. There is a separate PCB-mounted preset for adjusting the line input only, the front panel sound control adjusting the composite level of both inputs. There is also a subcarrier injection level preset provided on the PCB.

DESCRIPTION

The unit comes fully assembled in a black-painted diecast box measuring 188 x 120 x

57mm. A professionally produced front panel features four LEDs, one indicating the connection of the DC supply, another indicating transmit and two more indicating which channel is selected. There is a main ON/OFF switch and a CHANNEL select switch. Two potentiometers are provided, one for SOUND and the other for the VIDEO deviation. On the rear of the transmitter are the various connecting points. An N-type socket is provided for connection to the aerial, a BNC socket for the video input, a phono socket for the audio line input and 1/4in socket for the microphone. The DC input is a 3-pin plug with a matching line-socket and lead provided.

Internally the transmitter is neatly laid out with the main printed circuit board bearing the audio amplifier, modulator and subcarrier generator circuitry and the video circuits. This circuit board is held in place with four nuts, bolts and spacers, facilitating removal for future servicing needs.

A smaller diecast box occupying approximately one-third of the main case contains all the RF circuitry. This has the advantage of

providing a further level of screening between the baseband and RF sections of the transmitter. The RF output N-type socket is mounted through the case directly into the inner box and is soldered directly to the PCB, leaving no RF cables floating around inside. Interconnections between the RF box and the main PCB are by means of several feed-through terminals carrying the baseband signal, power supply and frequency switching control signals. Although a little intricate, removal of the RF assembly and the RF circuit board for servicing can be achieved with care.

Three user adjustment points are provided inside the transmitter: a preset potentiometer for audio subcarrier injection level, a trimmer capacitor for the audio subcarrier frequency and a preset potentiometer for the line audio level. Supply protection is by a miniature wire-ended fuse soldered between two posts on the PCB.

BENCH TESTS

Two transmit frequencies are available on the transmitter, selectable by the CHANNEL toggle switch. Knowing that the unit has a crystal-controlled PLL exciter I expected the frequency stability to be good, and it is. The review unit exhibited a downward drift of only 2200Hz over a 30-minute period.

The RF output power was monitored over a 30-minute period at 1249MHz. After an initial 20-minute period during which the power output dropped 0.37W (0.65dB) the output remained to all intents and purposes constant at 2.34W. A similar check was carried out at 1255MHz, the switch-on power being slightly higher at 2.84W with the final output power settling at 2.54W.

MANUFACTURER'S SPECIFICATIONS

Frequency	Channel 1, 1249MHz Channel 2, 1255MHz
RF output power	2.5W (typical)
Harmonics	less than -50dBc
Modulation system	FM with built-in pre-emphasis
Audio subcarrier	pre-set to 6MHz at least 17dB below carrier (variable with deviation setting)
Video input	1V peak-to-peak into 75 ohms
Audio inputs	dynamic microphone, adjustable line input (VCR etc)
Power consumption	1.6A at 13.8V

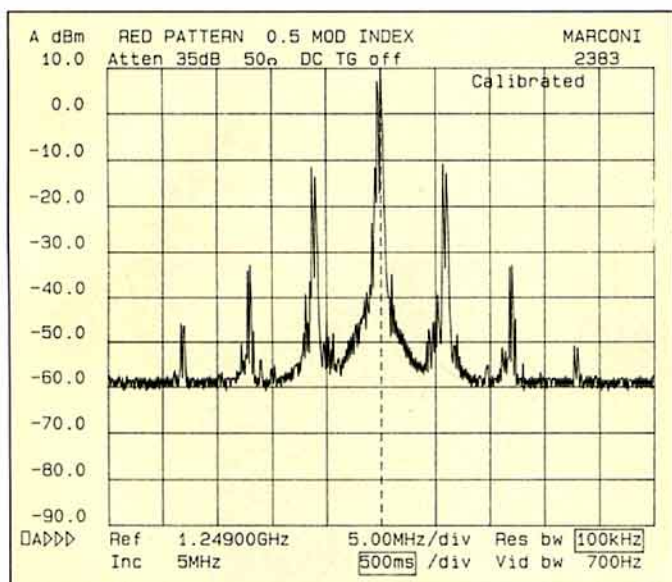


Fig 1: The spectrum obtained using a plain red pattern.

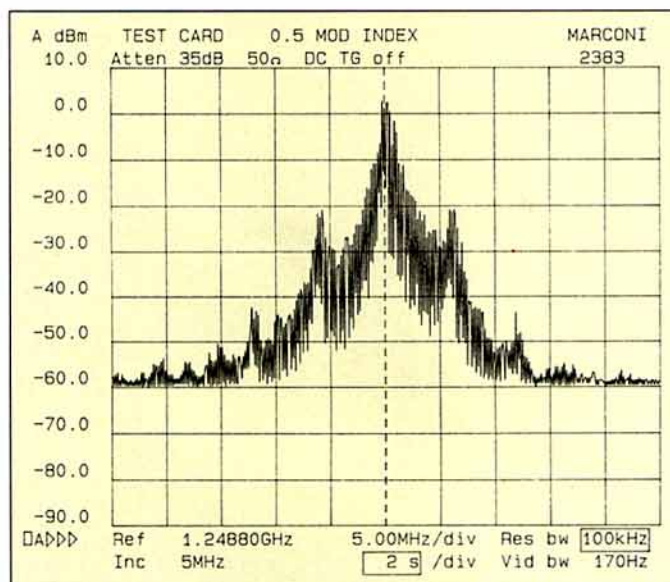


Fig 3: The spectrum obtained using a Philips PM5534 test card.

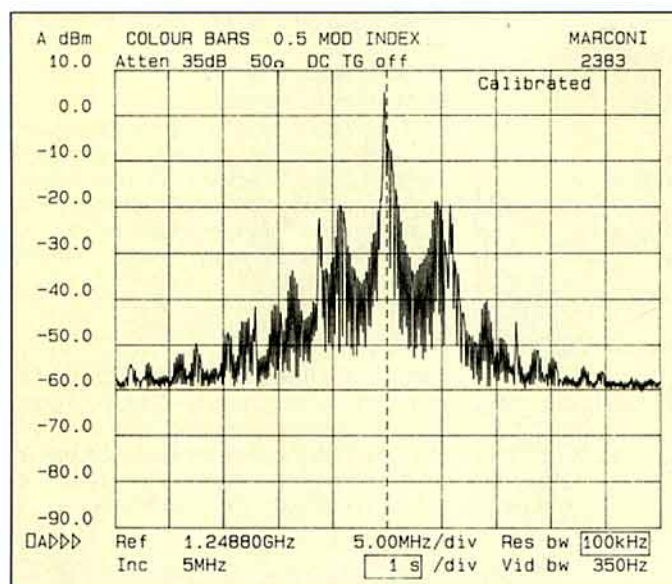


Fig 2: The spectrum obtained using 100% saturated colour bars.

The harmonic content of the unmodulated output was very low indeed, probably in the main due to the inherent out-of-band rejection of the SC1043 PA output device. The second harmonic was measured at slightly less than 50dB down on the carrier. Third and subsequent harmonics were not detectable above the -75dB noise floor of the analyser.

VIDEO AND AUDIO CHARACTERISTICS

A test system has been developed by the BATC for ascertaining a modulation index of 0.5. Apply a 5MHz sinewave to the video input and, viewing the output on a spectrum analyser, adjust the video amplitude (deviation) from the signal generator so that the sidebands coincide with the recommended modulation index of 0.5. Using this system the output from the signal generator into the transmitter was then measured and this level used as the reference output level from the Philips TV pattern generator for the spectrum plots. Fig 1 shows the spectrum obtained using a plain red pattern, Fig 2 the spectrum using 100% saturated colour bars and Fig 3

the spectrum with a Philips PM5534 test card. The audio subcarrier generator, unless otherwise specified, is set to 5.9996MHz for UK use. However, the subcarrier oscillator trimmer capacitor is accessible with the unit's cover removed, and the subcarrier can be easily reset to whatever frequency is needed for Continental DX. At maximum video deviation the subcarrier level was measured at 17dB below carrier. However, as the video deviation is reduced (using the front-panel VIDEO control) the relative difference becomes greater, and at minimum video deviation the subcarrier was measured at 32dB below carrier (dBc). With a standard video input level of 1V p-p the front panel VIDEO control needed to be set at approximately 50% in order to achieve a normally deviated picture; at this setting the audio subcarrier was measured at around -24dBc, which proved to be quite adequate for good audio with P5 contacts. I felt it necessary to adjust the internal subcarrier injection control to bring the relative level back to -17dBc at this VIDEO control setting, and this provided very good audio fidelity commensurate with picture reception. If the input video level to the transmitter is adjusted such that the VIDEO control on the transmitter has to be set towards fully clockwise in operation, then the audio subcarrier level will be satisfactory without any internal adjustment.

ON-AIR TESTS AND CONCLUSIONS

Overall I was very impressed with the workmanship and presentation of the transmitter. Upon receipt it was simply a matter of con-

necting 13.8V, plugging in the camera and microphone, connecting the aerial, switching on and adjusting the video and audio controls. The Aztex TVTX is ideal for those amongst us who are not of the home-brewing fraternity. Furthermore, the output level of around 2.5W is enough to drive a 2C39A valve linear to quite a useful output (in my case to approximately 60W). The colour handling characteristics of the unit gave excellent results, as did the audio response, when tested over a P5 path between myself and G0HOV.

My only criticism is the use of the soldered-in PCB mounted fuse. Whilst obtaining and changing this should not be a problem, some users might prefer a fuseholder. Finally, suffice it to say that I am so impressed with the transmitter that I am now using one myself.

THE AZTEX ULNA 23-24 GAASFET PREAMPLIFIER

DESCRIPTION

THE ULTRA LOW NOISE preamplifier comes in a blue hammer-finished die-cast box measuring 110 x 60 x 30mm, with N-type input and output sockets mounted one each side. NOTE - as stated by the manufacturer, this enclosure is not water-proof and needs to be mounted inside another weather-sealed enclosure for external/mast mounting.

The small printed circuit board is secured inside by solder tags, fixed to the PCB and secured on two of the N-type socket fixing bolts on each side. The AFT10135 GaAsFET is mounted on a vertical PCB screen soldered to the main circuit board. A horizontal brass screen is soldered to the vertical PCB screen and is also clamped to the output end of the box by two of the screws retaining the output socket. The input and output trimmer capacitors are mounted at the respective sockets and a preset bias potentiometer is located on the main PCB. The DC supply is fed into the box by two insulated solder terminals and a reverse-polarity protection diode is provided.

BENCH TESTS

The two plots shown in Figs 4 and 5 show

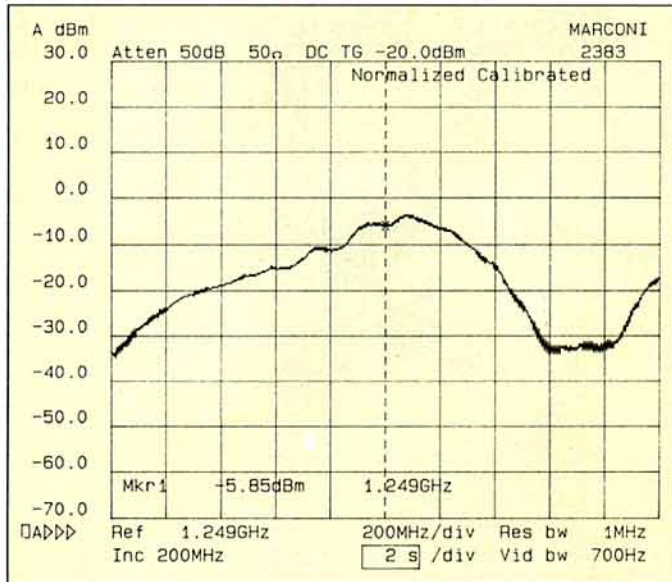


Fig 4: Gain over frequency range, 1249MHz to 2240MHz.

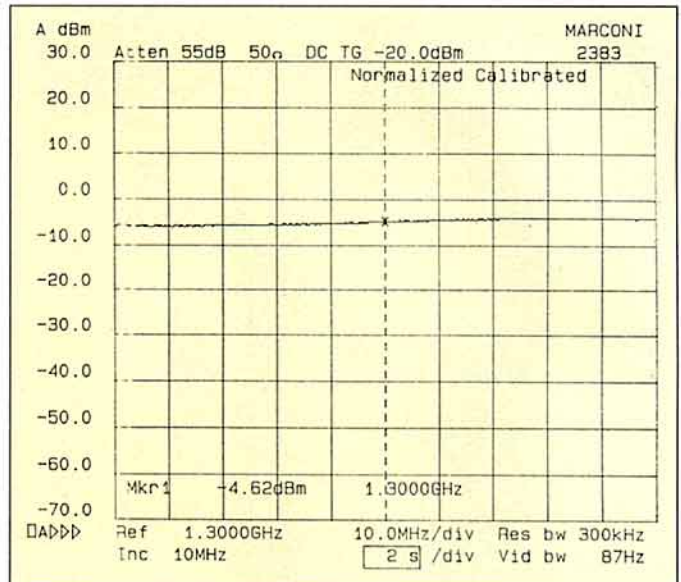


Fig 5: Gain over frequency range 1250MHz to 1350MHz.

gain versus frequency. Fig 4 shows the gain over the frequency band from 1249MHz to 2240MHz. The reference input level from the tracking generator of the spectrum analyser was -20dB and the centre frequency of the plot is 1249MHz. It can be seen that the 0dB gain points are approximately 600MHz and 1700MHz and the -3dB band is approximately 1150MHz to 1500MHz, with the rejection at 700MHz being in the order of 11dB.

Fig. 5 covers a frequency band from 1250MHz to 1350MHz, with a centre frequency of 1300MHz. Over this frequency range, essentially the 23/24cm band, the response is almost flat. The reference input level from the tracking generator is again -20dB and the gain at 1300MHz was measured at 16.1dB. The gain at 1249MHz was measured at 15.5dB and at 1318MHz it was 16.4dB.

MANUFACTURER'S SPECIFICATIONS

Typical gain	17dB
Noise figure	1dB
Bandwidth	1250 to 1350MHz +/- 1dB
Rejection	8dB at 700MHz
C supply	7V to 18V

figure means that the 15.5dB of gain appears to be a great deal more when compared against results obtained from other noisier preamps with perhaps higher gain figures.

My overall impression of the preamplifier is of a sound, well made unit with very good performance, and I wholly recommend that anyone requiring a preamp for 23/24cm (that just about encompasses everyone working 24cm ATV to my mind) should seriously consider this unit.

ON-AIR TESTS AND CONCLUSIONS

The flat, even response of the preamp over the entire 23/24cm band meant that I was able to tune to signals at both the RMT2 repeater input and output frequencies (1249 and 1318.5MHz) without any loss of preamplification. Also, the very low claimed noise

AVAILABILITY

ENQUIRIES ABOUT these products should go to: Aztex Electronics, 20 Coberley, Footshill Road, Hansham, Bristol, BS15 2ES; tel: 0272-677005. The Severnside TV Group can be contacted at 15 Witney Close, Saltford, Bristol, BS18 3DX. Tel: 0225 873098. □

Supplementary Information

**G3TSO
Miniature
Transceiver**

THE G3TSO MINIATURE 80 METRE transceiver was primarily designed as a one-off project to see how small a single band transceiver could be made. It was not designed as a kit type project.

As the interest in the project has grown, a number of companies have started to offer the transceiver as a kit. In order to have success in constructing any of these 'kits' the following notes should be read.

1. R56 (33Ω) gives the maximum gain for IC5, if this is too much, ie, unstable, increase R56 up to a maximum of 120Ω.
2. RL2 and RL3 can be 12V types or two 6V types connected in series. On the component layout, the wiring shows connections

for 6V types. If you use 12V relays, connect RL2 and RL3 in parallel.

3. C71 is mounted under the pcb.
4. C89 is mounted under the pcb.
5. The DC connection on the mic skt is for a 3-wire electret mic, a 2 wire type can be accommodated by connecting DC directly to the mic input pin. the unused pads on the pcb are provided for this purpose. A DC blocking capacitor must be used as per electret data sheet.
6. R12 has been connected to the wrong 6V line, it should be removed and replaced under the pcb from the drain of Q1 to pin 8 on IC1. This ensures the receive and transmit frequencies are the same. Switching Q1 pulls the VFO.
7. Pin 4 on IC3 should be grounded, this was omitted on the circuit diagram.

IMPORTANT NOTICE REGARDING PCB

PCBs ARE AVAILABLE FROM a number of sources, including the author. Most boards are drilled with a single hole size of 0.8mm, this is the majority hole size, some holes however will need to be enlarged to take

certain components. Drill the hole to the correct size, do not drill them excessively large.

Ensure before placing components that they have sufficient clearance from the groundplane, use a 'VERO Cutter' or an old 0.125in drill to make the clearance larger if required.

Check against the circuit diagram to ensure that all components that are shown connected to ground are soldered to the groundplane directly. There are very few ground tracks on the underside of the PCB. Do not connect anything to ground that is not shown grounded on the circuit diagram, ie coil taps. When mounting the PCB use small nylon stand-offs if required, so as not to short anything to the case.

Do not mount components on long leads, where possible all leads should be bent at right angles and components should be mounted flush with the PCB; ICs can be raised no more than 1/32in to ensure that the pin shoulders do not contact the groundplane. The use of IC sockets is not recommended.

Do not use low wattage soldering irons or those with huge bits. A hot pencil bit solders quicker and more efficiently without raising the track. □

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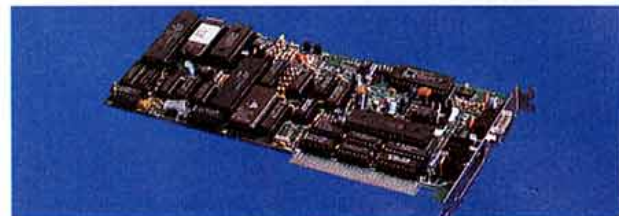
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Loop Antennas

Facts, Not Fiction

by A J Henk, C. Eng., M.I.E.E., G4XVF

NOT ANOTHER LOT of words on loop antennas, surely? So much has been written and said on the subject - at least in the amateur journals - but how much of it is of any use to the serious radio amateur? This article is intended to clear away some, at least, of the intellectual fog surrounding these devices and to address areas which have been generally neglected. For instance, how efficient are they, how effective are they (not the same thing) and how can they be made better?

Notwithstanding the proliferation of references to the subject, it is not intended to provide an extensive list of papers; others have already done this. The references which are included have something useful to say appropriate to this article.

DEBUNKING THE MYTHS

LET'S MAKE ONE THING CLEAR from the outset: there is no mystique of any sort associated with loop aerials. They obey the standard laws of physics like anything else and the principles are quite simple. Anyone who tries to make it sound otherwise and wraps it all up in arcane language or presents it as a 'black art' should have his credibility suspected immediately. It is hoped that this article will explain the operating principles, without too many shortcuts, and in language which is easily understood by anyone with sufficient technical knowledge to have passed the RAE. There will be some maths presented but, again, the simplest and most basic knowledge of AC theory (RAE level) will be quite adequate to reveal many of the loop's innermost secrets.

WHAT IS AN AERIAL?

AN AERIAL (OR ANTENNA, if you must use the Americanism - both terms will be used synonymously here) is a device for coupling an electrical circuit to a medium through which radio waves propagate, in our case free space, or vice-versa. It was the development of this component (by Marconi) which took wireless communication out of the realms of a laboratory curiosity and turned it into practical reality. Without the 'elevated electrode' the signals don't go very far. A pair of aerials can form a simple four-terminal transmission network: four terminals because you feed the signal into one pair and a smaller version of it emerges from the other pair. Such a network is reciprocal, that is to say it works both ways.

In the first of a two-part article, A J Henk takes a factual look at how to quantify the real performance of a loop antenna. Next month: do loop antennas really work as well as is frequently claimed?

Any two antennas, of any sort, will exhibit this reciprocity, a feature which has been of great value to the author during the study of loops.

Reciprocity works like this. Firstly the two antennas must be correctly matched to the transmitter and the receiver respectively and this matching must be preserved. If this is the case and you feed, say, a one-watt signal into one aerial and then find that you get one microwatt from the second (receiving) antenna, you can be sure that if you now reverse things and feed your one watt (matched, of course) into the second antenna you will have a microwatt now out of the first. There are no exceptions to this rule.

Most common transmitting antennas are 'electric' or 'E-field' devices, and work basically by making as large an electrical disturbance as possible across a chunk of space. The bigger the chunk the better the aerial because the disturbance is more widespread. This is what you might expect; after all, particularly at low frequencies, big aerials work better than small ones if everything else is the same. Extracting big performances from little antennas is the aim of many amateurs, particularly in the UK, and smallness is one of the main attractions of the loop.

Where there is an oscillating electric field, there is also an oscillating magnetic field produced by it in space. A radio wave must contain both magnetic and electric components in order to exist. In the case of the loop, a strong magnetic field is generated by passing a heavy current through the radiating conductor and this magnetic field then generates a corresponding electric field in space, thus providing the two elements needed. For this reason the antenna is sometimes referred to as a 'magnetic loop'.

WHAT IS A LOOP AERIAL?

LET'S STOP FOR A MOMENT and have a look at loops from another perspective. Firstly,

what do we mean by a 'loop aerial'? In this article the term is taken to refer to a loop of one or more turns of conductor whose dimensions are small compared with the wavelength of the signals being transmitted. It may be circular, square or any other shape. Anything larger than about one-eighth of a wavelength across is becoming a bit big for this definition; such devices as 'delta-loops' are a different kettle of fish and this article does not apply to them.

Magnetic loop aerials are as old as wireless itself; indeed some of us remember very clearly the frame aerials used quite effectively by the early broadcast receivers before they became modernised by the availability of efficient magnetic materials and turned into ferrite rods (indeed the US term *loopstick* testifies to their origins). They have not gained widespread popularity for transmitting because of the great difficulty of achieving high efficiencies, but for receiving they have many desirable properties. It should be noted that, even though reciprocity applies (yes, also to ferrite rods) you cannot just interchange transmitting and receiving aerials and achieve the same communications quality or performance. However, that's another story.

Loops which are used for transmitting do not generally use ferrite and therefore need to be larger to be effective, and they have fewer turns, typically below five and quite often only one. Whereas you can't necessarily transmit on a receiving loop, you can normally receive very well with a transmitting unit. This, of course, applies equally to E-field aerials.

THE LOOP AS A RADIATOR - RADIATION RESISTANCE

WE HAVE SPENT QUITE enough time and space now looking at aerials in general and seeing how the loop fits into the scene - let's now examine it more carefully and see how it works. There is a simple but very useful concept which we can use to help us, and that is the idea of 'radiation resistance'. This can be used in connection with any antenna but here we are going to restrict ourselves to the loop. As we have seen, this works by pumping as much RF current as we can muster through a conductor, thus generating our oscillating magnetic field in true Faraday tradition. In order to do this we need RF power and this normally comes from our transmitter - in the interests of simplicity, let us assume a 100W rig. Let us also assume that the transmitter, feeder and aerial are all properly matched so that all of our 100W goes into the

LOOP ANTENNAS

aerial system. With any luck, some of this power will be radiated off into space - the rest disappears into the system losses and is dissipated as heat.

If we have been very lucky and manage to radiate 10 out of our 100 watts, 90 must go in loss resistances of one sort or another. Note that all losses are resistive, as pure inductance or capacitance cannot dissipate power. Since power only dissipates in resistance, it is seductive to consider the *radiated* power also as being absorbed into a resistance, although this is not a real resistance, just a concept. Our circulating current might be, say, 10A. We know from basic theory (power= I^2R) that, because we are losing 90W, our total loss resistance (from all sources) must be 0.9Ω , as $10^2 \times 0.9 = 90W$. Therefore why not consider the other (radiated) 10 watts as being in a resistance of 0.1Ω ? (Again $10^2 \times 0.1 = 10W$) This is called the 'radiation resistance' and every antenna has some. It must be remembered that, because this is not a *real* resistance, it is not an embarrassment (not in an aerial anyway) and, indeed, our aim is to push as much power into it as we can. It is therefore in our interests to achieve as high a value for this radiation resistance as possible. Low values are bad news.

Once we know the radiation resistance of our antenna and the current flowing through it (ie that flowing in the loop), we can calculate the power actually radiated and, since we know how much power we are feeding in, the efficiency follows very easily. More of this later - it is a key point in assessing the performance of a magnetic loop.

BASIC OPERATION

WE CAN NOW START TO LOOK at the antenna in a little more depth and see what makes it tick. Fig 1a shows the physical arrangement normally employed, stripped of all the non-essentials. It is shown for a single-turn loop but the principles are the same irrespective of the number of turns. A conductor is bent into a circle (or some other suitable shape) and the free ends connected across a capacitor. The arrangements for connecting this to the transmitter or receiver are discussed later. This forms a tuned circuit, resonant at the operating frequency and can be considered, to a high degree of accuracy, as comprising three simple components, as shown in Fig 1b. The inductance L is that of the bent conductor, and the capacitance C is that of the tuning capacitor (plus any stray capacitance) which resonates with L at the desired frequency F. The third component is resistive and represents, as one component, all the resistive parts of the system, or R_t (for total resistance). R_t will mainly be losses of one sort or another (no circuit being perfect) but there is a further non-lossy part of this component which we mentioned earlier, the radiation resistance, R_r .

In connection with these resistive components it should be realised that they are not all physically in series as shown in Fig 1. The conductor losses are clearly series losses, but losses in the capacitor dielectric appear across the capacitor terminals as a shunt resistance. Even so, we can still use a series resistance to represent these parallel losses by giving it a value which will have the same

effect on the circuit as the parallel losses themselves, and doing it this way brings great simplicity to the analysis. Also, in with this series resistance, we can include any losses which occur outside the physical confines of the loop, such as ground losses (which will affect the loop performance and Q) and therefore bring all losses, from whatever source, together in a single component. This keeps life very straightforward.

It is our avowed intention to make as much current as possible flow in this circuit. This will, of course, occur at the resonant frequency of L and C, given by

$$F = \frac{1}{2\pi\sqrt{LC}} \quad (1)$$

This current flows equally through all the circuit elements (their being in series) but actual power appears only in the resistive part as you cannot dissipate power in a pure reactance. Therefore the total power in the system is

$$P_t = I^2 R_t \text{ watts.}$$

If a transceiver, for example, is correctly matched to this system, then P_t is equal to the power output of the transmitter, let's say 100W.

Now, R_t is the total resistance of the circuit and is made up of many different parts. All but one of these parts will correspond to losses of various sorts and can be considered as forming a single aggregate loss resistance R_r . The one remaining non-lossy part is - yes, you've guessed it - our old friend R_r , the radiation resistance. Therefore we can say, because the total loss is the sum of all these separate parts,

$$R_t = R_r + R_r$$

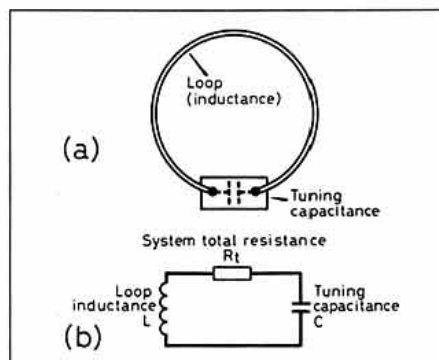


Fig 1: a) Loop antenna arrangement, b) Equivalent circuit.

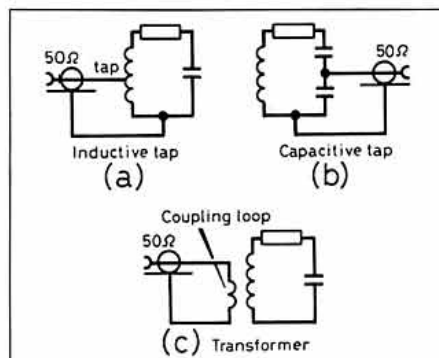


Fig 2: Methods of coupling to a loop antenna; a) inductive tap, b) capacitive tap, c) transformer.

EFFICIENCY

POWER DISSIPATED IN R_r is, of course, lost as expensively generated heat. However, power 'dissipated' in R_r is our precious radiated power and we cherish it tenderly as that is precisely what we are trying to achieve with our antenna. Suppose we radiate 25 out of our 100W, then our aerial is 25% efficient. The other 75W (ie three times as much) goes in the loss resistance. This means that R_l must be three times as big as R_r in this example since I and therefore I^2 is the same value for both R_l and R_r . We can write a simple equation to define our efficiency if we know these resistance values:

$$\text{Efficiency } (\eta) = \frac{R_r}{R_r + R_l} \cdot 100\% \quad (2)$$

We can now define the term 'efficiency' as the proportion (percentage) of the power fed to the system which is actually radiated. For transmitting, this efficiency is obviously of great interest because you will need to pump 1000W into an antenna which is 10% efficient in order to achieve the same results as 100W into a 100% efficient radiator. There's money in there somewhere, as always. Notice that we have not needed to bother with L or C in arriving at this conclusion. That is not to say that they don't affect efficiency, far from it, but they do it by altering the values of these resistances and the current flowing through them.

COUPLING THE RADIO TO THE LOOP

LET'S TAKE A BREAK FROM the theory for a while and look at another practical aspect of our aerial. So far we have not considered how best to connect, or couple, the transmitter or receiver to the loop. Whilst obviously very important, it is in practice not at all difficult. There are three basic methods, all of which have one thing in common: they form an impedance matching function between the transmitter feeder and the resonant circuit. They are shown in Fig 2. It is assumed that 50Ω coaxial feeder is used although other types can be accommodated. It is possible to achieve a virtually perfect match at a spot operating frequency with any of these coupling systems.

The **inductive tap** method (Fig 2a) is quite convenient; simply connect the coax outer to the electrically neutral point on the loop (this should be the mechanical centre if the construction is symmetrical) and move the inner along the loop conductor until the VSWR at resonance becomes 1:1. If you are actually doing this in practice you will find it necessary to move, re-tune, move, re-tune and so on until it reaches the right point. This is not difficult though it might be a bit tedious.

Capacitive tapping (Fig 2b) is similar in principle to inductive tapping but is far less easy to achieve and it is less easy to synchronise the feeder connection point to the electrically neutral point. The author is not aware of any practical transmitting systems using this method. It is worth noting, in connection with the electrically neutral point, that the system will work wherever the connection is made but, if it is not at the neutral point,

current will flow down the feeder and this will introduce performance differences which are not readily calculable and, more importantly, will introduce extra losses.

Transformer coupling (Fig 2c) is one of the most popular methods and involves connecting the radio equipment to a small loop which is placed near to the main conductor, the arrangement acting as a tuned transformer. The small loop can be moved in and out to affect the matching, and a position will be found at which the correctly matched situation results in a precise 1:1 VSWR at the selected frequency.

It is a happy coincidence that, with any of these coupling methods, the matching condition stays much the same over a very wide bandwidth. That is to say, if you change frequency or frequency band you will have, of course, to re-tune the loop but the coupling will remain correct. For those interested in the reason for this, a useful qualitative treatment is given in [1] (part two).

RADIATION RESISTANCE - HOW MUCH?

MUCH REFERENCE HAS BEEN made to radiation resistance, but this concept is only useful if we know what the value is in real engineering units, like Ohms. Fortunately, it is a very simple matter to calculate it for a loop of any shape. It depends only on the area of the loop ($=\pi r^2$ for a circular loop of radius r), the number of turns N , and the frequency. If the frequency is expressed as a wavelength, no units need be specified provided the same are used for wavelength and area. The simple formula is:

$$R_r = 320 \cdot \pi^4 \cdot \left(\frac{A}{\lambda^2}\right)^2 \cdot N^2 \Omega \quad (3)$$

where A is the area and λ is the wavelength, both in the same units. N is the number of turns.

This is true for any shape of loop.

For example, take a single turn loop, 1 metre in diameter, at 10MHz. Here the wavelength is

$$\lambda = \frac{3 \cdot 10^8}{10 \cdot 10^6} = 30 \text{ metres}$$

and the area is

$$A = 0.5^2 \cdot \pi = 0.785 \text{ square metres.}$$

Since $N = 1$ for the single turn, the radiation resistance is

$$R_r = 320 \cdot \pi^4 \cdot \left(\frac{0.785}{30^2}\right)^2 = 0.0237 \Omega \quad (23.7 \text{ m}\Omega)$$

Note that 23.7 milli Ω is not a large value and the problem of making enough current (65A) flow in this to radiate 100W of RF can be appreciated.

A graph showing R_r against size for most practical loop sizes is given in Fig 3.

THE MISSING LINK

WE HAVE HAD A BRIEF (qualitative) look at coupling the transmitter into the loop and we have seen how we can determine the radiation resistance. We still need to know more,

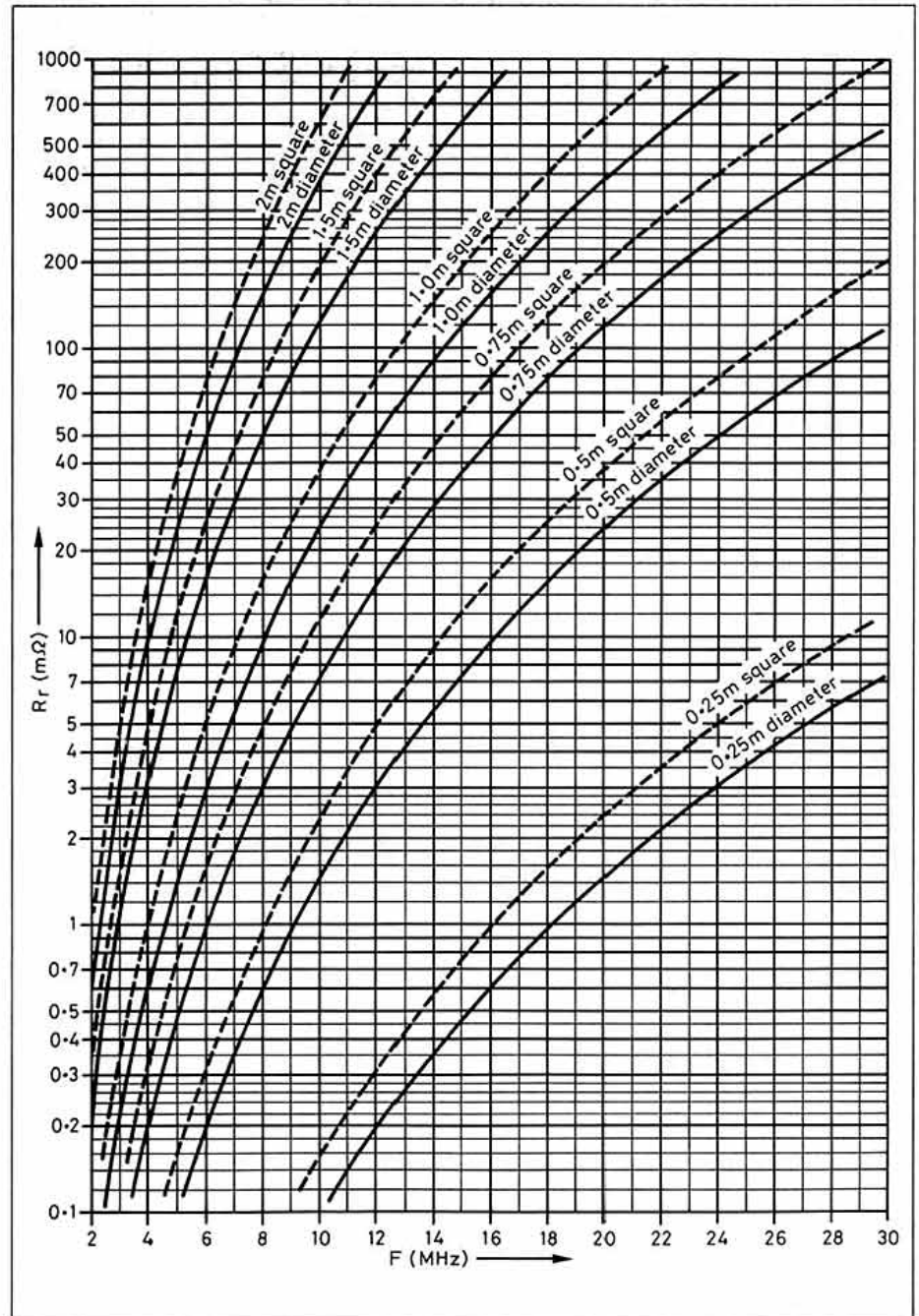


Fig 3: Radiation resistance of square and circular loops.

though, before we can claim to have a full picture of how the system works. What happens between the RF feeder and the radiation resistance? Here we need to consider the loop inductance, the tuning capacitance and our loss resistance. It is interesting to note that the physical loop of conductor serves two different electrical purposes. One is to provide the radiating action (R_r , the aerial function) and the other is to provide inductance L for the matching function we are now going to examine. This is where everything finally comes together.

Returning to our diagram (Fig 1b), we have a standard tuned circuit. The loop provides the inductance L , the value of which can be deduced in a number of ways. The loop dimensions are, particularly at low frequencies, generally chosen to maximise R_r , and the resulting inductance accepted whatever its value is. This is not always the case, but happens far more often than not. The induc-

tance value can be measured on a bridge or other inductance meter, it can be calculated (see opposite) or it can be derived when it is resonated at a known frequency by a known capacitor using the relationship:

$$L = \frac{1}{4 \cdot \pi^2 \cdot F^2 \cdot C} \quad (4)$$

where L is in Henries, C is in Farads and F is in Hz.

Because the circuit is resonant (at our operating frequency), we know L , C and F . The relationship of Equation 1 applies, of course. What we don't know is the resistive component. We know part of it, though, because we can calculate R_r from Equation 3, which only leaves the loss resistance, R_l .

... to be continued

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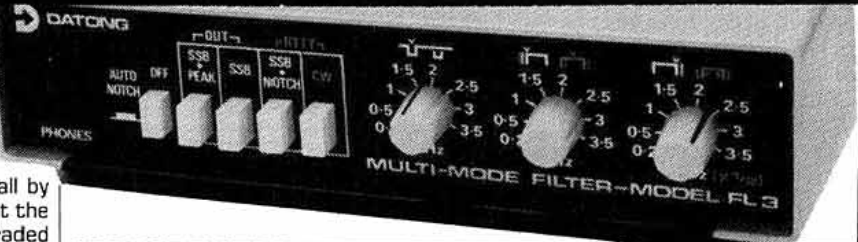
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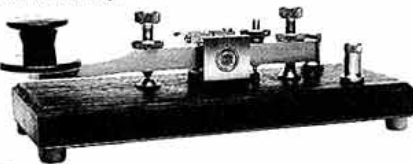
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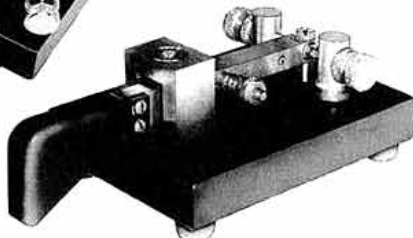
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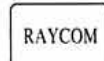
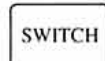
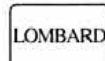
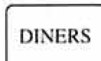
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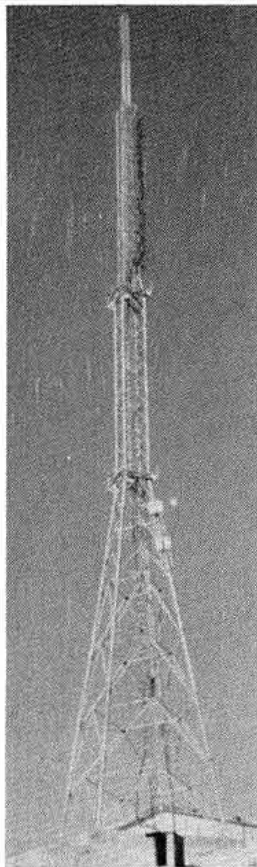
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EVERY SO OFTEN AMATEUR RADIO gets a really good dose of favourable 'public relations' coverage by the media. The latest, of course, has been Helen Sharman's mission which included a real boost for the hobby. One of the best aspects of the project was the encouragement given to young people to get interested in amateur radio through the JUNO project. We continue to hear examples of schools and individuals wanting to get into amateur radio through their participation in the JUNO project.

Some indication of the enthusiasm generated by activities of this sort in the young is illustrated by Richard Ensign in May's *AMSAT Education News*. This is devoted almost entirely to an Australian's school's experience with Mir, in particular the efforts of VK3CFI and her students at Western Victoria, Australia. Maggie had tried for two years for a contact with Mir on 2m FM, but it was not until January 1991, that she achieved a voice contact with U2MIR, who subsequently played a leading part in the JUNO mission. She followed this up with a proposition that a Soviet cosmonaut should speak to a group of school children. On 14 February, a group of about 50 parents, teachers and students gathered at Maggie's home to join in the history-making event. Some 21 children spoke to the cosmonauts during three orbit passes while Mir was in range for about ten minutes each time. It is believed to be the first radio contact of its type in the western world. Maggie said: "The students are still working through their experience - it has made quite an amazing impact. Their horizons and thoughts have been broadened beyond belief. A lot of kids in a very small town now know a heck of a lot about satellites, space, cosmonauts and the human side of these space pioneers". This event got much coverage in several major Australian newspapers and on news and talk programmes on radio. Tammy Fleming (15), summed up the general enthusiasm by her comment "The best 10 minutes of my life!".

One of the difficulties of getting involved in amateur radio satellites is the lack of literature for the newcomer to this mode. The well informed radio amateur will have little difficulty in extending his knowledge and equipment to cover satellite activity. However, those who are new to amateur radio and who want to participate in satellites will find the going difficult and frequently disappointing.

BOOKLETS

I HAVE JUST HAD the opportunity of reading three booklets and a 240 page manual recently written by John Branegan, GM4IHJ,

which really do present amateur radio space information in a readable and intelligible way. John wrote the first book on computer satellite tracking and supplied software for the early satellites way back in 1982, the proceeds from which he generously donated to AMSAT-UK. He has now ventured into Desk Top Publishing and his first efforts are *Space Station Mir*, *Satellite Dove Operating Manual* and *UoSAT 3 Oscar Operating Manual*. Their aim is to "bridge the information gap which accompanies all new satellites".

The contents of the Dove manual include:- Description of frequencies and operating modes, special telemetry, simple reception equipment, Space Station units, Cosmonaut's operating schedule, typical VHF Ground Station equipment and much else. A very interesting feature in this book is the inclusion of a number of experiments which can be carried out using the satellites enabling students to get 'hands-on' experience of satellite working. This should prove most helpful to teachers who want to add some practical work to their lessons on Space Science.



The Mir Booklet includes a description of the Space Station, the Cosmonauts' operating schedule, typical ground station units, the AREM - Austrian Amateur Radio Experiments to be carried eventually on Mir - and experiments using both Mir's radio signals and Mir as a visual target for eclipse and tracking studies.

The contents of the UoSAT 3 Manual include frequency, modes and operating data, simple receiving equipment, how to transmit to UoSAT 3, TNC modules, receiving and transmitting systems, etc. John comments:- "Please note UoSAT 3 is a very complex satellite requiring both 2 metre transmitter and 70cm receiver, a complex satellite 9600bps modem, a TNC and a computer with special software". If you only want to read UoSAT's bulletin on the downlink you do not of course need a transmitter, but you do need all the rest! This booklet also describes the operating facilities of the forthcoming UoSAT F. John thought the booklet would be slightly unpopular because of the complexity of the

satellite dealt with, but he has in fact already had to do two reprints of it. "In fact", he says, "Many of the purchasers really want to learn about using 9600bps FSK packet for terrestrial purposes rather than satellites. I had not considered this group but they have bought a lot of copies from quite a few places around the world because there is no other book anywhere about 9600bps operating". These booklets can be purchased directly from John Branegan, 8 Whitehills, Saline, Fife, Scotland, KY12 9UJ. The prices are: *Satellite Dove Operating Manual*, £4.50 (inc P&P). Foreign orders should be accompanied by UK Sterling cheques or money orders to cover cost and an extra £1 for postage. The *UoSAT 3 Oscar Operating Manual* is priced at £4.00, with an extra £1 for overseas purchasers. *Space Station Mir* is the same price. The three booklets are produced on a 'non-profit' basis.

SPACE RADIO HANDBOOK

FOR ANYONE LOOKING for a book covering the overall space scene, the RSGB has published a large book by John Branegan, called the *Space Radio Handbook*. It costs £11.34 to RSGB members and £13.34 to non members. This is a very good publication indeed. It covers just about every topic the satellite enthusiast needs to know about. The easiest way of giving the reader some idea of the comprehensive nature of this Manual, is to give the list of Chapter headings:- Space Radio Physics; Types of Satellites; Orbits and Tracking; Satellite Radio Reception; Amateur Radio Satellites; Weather and Experimental Satellites; Experiments in Space Radio; Man in Space; Space Radio Computing; Meteors; Comets; Moons and Asteroids; Amateur Radio Astronomy; Future of Amateur Radio in Space. Appendix 1 - useful addresses. Appendix 2 - Glossary. A really useful instruction Manual - an absolute must for the satellite enthusiast.

UOSAT F

UOSAT F, OR OSCAR 22 as it will be designated when launched, will be in orbit by the time you read this. At the time of writing, the expected date and time of launch was 0145GMT on 16 July. It should be launched into a 800km, polar sun-synchronous orbit. It will be able to support both amateur and non-amateur activities. The primary non-amateur mission is to provide store-and-forward communication for SatLife, formed by 1985 Nobel Prize winner, Dr. Bernard Lown. SatLife will use UoSAT F for a non-profit E-mail network for professional health services called Health Net, organised by five African medical schools. When not serving Health Net, on non-amateur frequencies, UoSAT F will transmit and receive on Amateur Satellite Service channels. The uplink will be on 2 metres with a 70cm downlink (same frequency plan as UoSAT-Oscar 14), so that stations already equipped for UO-14 will be able to use UoSAT F with the same software and hardware. There is to be a CCD camera aboard which incorporates all the lessons learned from previous UoSAT CCD experiments. It has a wide angled lens of 110° giving a field of view only slightly smaller than the satellite's footprint.



DataComms

RICK STERRY G4BLT
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JUST WHEN YOU THOUGHT it was safe to open the pages of *RadCom*, **DATAComms** returns! This column will now appear regularly every two months. I would very much like to know what you want to see in this column, and obviously I would be very grateful for any contributions.

First the ground rules for contributing to the column. I am active on Packet, (G4BLT @ GB7WRG), though please bear in mind that messages sometimes can and do get delayed or lost in the system. Please restrict message size to no more than 5k, as many UK mailboxes will not forward messages greater than 7k, (including headers). I can accept 3½in or 5¼in disks in 360/720k DOS format, (though not 1.2/1.44Mb), and in any BBC/Acorn DFS/ADFS format you like. Text should be in plain ASCII format, with no special formatting codes etc. Finally, there is conventional letter post. If you would like an acknowledgment of a letter, or require the return of a disk, then please enclose a return SASE, stamped address label, or postcard, as appropriate. Overseas readers should of course use IRCs instead of stamps. This will save a great deal of time, and the expense of postage.

Packet radio is very much a self-advertising medium, so I would like to turn the spotlight away from it to some extent, and remind readers that it is just one of many data modes available to the radio amateur. I hope to be featuring RTTY, AMTOR, FAX, synchronous CW, and anything else you can think of. That reminds me; is anyone still using the old German *Hellschreiber* system I wonder? My knowledge of German is rather rudimentary, but I translate that as 'brightness writer', and I recall that it was somewhat similar to Facsimile.

RTTY AND AMTOR

BOB CANNING, G0ARF, has written a couple of very interesting letters, in which he points out the almost complete absence of references to RTTY and BARTG in *RadCom* since 1989. [Actually 134 'RTTYs' and 11 'BARTGs', but who's counting? - Ed]. He says . . .

"State-of-the-art RTTY is far removed from the smelly oily rag image of yesterday, and we now use some pretty sophisticated software, especially in contests. Although I have a collection of Creed machines that I use for demos, I also run an XT clone with a variety of UK and USA software covering most data modes. Many of the 'old brigade' have upgraded, or are doing so, to take advantage of enhanced facilities."

Well, I rather liked the smell of oil and ozone associated with the old machines, but in fairness they were very bulky and noisy,

and lacked the ability to do any other job; contrast that with the versatility of a computer.

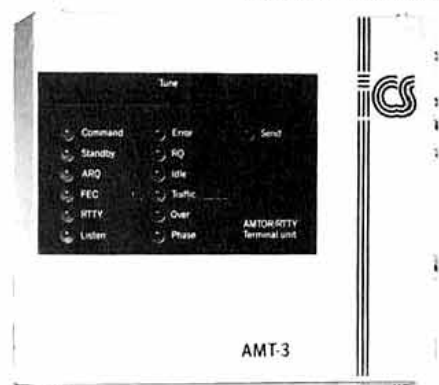
Packet is arguably best as a medium for sending and receiving information and files of various sorts. It certainly can be, and is, used as a 'live-QSO' mode, but in many cases it would be easier to pick up a microphone. However, though there are mailboxes for RTTY, and especially AMTOR, perhaps they are modes which are at their best when used for live QSOs. Packet is a frustrating mode for 'listeners', because a contact appears as many fragments intermingled with packets from other stations. AMTOR also can be a bit tricky to monitor, but RTTY is very easy, and listeners can enjoy it to the full. Unlike packet, which needs a fairly 'clean' frequency to work satisfactorily, RTTY and AMTOR, especially AMTOR, really come into their own when the going gets tough. With a good terminal unit and appropriate software, you can have a QSO under conditions that would be difficult or impossible on 'phone. Anyone who has not seen what AMTOR can do under conditions of heavy QRM, and with quite low transmitter powers, would be astonished.

RTTY/AMTOR EQUIPMENT

RTTY IS PROBABLY the easiest and cheapest data mode to become QRV on. All that is required is a simple 'unintelligent' RTTY Terminal Unit, a radio, and a suitable computer and software. In fact, in some cases the computer will do most of the work of a TU too, requiring minimal external hardware. AMTOR requires little or no extra hardware to RTTY, being effectively a sophisticated form of that mode, though the software has to be a lot more clever. For example, if you have a BBC microcomputer, then you can use the ROM software by Peter Harris, G3WHO, which caters for RTTY and AMTOR. This has been enhanced recently, and requires a simple TU such as the BARTG ST5 or the G3LIV board, plus an external clock generator from G3LIV. The only snag is the BBC Micro's infamous habit of generating S9+ RFI over a large portion of the radio spectrum!

RTTY and AMTOR are available on expensive multi-mode terminals such as the PK232 and KAM, but there are cheaper alternatives. A British company, ICS, make the AMT3, which is a dedicated AMTOR/RTTY unit, or if you are lucky you might well be able to pick up a cheap secondhand AMT1

PHOTOGRAPH: ICS ELECTRONICS LTD



The AMT3 dedicated RTTY/AMTOR intelligent terminal unit. The older AMT1 and AMT2 units can make attractive secondhand buys.

or AMT2 unit. These older units also work very well. Like a packet TNC, these are intelligent devices that connect to the computer via a simplified RS232 serial link. The computer requires only a simple 'dumb terminal' program to communicate with the TU; specialist software is not required to get started. Unlike packet TNCs which have only a few indicators on the front, the ICS units are positively festooned with LEDs, telling you everything you need to know about what the unit is doing. I hope to go into more detail in a later issue as AMTOR is a somewhat strange mode to use, and rather demanding of the radio, but well worth the effort.

VHF RTTY

I WONDERED RECENTLY if there was still any RTTY activity on the 144MHz band, and if there had ever been much on 430MHz. There is still plenty on the HF bands, as a listen around 14.090MHz will tell you. However, there does seem to be a small but dedicated band of RTTY operators on Two. Bob, G0ARF, says that about six stations in the Worcester/Birmingham area often meet on AFSK (FM) RTTY on 145.300MHz at 2030UTC. They normally use 50Baud, but most can also handle 45.45Baud. Ted, G8CDW, tells me that he runs a small AFSK RTTY net on 145.300MHz in West Norfolk. The net is on Mondays at 1930 local time, and there are usually three to four regulars, plus the odd other station showing up from time to time. Does anyone in the UK use FSK (SSB) RTTY on Two, or is activity confined to local FM matters?

BARTG

G0ARF REFERRED TO BARTG, and I think it worth giving them more than a little mention. This formally stood for the British Amateur Teleprinter Group, but 'Teleprinter' has since been replaced with the more appropriate 'Teledata'. BARTG now supports all radio data modes, and produces an excellent quarterly magazine called *DATACom*. The Spring 1991 issue covered everything from AMTOR and synchronous CW, to dot-matrix printers, iambic keyers and packet. The Summer issue will feature a new data mode called CLOVER, and how to cure computer-generated RFI. The group also has its own RTTY news bulletin service on various bands and frequencies, rather like *GB2RS*, but using the callsign GB2ATG. The current UK subscription is £10.00, and for further details write to the membership secretary, Ann Reynolds, G6ZTF, 169 Bell Green Road, Coventry, Warks, CV2 7GW or telephone 0203 668491. To my shame, I let my BARTG membership lapse some time ago, but have since rejoined.

FUTURE TOPICS

ALTHOUGH I HAVE ALREADY SAID that I would like to pay more attention to modes such as RTTY and AMTOR, packet is very much a growth area, and I shall certainly not be ignoring it. DX Clusters and TCP/IP will be featured, and I am already assembling the necessary information. However, I shall be listening to what readers think should appear in this column, so who knows where that will lead?



Microwaves

MIKE DIXON G3PFR

'Woodstock', Gazebank, Norley, Warrington, Cheshire WA6 8LL

10GHZ OPENS TO LA (AND ELSEWHERE)

A LETTER FROM CHRIS, G4LOJ (near Norwich), tells the epic story of a recent contact he had with Norway - yes, on 10GHz! It reads as follows: 'For weeks prior to 30 May, I had been struggling with the mechanical nightmare of rotating a new dish through 360 degrees with the whole contraption bolted to the side of the tower . . . I managed to get it fitted up on the 30th and had hopes of hearing the Martlesham beacon (GB3MHX), which I couldn't . . . the next night (31 May) I went on 70cm to look for G3LQR to get him 'spotted' on the (changed) rotator . . . I found him working LA1T on 70cm and bemoaning the fact that he was having problems with his gear . . . He suggested some of the other locals might be around, so I called in . . . I worked LA1T on 23cm (with 500mW) and one way on 13cm (my TX had failed) . . . then an attempt was made on 6cm - no contact . . . I didn't have much hope for 3cm, but put the 10W transmitter on and beamed in their general direction. After five minutes, they couldn't find it . . . I said I'd leave it on for a while. Suddenly I heard a shout 'We've found it, can you key it?'. . . Oh dear! I run a fixed oscillator source on TX and to key it isn't easy . . . a hastily fitted diode in the power lead with the key across the diode via some resistors, I eventually sent them some chirpy CW! . . . reports were 519(?)C in both directions . . . in the direction of LA the dish fires through the tower and rotator, I guess signals would have been much stronger without this obstruction . . . lots of tests have been carried out with G3ZFP, G3LQR and G3JVL over the past few weeks and I have been very surprised with the level of activity on 3cm . . . Propagation, be it rain scatter, tropo or ducting, often makes the signals on 3cm better than those on 2m or 70cm'. Chris describes his equipment as 'definitely not state of the art . . . The preamp is an old tunnel diode device, no GaAs FETs yet, but working on it . . . The plan is now to get a beacon going here as per (his personal beacon on) 6cm'. Shows what can be done when you are in the right place at the right time with the determination to do it! Congratulations on a notable contact, believed to be a 'First'.

FURTHER EXPLANATION!

I OMITTED, LARGELY because of available space, to mention some other PCBs available from the

Microwave Components Service, in addition to those described last time. Briefly they are as follows:

G4FRE Beacon callsign generator and keyer PCB. This is designed to accommodate the G4FRE EPROM beacon keyer which is fully described in volume 2 of the *RSGB Microwave Handbook*. Four messages (of 4kb) and the appropriate control channels, can be programmed into a 2732 EPROM which retains its memory even when the power is switched off. Useful for either formal or personal beacons. If you are unable to program EPROMS yourself, I can do it: all you need supply to me is a blank 2732 EPROM (21V programming voltage), *exact* text of the message(s) required and return postage for the programmed EPROM.

The Microwave Committee UHF source (UC04) is an older design which is still available and useful as a microwave source. Generating at least 100mW (and often much more) in the 350 to 450MHz range this design, also, is fully described in volume 2 of the *Handbook*. It could be used as a low power 70cm transmitter/driver in addition to its more usual use as an LO source for microwave converters and transmitters.

A useful **low-voltage-drop regulator** circuit, derived from a Wood and Douglas design, used to stabilise power supplies where there must be a minimum voltage drop, eg when operating portable from almost discharged accumulators, is available as UC05. It, too, is described in the *Handbook*!

Remember that the Components Service is now operated by Mrs P Suckling, G4KGC, at 314A, Newton Road, Rushden, Northants NN10 0SY. Orders or enquiries must go direct to Petra, *not to RSGB HQ*.

TECHNICAL CORNER

DEVELOPMENT OF THE G3WDG series of 10GHz modules has continued, since the last update, with a major new module released at the end of June. This was the G3WDG 003 144 - 10,368MHz up-converter which completes the modules for a basic, but nevertheless 'hi-tech', transverter system. I say 'basic'

because there are other add-on modules being developed to increase the performance of the '002/003 combination making up the basic transverter.

The '003 module requires LO drive at 2556MHz from the G4DDK-004 crystal controlled source, as usual. The circuit of the transmit up-converter is shown in Fig 1. The thick black elements in the circuit are representations of the microstrip lines and the black triangles are the radial decoupling stubs used widely in these modules. Note that a microwave monolithic integrated circuit (MMIC) - an Avanteck 'Modamp' or MODular AMplifier, IC1, - is included (and is, indeed, mandatory) and that this is followed by a 3dB splitter to divide the amplified LO signal, one half being fed to the coaxial connector, J2, for the receive converter and the other half via C4 to the x4 multiplier GaAs FET, TR1. This is followed by the now-familiar cavity resonator to select the required harmonic. TR2 is an active mixer requiring a 144MHz signal (via the coaxial connector J3) of about 1mW to be fed, along with the 10,224MHz LO signal, into the gate of this GaAs FET. Then follows an amplifier chain consisting of an image rejection cavity, filter FL2, amplifier TR3, filter FL3, amplifier TR4, filter FL4 and two further stages of amplification, this time without additional filters, to the final output socket, J4. The module fits into a type 7760 tinplate box from Piper Communications.

During development of this module, it was found that the input VSWR of the Modamp was rather poor, resulting in less than the maximum available gain from this stage. The poor match can also cause the 'DDK-004 output circuit to require retuning when connected to the module. The coaxial cable length between the modules will then become critical. These problems were overcome by modifying the input circuit to the modamp to include a 1pF capacitor to ground at a certain point on the input line. Users of the G3WDG-001 multiplier/PA module could probably also benefit from this modification. Full details of the modification, together with a suitable 1pF chip capacitor and Veropin are available from G3WDG, at the Components Service address given earlier, on receipt of an

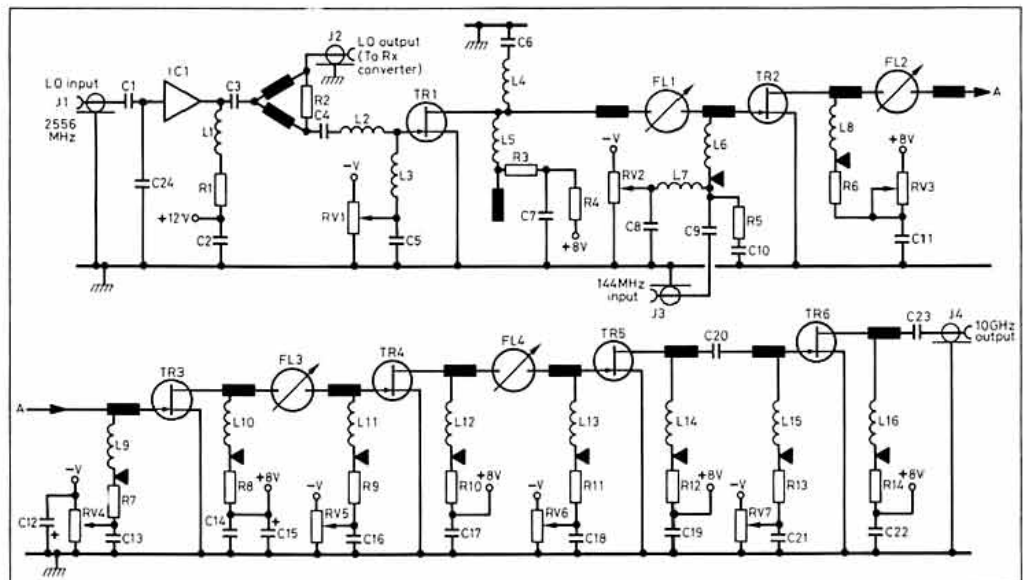


Fig 1: G3WDG - 003 transmit up-converter.

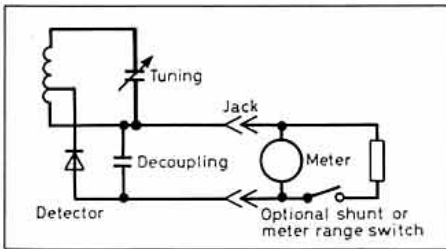


Fig 2: Wavemeter circuit.

SAE. Details and current price/availability of the '003 mini-kit (and other items in the Components Service) can be obtained from Petra, G4KGC.

The next modules in the pipeline are the G3WDG-005, a two-stage 10.0 - 10.5GHz amplifier with optional image rejection filter. Applications for this module are to improve the performance of existing 10GHz narrow-band equipment eg a G3JVL transverter, and as a front-end for recently available surplus equipment. This latter application requires the use of an image rejection filter, hence this option is included on the board. The module is, as I write (June), undergoing trial construction.

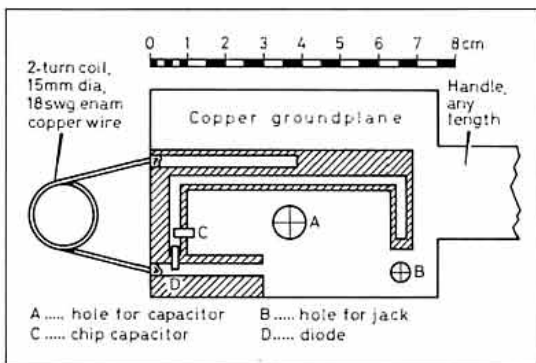


Fig 3: VHF wavemeter PCB.

Future plans are to produce a PA module to follow the G3WDG-001 or '003 units, with a power output of 200-250mW. A version with 500mW output is also being considered, if a source of reasonably priced GaAs FETs can be located. Some work on a single-stage low-noise preamplifier (G3WDG-004) has also been done. A version using a reasonably

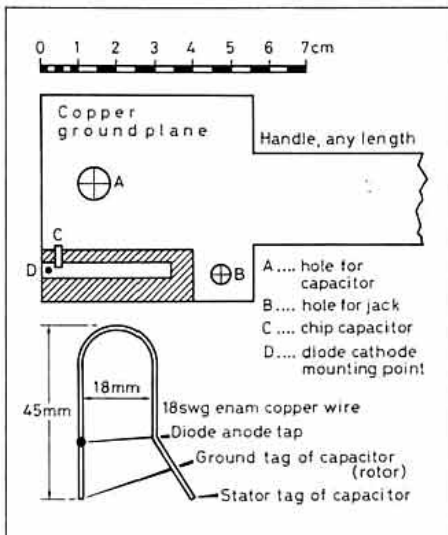


Fig 4: UHF wavemeter PCB.

priced HEMT (High Electron Mobility Transistor) has produced noise figures around 1.25dB with a gain of 14dB. Thanks to Charlie, G3WDG, for this latest update.

BEGINNERS CORNER

FIRST, APOLOGIES FOR an omission in the July column. Somehow I managed to omit, in the PCB milli-Wattmeter layout, the fact that the two chip resistors fit between the pads labelled A and B and the input line, the diode fits across the space marked X (with the shortest leads possible) and the four decoupling capacitors between pads C and D and the line and E and F and the line - where the dotted lines are. Also the caption read 1A419 but should have been 1N419.

Now to this month's subject, which is how to make frequency measurements in the VHF/UHF range. Thanks to Mike Scott, G3LYP, for supplying the following ideas for methods of measurement which don't require expensive or elaborate equipment. In fact, most of the ideas which follow need only cost tens of pence, rather than tens of pounds!

Typical microwave oscillator sources such as the G4DDK-001 (reviewed in the May column) usually start off with crystal frequencies around the 88 to 108MHz mark, depending on the application. That should immediately suggest a way of checking that the crystal oscillator stage is functioning correctly - yes, tune it in on an FM broadcast receiver with the antenna disconnected and the squelch disabled! The crystal is unmodulated and the signal will only be detectable by quieting of the hiss. The frequency reading on the tuning scale should approximate to that of the crystal. If it appears to be a long way out, the circuit could be self-oscillating at a frequency not controlled by the crystal. If the oscillator is controlled by the crystal, touching the oscillator coil or moving the core slightly will have little effect on the signal heard on the receiver. If it is self-oscillating, there will be a large change of frequency when the coil is touched or the core moved.

Checking the frequencies of the multiplier stages which follow the oscillator is a little more demanding! These frequencies might lie anywhere within the range 150 to 2500MHz. The simplest solution is to use absorption wavemeters. Note the plural! It is difficult (but possible) to build a single wavemeter covering the whole of this range and so it is better to build two or three covering, for instance, 60 to 160MHz, 150 to 300 MHz and 250 to 2500MHz.

The first two are easily and inexpensively made. Fig 2 gives the circuit of the first two. Either consists of a coil or loop of wire, a variable tuning capacitor, a diode to detect the RF, a decoupling capacitor and a meter to indicate resonance. Note that the diode is tapped into the tuned circuit. The tapping point is a compromise between obtaining enough signal to give a decent meter reading and reducing the Q of the circuit to an extent which affects the sharpness (or resolution) of the tuning. The use of a sensitive meter eg 10 to 50 or 100µA helps in this respect.

The suggested method of construction is shown in Figs 3 and 4. Each is built on a piece of 0.1in thick single clad PCB material cut to roughly the dimensions shown: the sizes are not critical, except you'll find difficulty in coupling the wavemeter to the circuit under test if the wavemeter is too large. Again, it is possible to use thinner (1/16in) board, but this is less rigid. Etching patterns are also given in the figures: again, these are not really critical and you could produce the tracks by cutting through the copper with a sharp blade and stripping off the unwanted copper by applying a hot soldering iron to the unwanted copper and peeling it off whilst the board bonding is soft. The tuning capacitors were small 50pF types with 5/16in bushes and 7/32in shafts, obtained from a rally. One was used 'as is' for the 60MHz to 160MHz version. For the other, half the rotor and stator plates were removed. The copper track forms part of the tuned circuit in the lower frequency unit and the junction between the track and the rest of the coil forms a convenient tapping point for the diode. To keep the stray capacitance to a minimum, the loop on the higher frequency unit is soldered directly to the tags on the tuning capacitor, with the diode soldered between the loop, about 1/2in from the ground end, and a track on the PCB. The tuning capacitors are mounted on the track side of the board and a paper calibration scale on the other (tuning knob) side. Once calibrated, the scale can be protected by a coat of varnish or lacquer.



To keep the units small, a 3.5mm jack socket is fitted and used to connect a screened lead to a separate meter - either a multimeter or, for instance, an inexpensive miniature panel meter, again often obtainable from rallies and often with a sensitivity of 50 or 75µA. The scale of the meter does not matter, all that is required is an indication.

Once completed, how do you calibrate the wavemeters? This is best done with a Dip Oscillator or signal generator, maybe at a 'Round Table' for instance, or by enlisting help from another local amateur. Calibration does not have to be exact, because what you mainly are interested in is whether the stage being measured is within, say, 10 or 20MHz of where it ought to be. In other words you need to know whether that stage you've just peaked up by measuring voltage drop across an emitter resistor is doubling and not simply amplifying or tripling! Failing help, you could use Lecher lines (RSGB VHF/UHF Manual, pages 9.2 to 9.4) to calibrate a tunable oscillator (page 11.40) which is, in turn, used to calibrate your wavemeters. If really desperate, you could even buy ready-made wavemeters! More about that next time.

Next time we'll consider how to build a wavemeter covering the rest of the required range, from about 250MHz up to 2500MHz, using standard copper tube and plumbing fittings, plus a few more bits and pieces. □

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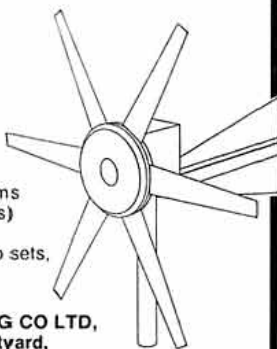
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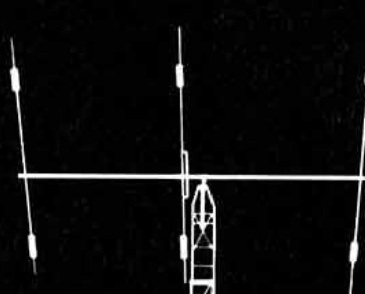
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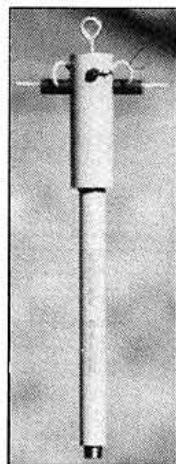
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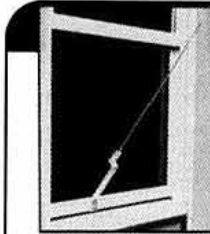
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MORSE

For many months, letters about the pros and cons of CW have appeared in *RadCom* and the other radio magazines. I believe that the Morse test should, of course, be kept for those wishing to use CW, but that it should no longer be the method of gaining the Class 'A' licence. I think that a further RAE type exam would be a genuine way of getting on to HF.

I have been an SWL since childhood, and a licensed amateur since 1985 and I enjoy the hobby very much indeed, being particularly interested in the practical side, such as conversion of ex-PMR etc. I would very much like to use HF, but do not have enough time or interest in CW.

I am 36, and I run my own small business, working six sometimes seven days per week. After a 10 hour working day plus one hour or more on the accounts, I've had enough; the last thing on my mind is playing with CW. I say playing because that is what it is, playing; it's only a hobby.

Mr McIntyre, G13YDH, in his letter in the August issue of *RadCom* suggests that if I don't do the CW it is because I am too lazy and not fit to go out on HF. I find this deeply insulting. Introduce a genuine method of gaining a Class 'A' licence and I will be happy to go for it.

Mr O W Rogers G1FXD

In *The Last Word* of recent months there have been some interesting letters re Morse and, as a relative newcomer to ham radio, I feel that I must also comment.

I personally read the news of a codeless licence with dismay as I frankly cannot see which advantages would accrue. At least with Morse there is better discipline and much less of the vital frequency space occupied than by other modes on the already overcrowded bands.

Also, before people rush to write in, I wish they would check their facts first. I can assure G3ENV that the military do still teach and use CW and their operators are classed as *specialists*!

Furthermore, CW is an important means of communication for certain handicapped people. So I can't quite see what G3ENV and G8BZL are trying to say. If they don't want to use CW that's their prerogative, but please don't rubbish those who do. Having qualified for my 'A' I don't think I particularly want to rush back to 'voice'; I can do that by picking up a telephone.

Tom Shelley G0MFV.

ELITIST

I cannot help but contrast the views expressed by G3JDK and G13YDH (*RadCom* August 1991). G3JDK believes that the use of HF AM will encourage people to hear and find out more about amateur radio.

G13YDH, on the other hand, believes that unless one passes a 20WPM Morse test, one is not worthy of holding an amateur licence. I have just gone through the ordeal of the Morse test and have passed but I resent this sort of narrow, elitist idea. Doesn't he care about introducing newcomers to the hobby? If he doesn't, it is indeed sad for all of us.

S A Slater BRS92755, soon to be G0P**

MORSE COSTS LESS

G8BZL asks why we "persist in maintaining such an archaic ritual" as the Morse test. Presumably the object of the Novice Licence is to encourage young people. If you were only 12 or 14, you would be unlikely to afford a commercial rig, but you could have a lot of fun making a simple QRP CW transmitter.

If Morse were excluded from the Novice Licence this option would be denied you and unless you had a generous uncle you might not get on the air at all.

M Lindsay G0IYY

NOT UNMANNED

As a user of all bands, I for one would like to continue to do so and not have to succumb to more noise coming from yet more *unmanned* transmissions.

I, and most one-to-one or group operators, enjoy the challenge of getting a contact at the time of being on-air, and not while asleep or at work. So, to the allocation of yet another frequency to packet radio on any band (UHF, VHF, HF, 2m or 6m), particularly to *unmanned stations*, I say "No, No, No!"

The VHF committee and the RSGB should try and keep an amateur band frequency for the amateur and not let it get lost in the noise of the 'commercial stations' which are getting more and more troublesome.

D G Still G0OOC

The Last Word

GAZUMPED!

The members of the North Cornwall/Cousin Jacks Contest Group wish to apologise for their absence on VHF NFD to all stations who usually get a DX contact.

After many years of using the same field we found we had been gazumped by another group. Perhaps all clubs could include in their newsletters the Code of Practice printed in *Radio Communication* (p64 December 1990).

"2. Take all possible steps to ensure that a site is not going to be used by some other group or club. Check with the club and last year's results table to see if any group used the site last year. Come to an amicable agreement before the event."

Where has the old spirit of Amateur Radio gone? Yours, in more sorrow than anger . . .

A E Warne G3YJX

A BIGGER CAKE?

The suggestion of VHF committee to allocate even more channels for use by packet is pushing the 144MHz bandplan a bit too far. The infringement of the FM simplex S11-S23 would mean a severe loss.

Now that 146MHz+ is being cleared, is there any pressure for an increase in the total frequency allocation, in which case the positioning of all digital or pulse type communications could be given a few discrete channels above 146. Most current sets can be modified to include 144 to above 146MHz.

It may be that in some parts of the country full use is not made of the existing channels, but in other parts these channels can be very busy. I am sure the average amateur would prefer to keep the speech channels clear of digital noise, so I would suggest that more thought and consideration be taken by the VHF communications before damage is done to the present channels.

C B B Farmer G1LDP

AFTERBYRNE

I note that you have seen fit to publish (*RadCom* August 1991 p 5) a cartoon of a beagle riding a space shuttle. I find it regrettable that you should consider printing something so trivial and flippant. Shame, sir! *Radio Communication* is a serious journal, not a comic.

In disgust, Paul Thompson G6MEN

[Sorry Paul, I obviously Byrnt my fingers there - Ed]

50P A QSO

Noting that Graham Layzell (G3AMM) has had 5000 QSOs with just one station (*Last Word*, August 1991) prompts me to mention that this is more than all the QSOs I have ever had world-wide since being licensed in 1947. I have this week logged no:4488 and wonder whether this is perhaps another sort of record?

Activity, though low, has been fairly evenly spread over the 44 year period using full licensed power, phone/CW, all bands 80m to 10m plus a short spell on 2m. At this rate, the average cost per QSO for equipment and licence fee is not insignificant and works out at around 50p! Any advances on that figure?

K B Tackley G3BRQ

Please note that the views expressed in 'Last Word' are not necessarily those of the RSGB.

We reserve the right to edit letters and regret that we can no longer acknowledge them individually but will pass them on to the relevant department.

PACKET BANDPLANNING

One understands that the demand for 2m packet radio is over-stretching the present allocation of frequencies, so it is not unexpected to read that the VHF committee suggests that further allocations should be made in the band, even to the extent of proposing a frequency outside the IARU band plan provisions. This confirms the mania for the mode and the self-importance of many of those who use it. Packeteers should realise that they are in the minority among radio amateurs.

The proposal to make inroads into precious FM channels and into the SSB/CW part of the band is absolutely unacceptable to many of us, and must not be allowed. The 2m band is the basic phone band for most amateurs, particularly B licensees, and in heavily populated parts of the country, very crowded, especially on FM.

By contrast, 70cm, 6m and 4m are under-used and highly suitable for packet. 430MHz is in dire need of a shot in the arm, and expansion of 70cm packet would help enormously.

The item on page 7 of August *RadCom* was probably the most important topic for all B licensees (and most other amateurs) that I have seen since I was first licensed . . . and what was deemed to be the No:1 story? Incredibly, it was Snoopy. I can only assume that the packet frequency story was given less prominence in an attempt to push the proposals through with a minimum of fuss from the usually silent majority.

Laurie Bradshaw G0MRL

[Can one really describe a quarter-page *RadCom* item asking for the views of members as "an attempt to push proposals through"? - Ed]

THE ULTIMATE KEY

I thoroughly agree with Dave Ingram's, K4TJW, review of the G4ZPY 'VHS twin paddle'. Gordon Crowhurst has produced the ultimate key. I was privileged to purchase one of the early keys and I treasure it. Keep up the good work Gordon.

Bob Daw G0MCE

FACT NOT FICTION

I am sorry to write to you on an unsavoury aspect of amateur radio. Late evening tuning 80m SSB, a group was suffering obvious strong interference. My usual disgust was felt listening to this unnecessary behaviour when a strange voice (not in the group) announced the interference "is coming from G3RHM in Greenford".

We must all surely deprecate deliberate interference. However, a far greater crime is to accuse a totally innocent party. If the misguided announcer had applied his callsign to his comment, he would have been robustly reminded of the laws of libel. I would remind inexperienced amateurs, do not guess.

G D Clarkson G3RHM

[Any evidence of deliberate interference should be reported to the Coordinator of the RSGB Amateur Radio Observation Service, Geoff Griffiths, G3STG, and never mentioned over the air - Ed]

SRI NO QSL

I notice in *The Last Word*, August, I am credited as having helped in the QSLing of the QSL Bureau. Somehow, someone has got completely muddled up and I cannot take credit for something I did not do!

The QSL Bureau certainly is a super organisation and long . . . may it continue.

Constance Hall G8LY

EAR DAMAGE?

After watching a report on TV about how a personal portable hi-fi can damage your hearing with the music being played, I wonder how many radio amateurs and SWLs are damaging their hearing when they put on headphones and turn the volume up full to pick out DX in the QRM.

Colin Watson BR46598












PAY COLLECT

Re the letter from Ted Allen, G3DRN, (*Last Word*, August), whilst I have always appreciated the excellent work that he has performed during many years, I cannot agree with his suggestion that members who send large numbers of QSLs via the Bureau should pay a pro-rata fee. With respect, I would suggest that if more money is required for the service, then those who pay nothing at present - in other words non-members - should pay a fee for collecting their cards from the Bureau.

E J King G3DCC

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UR95, 2.3mm, 50 ohm, mini nylon coax	30p/m
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UR70, 6mm dia, 75 ohm transmitting coax	30p/m
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300 ohm standard ribbon	18p/m
RG62AU, 6mm dia, 95 ohm coax	50p/m
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Two core screened cable, 5mm	25p/m
3 core mains, 5 amp, cable	20p/m
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6 core rotator cable, heavy duty	45p/m
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Red/black DC power cable, 8 amp	30p/m
PVC coated AE wire, heavy duty	12p/m
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NEW 300 ohm HEAVY DUTY SLOTTED Feeder	60p/m
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Please write enclosing a full cv to

Richard McLachlan
Lowe Electronics Ltd
Chesterfield Road
Matlock Derbys
DE4 5LE

Government Communication Headquarters



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